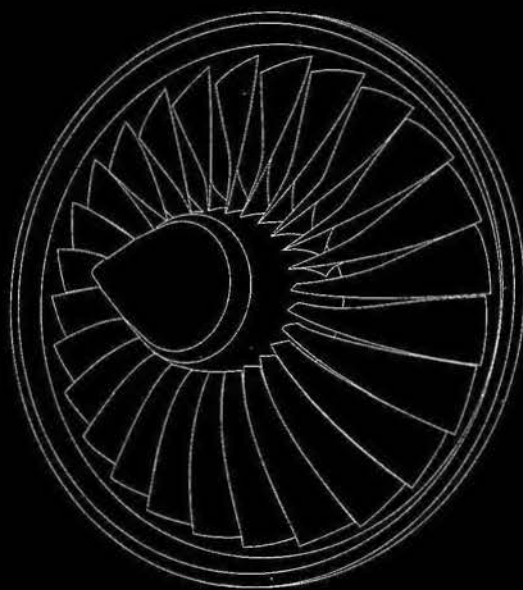


Turbofan and Turbojet Engines

Database Handbook



Élodie Roux

GE-1019.001

Élodie
Roux

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Éditions Élodie Roux

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ELODIE ROUX

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DATABASE HANDBOOK

Élodie Roux



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Foreword

This book shows the engine data which I have collected in recent years, from reference books or web sites (cf. the bibliography on page 595). I have tried to compare the sources in order to make these data as reliable as possible, but please feel free to inform me of any mistakes. I would like to improve and complete this database.

The data are listed under the engines' names, which should usually be the most convenient arrangement.

To find an engine from its manufacturer, use the index on page 575.

Also, the engines installed in a given jetliner or freighter can be found in the last chapter (page 565).

In an aircraft design study it could be useful to find an engine of given thrust, so a summary table (page 529) lists the engine specifications under static sea level thrust.

The list of variables (on page 41) shows the notation used.

Élodie Roux
(*Elodie.Roux@supaero.org*)

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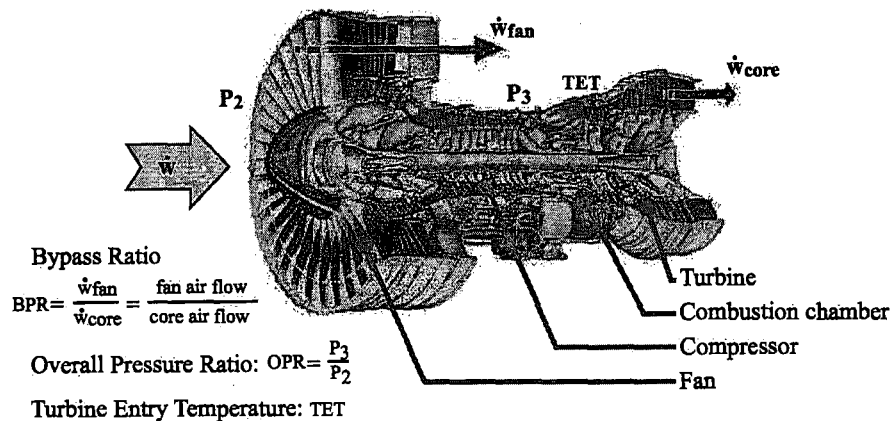
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Chapter 1

List of variables

Symbols	Designation	Units
BPR	: Engine bypass-ratio at static sea level. It is the rate of air flow moving through the fan and through the core.	
Composition	: Fan / LPC / HPC / HPT / IPT / LPT Stages	
	: Fan - Number of fan stages	
	: LPC - Number of low-pressure compressor stages	
	: HPC - Number of high-pressure compressor stages	
	: HPT - Number of high-pressure turbine stages	
	: IPT - Number of intermediate-pressure turbine stages	
	: LPT - Number of low-pressure turbine stages	
	: Sometimes, capital letters appear : "B" means Booster stage (The low-pressure compressor is fixed on the fan shaft.), "C" means centrifugal compressor, "G" means the fan and the low-pressure compressor have different rotational speed thanks to a gear box, "R" means radial turbine.	
D	: Engine diameter (max width)	m
D_{fan}	: Fan diameter	m
FPR	: Fan Pressure Ratio	
h_{cr}	: Cruise altitude	m

Symbols	Designation	Units
L	: Engine length	m
M_{cr}	: Cruise Mach number	
Nb of shafts	: Number of shafts	
OPR	: Overall Pressure Ratio at static sea level	
OPR_{cr}	: Overall Pressure Ratio in cruise	
SFC_{ssl}	: Specific Fuel Consumption (mass of fuel needed to provide a given thrust for a given period) at static sea level	$(kg/s)/N$
SFC_{ssl}^{AB}	: Specific Fuel consumption with afterburner	$(kg/s)/N$
SFC_{cr}	: Specific Fuel Consumption in cruise	$(kg/s)/N$
TET	: Turbine Entry Temperature at static sea level	K
T_{cr}	: Cruise thrust (at cruise Mach M_{cr} and altitude h_{cr})	N
T_{ssl}	: Static sea level thrust without afterburner	N
T_{ssl}^{AB}	: Static sea level thrust with afterburner	N
W_{eng}	: Engine mass (without pod or equipments)	kg
\dot{w}_{cr}	: Air flow in cruise	kg/s
\dot{w}_{ssl}	: Air flow at static sea level	kg/s



PW4000 cross-section

Chapter 2

Engine data

109-001

Manufacturer: Heinkel

Application: He 280

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4902 N$ $T_{ssl}^{AB} = N$

$= 1102 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

109-003A

Manufacturer: BMW

Application: Ar 234, MiG I-300 prototype

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7784 N$ $T_{ssl}^{AB} = N$

$= 1750 lbf$ $= lbf$

$SFC_{ssl} = 3.97 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.4 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 19.5 kg/s = 43 lb/s$

BPR = OPR = 3.1

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

109-004B-0

Manufacturer: Jumo

Application: Ar 234B-0/-1/-2, Ar 234C-2

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 8238 N$

$= 1852 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

109-004B-1

Manufacturer: Jumo

Application: Ju 287 (not produced)

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 8825 N$

$= 1984 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

109-004D

Manufacturer: Jumo

Application: Ar 234C-8 (not produced)

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 10298 N$

$= 2315 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

109-007

Manufacturer: Daimler-Benz

Application: Technology demonstrator

Composition: - / 9 / 8 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 11121 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 2.31 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.81 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 50.8 \text{ kg/s} = 112 \text{ lb/s}$

BPR = OPR = 8

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

109-011

Manufacturer: Heinkel

Application: Technology demonstrator

Composition: - / - / 3 + 1C / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 12749 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2866 \text{ lbf}$ $= lbf$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

109-012

Manufacturer: Jumo

Application: Ju 287 (not produced)

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 27445 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 6170 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 3.25 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 1.15 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 49.9 \text{ kg/s} = 110 \text{ lb/s}$

BPR = OPR = 5.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

109-018

Manufacturer: BMW

Application: Ju 287 (not produced)

Composition: - / - / 12 / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33317 N$ $T_{ssl}^{AB} = N$

$= 7490 lbf$ $= lbf$

$SFC_{ssl} = 3.33 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.18 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 44 kg/s = 97 lb/s$

BPR = OPR = 7

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adder

Manufacturer: Armstrong Siddeley

Application: Saab 210 (Draaken prototype)

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4448 N$ $T_{ssl}^{AB} = N$

$= 1000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adour Mk.851

Manufacturer: Rolls-Royce/Turboméca

Application: Hawk Mk.51/51A/52/53, (cf.également F405-RR-400)

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.785 m$

$W_{eng} = 568 kg = 1252 lb$ $= 30.9 in$

Static Sea Level:

$T_{ssl} = 23131 N$ $T_{ssl}^{AB} = N$

$= 5200 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 1.948 m$

$= 76.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adour Mk.861

Manufacturer: Rolls-Royce/Turboméca

Application:

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.782 m$

$W_{eng} = 577 kg = 1272 lb$ $= 30.8 in$

Static Sea Level:

$T_{ssl} = 25355 N$ $T_{ssl}^{AB} = N$

$= 5700 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 11.3

FPR = TET = °K

Nb of shafts = 2

$L = 1.948 m$

$= 76.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adour Mk.861-49

Manufacturer: Rolls-Royce/Turboméca

Application: Hawk Mk.60/60A/61/63A/63C/64/65/66/67

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.782 m$

$W_{eng} = 582 kg = 1283 lb$ $= 30.8 in$

Static Sea Level:

$T_{ssl} = 24243 N$ $T_{ssl}^{AB} = N$

$= 5450 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 1.948 m$

$= 76.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adour Mk.871

Manufacturer: Rolls-Royce/Turboméca

Application: Hawk Mk.102/103/108/109/127/200-60/200-100/203/205/208/209, CT-155 Hawk, Jaguar I

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = 0.559 m = 22 in$ $D = 0.785 m$

$W_{eng} = 603 kg = 1329 lb$ $= 30.9 in$

Static Sea Level:

$T_{ssl} = 26823 N$ $T_{ssl}^{AB} = N$

$= 6030 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 44 kg/s = 97 lb/s$

BPR = 0.8 OPR = 11.3

FPR = TET = °K

Nb of shafts = 2

$L = 1.948 m$

$= 76.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adour RT.172 Mk.102

Manufacturer: Rolls-Royce/Turboméca

Application: Jaguar GR.1, Jaguar A/E/S

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.782 m$

$W_{eng} = 704 kg = 1552 lb$ $= 30.8 in$

Static Sea Level:

$T_{ssl} = 22730 N$ $T_{ssl}^{AB} = 30826 N$

$= 5110 lbf$ $= 6930 lbf$

$SFC_{ssl} = 2.1 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 4.25 \cdot 10^{-5} (kg/s)/N$

$= 0.74 (lb/h)/lbf$ $= 1.5 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 9.6

FPR = TET = °K

Nb of shafts = 2

$L = 2.969 m$

$= 116.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adour RT.172 Mk.104

Manufacturer: Rolls-Royce/Turboméca

Application: Jaguar GR.1/GR.1A/T.2/T.2A/GR.3/T.4, Jaguar B/IB/S/IS/IM, Jaguar M (not produced)

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = 713 kg = 1572 lb$ $= in$

Static Sea Level:

$T_{ssl} = 22730 N$ $T_{ssl}^{AB} = 32494 N$

$= 5110 lbf$ $= 7305 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adour RT.172 Mk.106

Manufacturer: Rolls-Royce/Turboméca

Application: Jaguar GR.3/T.4

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24910 N$ $T_{ssl}^{AB} = N$

$= 5600 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Adour RT.172 Mk.151

Manufacturer: Rolls-Royce/Turboméca

Application: Hawk T.1/T.1A/T.1W

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.782 \text{ m}$
 $W_{eng} = 544 \text{ kg} = 1199 \text{ lb}$ $= 30.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 23131 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 5200 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/N$ $SFC_{ssl}^{AB} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR = 0.8$ $OPR = 11$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = 1.948 \text{ m}$
 $= 76.7 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Adour RT.172 Mk.804

Manufacturer: Rolls-Royce/Turboméca

Application: Jaguar I

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.782 \text{ m}$
 $W_{eng} = 713 \text{ kg} = 1572 \text{ lb}$ $= 30.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 23664 \text{ N}$ $T_{ssl}^{AB} = 35764 \text{ N}$
 $= 5320 \text{ lbf}$ $= 8040 \text{ lbf}$
 $SFC_{ssl} = (\text{kg/s})/N$ $SFC_{ssl}^{AB} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = 2.969 \text{ m}$
 $= 116.9 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Adour RT.172 Mk.811

Manufacturer: Rolls-Royce/Turboméca

Year: 1977

Application: Jaguar I, Hawk, T45A sans PC, et Jaguar, T-2, F-1 avec PC

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = 0.559 \text{ m} = 22 \text{ in}$ $D = 0.782 \text{ m}$
 $W_{eng} = 738 \text{ kg} = 1627 \text{ lb}$ $= 30.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 24554 \text{ N}$ $T_{ssl}^{AB} = 37365 \text{ N}$
 $= 5520 \text{ lbf}$ $= 8400 \text{ lbf}$
 $SFC_{ssl} = 2.03 \cdot 10^{-5} (\text{kg/s})/N$ $SFC_{ssl}^{AB} = (\text{kg/s})/N$
 $= 0.72 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 43.1 \text{ kg/s} = 95 \text{ lb/s}$
 $BPR = 0.75$ $OPR = 11.3$
 $FPR = 2.35$ $TET = 1413 ^\circ K$

Nb of shafts = 2

$L = 2.969 \text{ m}$
 $= 116.9 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Adour RT.172 Mk.815

Manufacturer: Rolls-Royce/Turboméca

Application: Jaguar I

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.782 m$

$W_{eng} = 741 kg = 1634 lb$ $= 30.8 in$

Static Sea Level:

$T_{ssl} = 24554 N$ $T_{ssl}^{AB} = 37365 N$

$= 5520 lbf$ $= 8400 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 43.1 kg/s = 95 lb/s$

BPR = 0.75 OPR = 11.3

FPR = TET = °K

Nb of shafts = 2

$L = 2.969 m$

$= 116.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AE3007

Manufacturer: Allison

Application: EMB-145, Citation 10

Composition: / / / /

$D_{fan} = 0.978 m = 38.5 in$ $D = m$

$W_{eng} = 717 kg = 1581 lb$ $= in$

Static Sea Level:

$T_{ssl} = 32000 N$ $T_{ssl}^{AB} = N$

$= 7194 lbf$ $= lbf$

$SFC_{ssl} = 1.02 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.36 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 110 kg/s = 242.5 lb/s$

BPR = 5 OPR = 23

FPR = TET = °K

Year: 1994

Nb of shafts =

$L = 2.713 m$

$= 106.8 in$

Cruise:

$T_{cr} = N$

$= 0 lbf$

$SFC_{cr} = 1.84 \cdot 10^{-5} (kg/s)/N$

$= 0.65 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10670 m$

AE3007A

Manufacturer: Allison

Application: ERJ-135ER, ERJ-145ER

Composition: 1 / - / 14 / 3 / - / 2

$D_{fan} = 0.978 m = 38.5 in$ $D = 1.105 m$

$W_{eng} = 719 kg = 1585 lb$ $= 43.5 in$

Static Sea Level:

$T_{ssl} = 33717 N$ $T_{ssl}^{AB} = N$

$= 7580 lbf$ $= lbf$

$SFC_{ssl} = 1.02 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.36 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 133.4 kg/s = 294.1 lb/s$

BPR = 5.3 OPR = 24

FPR = TET = °K

Nb of shafts = 2

$L = 2.705 m$

$= 106.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AE3007A1

Manufacturer: Allison

Application: ERJ-135ER, ERJ-145ER

Composition: 1 / - / 14 / 3 / - / 2

$D_{fan} = 0.978 \text{ m} = 38.5 \text{ in}$ $D = 1.105 \text{ m}$

$W_{eng} = 719 \text{ kg} = 1585 \text{ lb}$ $= 43.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 33717 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7580 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 133.4 \text{ kg/s} = 294.1 \text{ lb/s}$

BPR = 5.3 OPR = 24

FPR = TET = °K

Nb of shafts = 2

$L = 2.705 \text{ m}$

$= 106.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

AE3007A1/1

Manufacturer: Allison

Application: ERJ-135ER/LR, ERJ-145LR

Composition: 1 / - / 14 / 3 / - / 2

$D_{fan} = 0.978 \text{ m} = 38.5 \text{ in}$ $D = 1.105 \text{ m}$

$W_{eng} = 730 \text{ kg} = 1609 \text{ lb}$ $= 43.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 33717 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7580 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.3 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 2.705 \text{ m}$

$= 106.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

AE3007A1/3

Manufacturer: Allison

Application: ERJ-135LR, ERJ-140, Legacy Corporate Shuttle

Composition: 1 / - / 14 / 3 / - / 2

$D_{fan} = 0.978 \text{ m} = 38.5 \text{ in}$ $D = 1.105 \text{ m}$

$W_{eng} = 730 \text{ kg} = 1609 \text{ lb}$ $= 43.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 32027 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.3 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 2.705 \text{ m}$

$= 106.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

AE3007A1E**Manufacturer:** Allison**Application:** ERJ-145XR**Composition:** 1 / - / 14 / 3 / - / 2 $D_{fan} = 0.978 \text{ m} = 38.5 \text{ in}$ $D = 1.105 \text{ m}$ $W_{eng} = 730 \text{ kg} = 1609 \text{ lb}$ $= 43.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 36075 \text{ N}$ $= 8110 \text{ lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 5.3$ $FPR =$ $T_{ssl}^{AB} = \text{N}$ $= \text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $OPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 2.705 \text{ m}$ $= 106.5 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **AE3007A1P****Manufacturer:** Allison**Application:** ERJ-145LR, Legacy Executive**Composition:** 1 / - / 14 / 3 / - / 2 $D_{fan} = 0.978 \text{ m} = 38.5 \text{ in}$ $D = 1.105 \text{ m}$ $W_{eng} = 730 \text{ kg} = 1609 \text{ lb}$ $= 43.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 33717 \text{ N}$ $= 7580 \text{ lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 5.3$ $FPR =$ $T_{ssl}^{AB} = \text{N}$ $= \text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $OPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 2.705 \text{ m}$ $= 106.5 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **AE3007A3****Manufacturer:** Allison**Application:** ERJ-135**Composition:** 1 / - / 14 / 3 / - / 2 $D_{fan} = 0.978 \text{ m} = 38.5 \text{ in}$ $D = 1.105 \text{ m}$ $W_{eng} = 730 \text{ kg} = 1609 \text{ lb}$ $= 43.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 31137 \text{ N}$ $= 7000 \text{ lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 5.3$ $FPR =$ $T_{ssl}^{AB} = \text{N}$ $= \text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $OPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 2.705 \text{ m}$ $= 106.5 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$

AE3007C**Manufacturer:** Allison**Application:** Citation X**Composition:** 1 / - / 14 / 3 / - / 2 $D_{fan} = 0.978 \text{ m} = 38.5 \text{ in}$ $D = 1.105 \text{ m}$ $W_{eng} = 719 \text{ kg} = 1585 \text{ lb}$ $= 43.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 28655 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 6442 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 5.3$ $OPR =$ $FPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 2.705 \text{ m}$ $= 106.5 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **AE3007C1****Manufacturer:** Allison**Application:** Citation X**Composition:** 1 / - / 14 / 3 / - / 2 $D_{fan} = 0.978 \text{ m} = 38.5 \text{ in}$ $D = 1.105 \text{ m}$ $W_{eng} = 720 \text{ kg} = 1587 \text{ lb}$ $= 43.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 30088 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 6764 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 5.3$ $OPR =$ $FPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 2.705 \text{ m}$ $= 106.5 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **AI-222-25****Manufacturer:** Ivchenko**Application:****Composition:** / / / / $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 40345 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 9070 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.81 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= 0.64 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 1.19$ $OPR = 15.9$ $FPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = $L = \text{m}$ $= \text{in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$

AI-222-28

Manufacturer: Ivchenko

Application:

Composition: / / / /

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 45149 N$
 $T_{ssl}^{AB} = N$
 $= 10150 lbf$
 $= lbf$
 $SFC_{ssl} = 1.91 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.68 (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR = 1.13

OPR = 16.9

FPR =

TET = °K

Nb of shafts =

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$
AI-25

Manufacturer: Ivchenko

Application: Yak-40 'Codling', M-15

Composition: 3 / - / 8 / 1 / - / 2

 $D_{fan} = 0.56 m = 22 in$
 $D = 0.896 m$
 $W_{eng} = 320 kg = 705 lb$
 $= 35.3 in$

Static Sea Level:

 $T_{ssl} = 14679 N$
 $T_{ssl}^{AB} = N$
 $= 3300 lbf$
 $= lbf$
 $SFC_{ssl} = 1.62 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.57 (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 15 kg/s = 33.1 lb/s$

BPR = 2.1

OPR = 8

FPR = 1.7

TET = °K

Nb of shafts = 2

 $L = 1.993 m$
 $= 78.5 in$

Cruise:

 $T_{cr} = 4341 N$
 $= 976 lbf$
 $SFC_{cr} = 2.25 \cdot 10^{-5} (kg/s)/N$
 $= 0.8 (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = 0.5, h_{cr} = 6096 m$
AI-25A

Manufacturer: Ivchenko

Application: Yak-40A

Composition: 3 / - / 8 / 1 / - / 2

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 17126 N$
 $T_{ssl}^{AB} = N$
 $= 3850 lbf$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR = 2.1

OPR =

FPR = 1.7

TET = °K

Nb of shafts = 2

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$

AI-25TL**Manufacturer:** Ivchenko**Application:** L-39/-39C/-39V/-39ZA/-39ZO**Composition:** 3 / - / 9 / 1 / - / 2 $D_{fan} = m = in$ $D = m$ $W_{eng} = 350 \text{ kg} = 772 \text{ lb}$ $= in$ **Static Sea Level:** $T_{ssl} = 16868 \text{ N}$ $T_{ssl}^{AB} = N$ $= 3792 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.58 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 2$ $OPR = 9.5$ $FPR = 1.7$ $TET = ^\circ K$ **Nb of shafts** = 2 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **AI-25TLK****Manufacturer:** Ivchenko**Application:** K-8J**Composition:** 3 / - / 9 / 1 / - / 2 $D_{fan} = m = in$ $D = m$ $W_{eng} = 350 \text{ kg} = 772 \text{ lb}$ $= in$ **Static Sea Level:** $T_{ssl} = 16868 \text{ N}$ $T_{ssl}^{AB} = N$ $= 3792 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.58 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$ **Nb of shafts** = 2 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **AL-21****Manufacturer:** Saturn**Application:** Yak-38 'Forger-A'**Composition:** - / - / 14 / 3 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = \text{kg} = \text{lb}$ $= in$ **Static Sea Level:** $T_{ssl} = 79601 \text{ N}$ $T_{ssl}^{AB} = N$ $= 17895 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$ **Nb of shafts** = 1 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

AL-21F**Manufacturer:** Saturn**Application:** Tu-28P 'Fiddler-A/B'**Composition:** - / - / 14 / 3 / - / - $D_{fan} = m = in$ $D = m$

Nb of shafts = 1

 $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:** $T_{ssl} = N$ $T_{ssl}^{AB} = 109871 N$ **Cruise:** $T_{cr} = N$ $= lbf$ $= 24700 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$ **AL-21F-3****Manufacturer:** Saturn**Application:** Su-17M (Su-32M) 'Fitter-C', Su-17M2 'Fitter-D', Su-17UM (Su-22U)

'Fitter-E', Su-17M2D 'Fitter-F', Su-17UM3 'Fitter-G', Su-17M3 (Su-22M3) 'Fitter-H',

Su-17M4 (Su-22M4) 'Fitter-K', Su-24 'Fencer-A/B', Su-24MP 'Fencer-F'

Composition: - / - / 14 / 3 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$ $D = 0.884 m$ $L = 5.156 m$ $W_{eng} = 2005 kg = 4420 lb$ $= 34.8 in$ $= 203 in$ **Static Sea Level:** $T_{ssl} = 76509 N$ $T_{ssl}^{AB} = 110315 N$ $T_{cr} = N$ $= 17200 lbf$ $= 24800 lbf$ $= lbf$ $SFC_{ssl} = 2.15 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.27 \cdot 10^{-5} (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= 0.76 (lb/h)/lbf$ $= 1.86 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = 104.3 kg/s = 229.9 lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR = 14.8

OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$ **AL-21F-3A****Manufacturer:** Saturn**Application:** Su-24 'Fencer-C', Su-24M 'Fencer-D'**Composition:** - / - / 14 / 3 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$ $D = m$ $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:** $T_{ssl} = 76509 N$ $T_{ssl}^{AB} = 110315 N$ $T_{cr} = N$ $= 17200 lbf$ $= 24800 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$

AL-31F

Manufacturer: Saturn

Year: 1997

Application: Su-27 'Flanker-B', Su-30M/MKI/MKI (Su-27P) 'Flanker-C', Su-33 (Su-27K) 'Flanker-D'

Composition: 4 / - / 9 / 1 / - / 2

Nb of shafts = 2

 $D_{fan} = 0.905 \text{ m} = 35.6 \text{ in}$
 $D = 1.219 \text{ m}$
 $L = 4.953 \text{ m}$
 $W_{eng} = 1530 \text{ kg} = 3373 \text{ lb}$
 $= 48 \text{ in}$
 $= 195 \text{ in}$

Static Sea Level:

 $T_{ssl} = 79400 \text{ N}$
 $T_{ssl}^{AB} = 122592 \text{ N}$
 $= 17850 \text{ lbf}$
 $= 27560 \text{ lbf}$
 $SFC_{ssl} = 1.86 \cdot 10^{-5} \text{ (kg/s)/N}$
 $SFC_{ssl}^{AB} = 5.83 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.66 \text{ (lb/h)/lbf}$
 $= 2.06 \text{ (lb/h)/lbf}$
 $\dot{w}_{ssl} = 110.2 \text{ kg/s} = 242.9 \text{ lb/s}$
 $BPR = 0.57$
 $OPR = 23$
 $FPR =$
 $TET = 1600 \text{ }^{\circ}\text{K}$

Cruise:

 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$
AL-31MF

Manufacturer: Saturn

Application: Su-32FN (Su-27IB/Su-34) 'Flanker-C'

Composition: 4 / - / 9 / 1 / - / 2

Nb of shafts = 2

 $D_{fan} = \text{m} = \text{in}$
 $D = 1.278 \text{ m}$
 $L = 4.953 \text{ m}$
 $W_{eng} = 1520 \text{ kg} = 3351 \text{ lb}$
 $= 50.3 \text{ in}$
 $= 195 \text{ in}$

Static Sea Level:

 $T_{ssl} = 79400 \text{ N}$
 $T_{ssl}^{AB} = 130421 \text{ N}$
 $= 17850 \text{ lbf}$
 $= 29320 \text{ lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$
 $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 110.2 \text{ kg/s} = 242.9 \text{ lb/s}$
 $BPR = 0.57$
 $OPR =$
 $FPR =$
 $TET = \text{ }^{\circ}\text{K}$

Cruise:

 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$
AL-35F

Manufacturer: Saturn

Application: Su-32FN (Su-27IB/Su-34) 'Flanker-C', Su-35 (Su-27M) 'Flanker-E'

Composition: 4 / - / 9 / 1 / - / 2

Nb of shafts = 2

 $D_{fan} = \text{m} = \text{in}$
 $D = \text{m}$
 $L = \text{m}$
 $W_{eng} = \text{kg} = \text{lb}$
 $= \text{in}$
 $= \text{in}$

Static Sea Level:

 $T_{ssl} = \text{N}$
 $T_{ssl}^{AB} = 133001 \text{ N}$
 $= \text{lbf}$
 $= 29900 \text{ lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$
 $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$
 $OPR =$
 $FPR =$
 $TET = \text{ }^{\circ}\text{K}$

Cruise:

 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

AL-37FU

Manufacturer: Saturn

Application: Su-37, S-37 'Berkut'

Composition: 4 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 137249 N$

$= lbf$ $= 30855 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 119.7 kg/s = 263.9 lb/s$

BPR = 0.6 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AL-5

Manufacturer: Saturn

Application: Tu-110, Su-17 'Fitter-B', Il-46/-46S, I-350, Il-30, La-190, Tu-86, Yak-1000 (not produced)

Composition: 2 / 2B / 6 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 53934 N$ $T_{ssl}^{AB} = N$

$= 12125 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 1 OPR = 10

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AL-7

Manufacturer: Saturn

Application: Il-54 'Blowlamp', Su-7A 'Fitter', Tu-98 'Backfin'

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 63743 N$ $T_{ssl}^{AB} = N$

$= 14330 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 113.9 kg/s = 251.1 lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AL-7F

Manufacturer: Saturn

Application: Su-7B 'Fitter-A', Su-9 'Fishpot-B'

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 63743 \text{ N}$ $T_{ssl}^{AB} = 88261 \text{ N}$

$= 14330 \text{ lbf}$ $= 19842 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AL-7F-1

Manufacturer: Saturn

Application: Su-7BMK 'Fitter-A', Su-11 'Fishpot-C', Su-17 'Fitter-B'

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 68645 \text{ N}$ $T_{ssl}^{AB} = 98065 \text{ N}$

$= 15432 \text{ lbf}$ $= 22046 \text{ lbf}$

$SFC_{ssl} = 2.78 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.53 \cdot 10^{-5} (kg/s)/N$
 $= 0.98 (lb/h)/lbf$ $= 2.3 (lb/h)/lbf$

$\dot{w}_{ssl} = 113.4 \text{ kg/s} = 250 \text{ lb/s}$

BPR = OPR = 9.1

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AL-7F-2

Manufacturer: Saturn

Application: Su-11 'Fishpot-C'

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 68645 \text{ N}$ $T_{ssl}^{AB} = N$

$= 15432 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AL-7PB**Manufacturer:** Saturn**Application:** Be-10 'Mallow'**Composition:** - / - / 9 / 2 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 68645 \text{ N}$ $T_{ssl}^{AB} = N$ $= 15432 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **ALF301****Manufacturer:** Avco Lycoming**Application:** Technology demonstrator**Composition:** 1 / - / 5 + 1C / 2 / - / 2 $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 12144 \text{ N}$ $T_{ssl}^{AB} = N$ $= 2730 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.25 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= 0.44 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = 45.4 \text{ kg/s} = 100.1 \text{ lb/s}$ $BPR = 5.6$ $OPR = 9$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **ALF501****Manufacturer:** Avco Lycoming**Application:** Technology demonstrator**Composition:** 1 / - / 7 + 1C / 2 / - / 2 $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 25800 \text{ N}$ $T_{ssl}^{AB} = N$ $= 5800 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.13 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= 0.4 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = 100.2 \text{ kg/s} = 220.9 \text{ lb/s}$ $BPR = 6$ $OPR = 9.3$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

ALF502L

Manufacturer: Avco Lycoming

Application: Challenger 600

Composition: 1 / 2B / 7 + 1C / 2 / - / 2

$D_{fan} = 1.059 \text{ m} = 41.7 \text{ in}$ $D = 1.27 \text{ m}$

$W_{eng} = 595 \text{ kg} = 1312 \text{ lb}$ $= 50 \text{ in}$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.21 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.43 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 116.1 \text{ kg/s} = 256 \text{ lb/s}$

$BPR = 5.2$ $OPR = 13.6$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.666 \text{ m}$

$= 65.6 \text{ in}$

Cruise:

$T_{cr} = 9564 \text{ N}$

$= 2150 \text{ lbf}$

$SFC_{cr} = 2.07 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.73 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.75, h_{cr} = 9144 \text{ m}$

ALF502L-2

Manufacturer: Avco Lycoming

Application: Challenger 600

Composition: 1 / 2B / 7 + 1C / 2 / - / 2

$D_{fan} = \text{m} = \text{in}$ $D = 1.27 \text{ m}$

$W_{eng} = 595 \text{ kg} = 1312 \text{ lb}$ $= 50 \text{ in}$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.21 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.43 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 5$ $OPR = 13.6$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.666 \text{ m}$

$= 65.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

ALF502L-2A

Manufacturer: Avco Lycoming

Application: Challenger 600

Composition: 1 / 2B / 7 + 1C / 2 / - / 2

$D_{fan} = \text{m} = \text{in}$ $D = 1.27 \text{ m}$

$W_{eng} = 595 \text{ kg} = 1312 \text{ lb}$ $= 50 \text{ in}$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.17 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.41 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 5$ $OPR = 13.8$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.666 \text{ m}$

$= 65.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

ALF502L-2C

Manufacturer: Avco Lycoming

Application: Challenger 600

Composition: 1 / 2B / 7 + 1C / 2 / - / 2

$D_{fan} = m = in$ $D = 1.27 m$

$W_{eng} = 595 kg = 1312 lb$ $= 50 in$

Static Sea Level:

$T_{ssl} = 33362 N$ $T_{ssl}^{AB} = N$
 $= 7500 lbf$ $= lbf$

$SFC_{ssl} = 1.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.41 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 5 OPR = 13.8

FPR = TET = °K

Nb of shafts = 2

$L = 1.666 m$

$= 65.6 in$

Cruise:

$T_{cr} = N$
 $= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

ALF502L-3

Manufacturer: Avco Lycoming

Application: Challenger 600

Composition: 1 / 2B / 7 + 1C / 2 / - / 2

$D_{fan} = m = in$ $D = 1.27 m$

$W_{eng} = 595 kg = 1312 lb$ $= 50 in$

Static Sea Level:

$T_{ssl} = 34696 N$ $T_{ssl}^{AB} = N$
 $= 7800 lbf$ $= lbf$

$SFC_{ssl} = 1.18 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.42 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 5 OPR = 13.8

FPR = TET = °K

Nb of shafts = 2

$L = 1.666 m$

$= 65.6 in$

Cruise:

$T_{cr} = N$
 $= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

ALF502R-3

Manufacturer: Avco Lycoming

Application: BAe 146-100

Composition: 1 / 1B / 7 + 1C / 2 / - / 2

$D_{fan} = m = in$ $D = 1.27 m$

$W_{eng} = 606 kg = 1336 lb$ $= 50 in$

Static Sea Level:

$T_{ssl} = 29803 N$ $T_{ssl}^{AB} = N$
 $= 6700 lbf$ $= lbf$

$SFC_{ssl} = 1.16 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.41 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 5.71 OPR = 11.6

FPR = TET = °K

Nb of shafts = 2

$L = 1.621 m$

$= 63.8 in$

Cruise:

$T_{cr} = N$
 $= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

ALF502R-3A

Manufacturer: Avco Lycoming

Application: BAe 146-100

Composition: 1 / 2B / 7 + 1C / 2 / - / 2

$D_{fan} = m = in$ $D = 1.27 m$

$W_{eng} = 606 kg = 1336 lb$ $= 50 in$

Static Sea Level:

$T_{ssl} = 31004 N$ $T_{ssl}^{AB} = N$

$= 6970 lbf$ $= lbf$

$SFC_{ssl} = 1.16 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.41 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 5.71 OPR = 11.6

FPR = TET = °K

Nb of shafts = 2

$L = 1.621 m$

$= 63.8 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

ALF502R-5

Manufacturer: Avco Lycoming

Application: BAe 146-100/-200/-200ER/-300

Composition: 1 / 2B / 7 + 1C / 2 / - / 2

$D_{fan} = 1.272 m = 50.1 in$ $D = 1.27 m$

$W_{eng} = 606 kg = 1336 lb$ $= 50 in$

Static Sea Level:

$T_{ssl} = 31004 N$ $T_{ssl}^{AB} = N$

$= 6970 lbf$ $= lbf$

$SFC_{ssl} = 1.16 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.41 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 5.6 OPR = 12.2

FPR = TET = °K

Year: 1982

Nb of shafts = 2

$L = 1.621 m$

$= 63.8 in$

Cruise:

$T_{cr} = 10008 N$

$= 2250 lbf$

$SFC_{cr} = 2.04 \cdot 10^{-5} (kg/s)/N$

$= 0.72 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.7, h_{cr} = 7620 m$

ALF502R-6

Manufacturer: Avco Lycoming

Application: BAe 146-200/-200ER/-300

Composition: 1 / 2B / 7 + 1C / 2 / - / 2

$D_{fan} = m = in$ $D = 1.27 m$

$W_{eng} = 624 kg = 1376 lb$ $= 50 in$

Static Sea Level:

$T_{ssl} = 33362 N$ $T_{ssl}^{AB} = N$

$= 7500 lbf$ $= lbf$

$SFC_{ssl} = 1.18 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.42 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 87.1 kg/s = 192 lb/s$

BPR = 5.6 OPR = 13.8

FPR = TET = °K

Nb of shafts = 2

$L = 1.666 m$

$= 65.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

AM-3A**Manufacturer:** Mikulin**Application:** Tu-16 'Badger-A'**Composition:** - / - / 8 / 2 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 85806 \text{ N}$ $T_{ssl}^{AB} = N$ $= 19290 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = 160.6 \text{ kg/s} = 354.1 \text{ lb/s}$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **AM-3D****Manufacturer:** Mikulin**Application:** M-4 'Bison-A'**Composition:** - / - / 8 / 2 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 85316 \text{ N}$ $T_{ssl}^{AB} = N$ $= 19180 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **AM-3M-500****Manufacturer:** Mikulin**Application:** Tu-16 'Badger-A'**Composition:** - / - / 8 / 2 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 93145 \text{ N}$ $T_{ssl}^{AB} = N$ $= 20940 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

AM-5A

Manufacturer: Mikulin

Application: Yak-25 'Flashlight-A', Yak-120, Yak-125

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 21574 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 4850 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

$BPR =$

$OPR =$

$OPR_{cr} =$

$FPR =$

$TET = ^\circ K$

$M_{cr} = , h_{cr} = m$

AM-5B

Manufacturer: Mikulin

Application: Yak-25 'Flashlight-A'

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 25488 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 5730 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

$BPR =$

$OPR =$

$OPR_{cr} =$

$FPR =$

$TET = ^\circ K$

$M_{cr} = , h_{cr} = m$

AM-5F

Manufacturer: Mikulin

Application: MiG-19 'Farmer', Il-40 'Brawny' (not produced)

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 26689 N$

$T_{ssl}^{AB} = 29812 N$

Cruise:

$T_{cr} = N$

$= 6000 lbf$

$= 6702 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

$BPR =$

$OPR =$

$OPR_{cr} =$

$FPR =$

$TET = ^\circ K$

$M_{cr} = , h_{cr} = m$

Arbizon 3

Manufacturer: Turboméca

Year: 1970

Application:

Composition: / / / /

$D_{fan} = m = 0 \text{ in}$ $D = m$

$W_{eng} = 115 \text{ kg} = 254 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 3924 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 882 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 6 \text{ kg/s} = 13.2 \text{ lb/s}$

BPR = 0 OPR = 5.5

FPR = TET = °K

Nb of shafts =

$L = 1.51 \text{ m}$

$= 59.4 \text{ in}$

Cruise:

$T_{cr} = 1305 \text{ N}$

$= 293 \text{ lbf}$

$SFC_{cr} = 3.23 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 1.14 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 11000 \text{ m}$

Arbizon 3B2

Manufacturer: Turboméca

Application: Otomat

Composition: - / - / 1 + 1C / 1 / - / -

$D_{fan} = m = \text{in}$ $D = m$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 4035 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 907 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 5.9

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =, h_{cr} = m$

Arbizon 3D

Manufacturer: Turboméca

Application: Milas

Composition: - / - / 1 + 1C / 1 / - / -

$D_{fan} = m = \text{in}$ $D = m$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 4164 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 936 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 5.9

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =, h_{cr} = m$

AS907**Manufacturer:** ASE : AlliedSignal Engines**Application:** Challenger 300**Composition:** 1 / 4B / 1C / 2 / - / 3 $D_{fan} = 0.869 \text{ m} = 34.2 \text{ in}$ $D = 1.176 \text{ m}$ $W_{eng} = 619 \text{ kg} = 1365 \text{ lb}$ $= 46.3 \text{ in}$ **Static Sea Level:** $T_{ssl} = 28913 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 6500 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = 1.19 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$ $= 0.42 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $\text{BPR} = 4.5$ $\text{OPR} = 21$ $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 2.347 \text{ m}$ $= 92.4 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $\text{OPR}_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **AS977-1A****Manufacturer:** ASE : AlliedSignal Engines**Application:** RJX-70/-85/-100/-115, SL-100 (not produced)**Composition:** 1 / 4B / 1C / 2 / - / 3 $D_{fan} = 0.869 \text{ m} = 34.2 \text{ in}$ $D = 1.267 \text{ m}$ $W_{eng} = 619 \text{ kg} = 1365 \text{ lb}$ $= 49.9 \text{ in}$ **Static Sea Level:** $T_{ssl} = 31582 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 7100 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = 1.18 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$ $= 0.42 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $\text{BPR} = 4.5$ $\text{OPR} = 23$ $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 2.347 \text{ m}$ $= 92.4 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $\text{OPR}_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **Astafan 2****Manufacturer:** Turboméca**Application:****Composition:** 1 / - / 2 + 1C / 3 / - / - $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 7495 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 1685 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = 1.08 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$ $= 0.38 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $\text{BPR} = 1$ $\text{OPR} = 8.5$ $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$ **Nb of shafts** = 1 $L = \text{m}$ $= \text{in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $\text{OPR}_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$

Astafan 3

Manufacturer: Turboméca

Application:

Composition: 1 / - / 2 + 1C / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8452 N$ $T_{ssl}^{AB} = N$

$= 1900 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Astafan 4

Manufacturer: Turboméca

Application:

Composition: 1 / - / 2 + 1C / 4 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 10738 N$ $T_{ssl}^{AB} = N$

$= 2414 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar

Manufacturer: SNECMA

Application: Prototype

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.2

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 08C**Manufacturer:** SNECMA**Application:** Super Etendard IVM/-P**Composition:** - / - / 9 / 2 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 40479 N$ $T_{ssl}^{AB} = 49041 N$
 $= 9100 lbf$ $= 11025 lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$ **Atar 08C-1****Manufacturer:** SNECMA**Application:** Super Etendard**Composition:** - / - / 9 / 2 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 43148 N$ $T_{ssl}^{AB} = N$
 $= 9700 lbf$ $= lbf$ $SFC_{ssl} = 2.75 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.97 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = 68 kg/s = 149.9 lb/s$

BPR = OPR = 5.8

FPR = TET = °K

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$ **Atar 08K-50****Manufacturer:** SNECMA**Application:** Super Etendard**Composition:** - / - / 9 / 2 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 49175 N$ $T_{ssl}^{AB} = 70593 N$
 $= 11055 lbf$ $= 15870 lbf$ $SFC_{ssl} = 2.75 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.09 \cdot 10^{-5} (kg/s)/N$
 $= 0.97 (lb/h)/lbf$ $= 2.15 (lb/h)/lbf$ $\dot{w}_{ssl} = 72.1 kg/s = 159 lb/s$

BPR = OPR = 6.2

FPR = TET = °K

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$

Atar 09B

Manufacturer: SNECMA

Application: Mirage IIIB1/-B2RV/-BSV/-C/-CJ/-CS/-CZ/-S, Super Mystère B4 prototypes

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 40923 N$ $T_{ssl}^{AB} = 58841 N$

$= 9200 lbf$ $= 13228 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 09B-3

Manufacturer: SNECMA

Application: Mirage IIIBJ/-CJ/-CS/-CZ

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 40923 N$ $T_{ssl}^{AB} = 58841 N$

$= 9200 lbf$ $= 13228 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 09C

Manufacturer: SNECMA

Application: Mirage IIIE/-EX/-O(A)/-O(F), Cheetah C/D/E/R, Mirage IV prototype, Mirage IIIM (not produced)

Composition: - / - / 9 / 2 / - / -

$D_{fan} = 0.786 m = 30.9 in$ $D = 1.021 m$

$W_{eng} = 1456 kg = 3210 lb$ $= 40.2 in$

Static Sea Level:

$T_{ssl} = 41947 N$ $T_{ssl}^{AB} = 60802 N$

$= 9430 lbf$ $= 13669 lbf$

$SFC_{ssl} = 2.86 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.75 \cdot 10^{-5} (kg/s)/N$

$= 1.01 (lb/h)/lbf$ $= 2.03 (lb/h)/lbf$

$\dot{w}_{ssl} = 68 kg/s = 149.9 lb/s$

BPR = OPR = 5.7

FPR = TET = °K

Nb of shafts = 1

$L = 5.944 m$

$= 234 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 09C-3

Manufacturer: SNECMA

Application: Mirage IIIBE/-BBR/-E/-EZ/-R/-RD/-RS, Mirage 5SDD

Composition: - / - / 9 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 41947 \text{ N}$ $T_{ssl}^{AB} = 60802 \text{ N}$
 $= 9430 \text{ lbf}$ $= 13669 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 09C-5

Manufacturer: SNECMA

Application: Mirage IIID, Mirage 5/5D/5R

Composition: - / - / 9 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 41947 \text{ N}$ $T_{ssl}^{AB} = 60802 \text{ N}$
 $= 9430 \text{ lbf}$ $= 13669 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 09K-10

Manufacturer: SNECMA

Year: 1996

Application: Mirage IVA/-P/-R, Mirage G4, Mirage G8

Composition: - / - / 9 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 65833 \text{ N}$
 $= lbf$ $= 14800 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 09K-50**Manufacturer:** SNECMA**Year:** 1973**Application:** Mirage 5S (Milan), Mirage 50, Mirage IVA/-P/-R, Mirage F1C, Mirage IIING (not produced)**Composition:** - / - / 9 / 2 / - / - $D_{fan} = 0.786 \text{ m} = 30.9 \text{ in}$ $D = 1.021 \text{ m}$ $W_{eng} = 1582 \text{ kg} = 3488 \text{ lb}$ $= 40.2 \text{ in}$

Nb of shafts = 1

 $L = 6.589 \text{ m}$ $= 259.4 \text{ in}$ **Static Sea Level:** $T_{ssl} = 49175 \text{ N}$ $T_{ssl}^{AB} = 70606 \text{ N}$ $= 11055 \text{ lbf}$ $= 15873 \text{ lbf}$ $SFC_{ssl} = 2.78 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5.64 \cdot 10^{-5} \text{ (kg/s)/N}$ $= 0.98 \text{ (lb/h)/lbf}$ $= 1.99 \text{ (lb/h)/lbf}$ $\dot{w}_{ssl} = 72.6 \text{ kg/s} = 160.1 \text{ lb/s}$

BPR = 0

OPR = 6.2

FPR =

TET = 1208 °K

Cruise: $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = 2, h_{cr} = 11000 \text{ m}$ **Atar 101A-0****Manufacturer:** SNECMA**Year:** 1946**Application:****Composition:** - / - / 7 / 1 / - / - $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $W_{eng} = 880 \text{ kg} = 1940 \text{ lb}$ $= \text{in}$

Nb of shafts = 1

 $L = \text{m}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 21574 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 4850 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 3.25 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$ $= 1.15 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = 45.4 \text{ kg/s} = 100.1 \text{ lb/s}$

BPR =

OPR = 4.2

FPR =

TET = 1083 °K

Cruise: $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$ **Atar 101B****Manufacturer:** SNECMA**Application:** Vautour I, Vautour IIB prototype**Composition:** - / - / 7 / 1 / - / - $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Nb of shafts = 1

 $L = \text{m}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 23535 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 5291 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Cruise: $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$

Atar 101C**Manufacturer:** SNECMA**Application:** Gerfaut IA, Mystère IIC prototypes, Vautour IIB prototype, Baroudeur prototype**Composition:** - / - / 7 / 1 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$ $D = m$ $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:** $T_{ssl} = 22908 \text{ N}$ $T_{ssl}^{AB} = N$ $= 5150 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise: $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$ **Atar 101D****Manufacturer:** SNECMA**Application:** Vautour IA, Vautour IIB prototype**Composition:** - / - / 7 / 1 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$ $D = m$ $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:** $T_{ssl} = 29425 \text{ N}$ $T_{ssl}^{AB} = N$ $= 6615 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 3.09 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= 1.09 (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$ $\dot{w}_{ssl} = 51.7 \text{ kg/s} = 114 \text{ lb/s}$

BPR = OPR = 4.5

FPR = TET = °K

Cruise: $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$ **Atar 101D-1****Manufacturer:** SNECMA**Application:** Gerfaut IB**Composition:** - / - / 7 / 1 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$ $D = m$ $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:** $T_{ssl} = 29425 \text{ N}$ $T_{ssl}^{AB} = N$ $= 6615 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise: $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$

Atar 101D-2

Manufacturer: SNECMA

Application: Gerfaut IB, Mystère IIC

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 29425 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6615 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 101D-3

Manufacturer: SNECMA

Application: Mystère IIC

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 29425 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6615 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 101E

Manufacturer: SNECMA

Application: Vautour IIA/-B/-N

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$ $T_{ssl}^{AB} = N$

$= 7500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 101E-3

Manufacturer: SNECMA

Application: Griffon II, Vautour IIA/-B/-N, Etendard IV (Mystère XXIV)

Composition: - / - / 8 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 34322 \text{ N}$ $T_{ssl}^{AB} = N$

$= 7716 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 101E-4

Manufacturer: SNECMA

Application: Baroudeur prototypes

Composition: - / - / 8 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 36208 \text{ N}$ $T_{ssl}^{AB} = N$

$= 8140 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 101E-5

Manufacturer: SNECMA

Application: Vautour IIN

Composition: - / - / 8 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 36208 \text{ N}$ $T_{ssl}^{AB} = N$

$= 8140 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 101F

Manufacturer: SNECMA

Application: Gerfaut II, Griffon I, Mystère IIC prototypes, Mystère IVB prototype

Composition: - / - / 7 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = N$

$T_{ssl}^{AB} = 37276 N$

Cruise:

$T_{cr} = N$

$= lbf$

$= 8380 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Atar 101G

Manufacturer: SNECMA

Application: Super Mystère B2 prototypes, Mirage IIIA, Mirage IIIC prototypes

Composition: - / - / 8 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 32917 N$

$T_{ssl}^{AB} = 43148 N$

Cruise:

$T_{cr} = N$

$= 7400 lbf$

$= 9700 lbf$

$= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = 5.5 \cdot 10^{-5} (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$

$= 1.94 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 59 kg/s = 130.1 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR = 4.8

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Atar 101G-2

Manufacturer: SNECMA

Application: Mystère IVB prototypes, Super Mystère B2, Mirage IIIA

Composition: - / - / 8 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 32917 N$

$T_{ssl}^{AB} = 44037 N$

Cruise:

$T_{cr} = N$

$= 7400 lbf$

$= 9900 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Atar 101G-2-1

Manufacturer: SNECMA

Application: Gerfaut II, Griffon I

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32917 \text{ N}$ $T_{ssl}^{AB} = 44037 \text{ N}$

$= 7400 \text{ lbf}$ $= 9900 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Atar 101G-3

Manufacturer: SNECMA

Application: Super Mystère B2

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32917 \text{ N}$ $T_{ssl}^{AB} = 44037 \text{ N}$

$= 7400 \text{ lbf}$ $= 9900 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

ATF3

Manufacturer: ASE : AlliedSignal Engines

Application: Sabreliner 60, HFB 330

Composition: 1 / 5 / 1C / 1 / 3 / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 18015 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4050 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 1.25 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.44 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 63.5 \text{ kg/s} = 140 \text{ lb/s}$

BPR = 3

OPR = 17

FPR =

TET = °K

Nb of shafts = 3

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

ATF3-6

Manufacturer: ASE : AlliedSignal Engines

Year: 1981

Application: Guardian

Composition: / / / / /

$D_{fan} = 0.767 \text{ m} = 30.2 \text{ in}$ $D = \text{m}$

$W_{eng} = 510 \text{ kg} = 1124 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 23130 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 5200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.47 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.52 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 73.5 \text{ kg/s} = 162 \text{ lb/s}$

BPR = 2.9 OPR = 21

FPR = 1.6 TET = 1449 °K

Nb of shafts =

$L = 2.304 \text{ m}$

$= 90.7 \text{ in}$

Cruise:

$T_{cr} = 4890 \text{ N}$

$= 1099 \text{ lbf}$

$SFC_{cr} = 2.29 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.81 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 26.7

$M_{cr} = 0.8, h_{cr} = 12200 \text{ m}$

ATF3-6A

Manufacturer: ASE : AlliedSignal Engines

Application: Falcon 200, UC-35A (candidate engine)

Composition: 1 / 5 / 1C / 1 / 3 / 2

$D_{fan} = \text{m} = \text{in}$ $D = 0.853 \text{ m}$

$W_{eng} = 510 \text{ kg} = 1124 \text{ lb}$ $= 33.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 23131 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 5200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 73.5 \text{ kg/s} = 162 \text{ lb/s}$

BPR = 2.8 OPR = 21.3

FPR = TET = °K

Nb of shafts = 3

$L = 2.591 \text{ m}$

$= 102 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Aubisque 1A

Manufacturer: Turboméca

Application: Saab 105

Composition: 1G / - / 1 + 1C / 2 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 7273 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 1635 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 21.8 \text{ kg/s} = 48.1 \text{ lb/s}$

BPR = 2 OPR = 6.9

FPR = 1.5 TET = °K

Nb of shafts = 1

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Avon RA.14 Mk.201
Manufacturer: Rolls-Royce

Application: Valiant B.1

Composition: - / - / 15 / 2 / - / -

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$
Static Sea Level:
 $T_{ssl} = 42258 \text{ N}$
 $T_{ssl}^{AB} = N$
 $= 9500 \text{ lbf}$
 $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$

Nb of shafts = 1

 $L = m$
 $= in$
Cruise:
 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
Avon RA.2
Manufacturer: Rolls-Royce

Application: Canberra B.1 prototype, Sperrin prototype

Composition: - / - / 12 / 1 / - / -

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$
Static Sea Level:
 $T_{ssl} = 26689 \text{ N}$
 $T_{ssl}^{AB} = N$
 $= 6000 \text{ lbf}$
 $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$

Nb of shafts = 1

 $L = m$
 $= in$
Cruise:
 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
Avon RA.24R Mk.200R
Manufacturer: Rolls-Royce

Application: Lightning F.1/F.1A

Composition: - / - / 15 / 2 / - / -

 $D_{fan} = m = in$
 $D = 1.067 \text{ m}$
 $W_{eng} = kg = lb$
 $= 42 \text{ in}$
Static Sea Level:
 $T_{ssl} = 50042 \text{ N}$
 $T_{ssl}^{AB} = 63921 \text{ N}$
 $= 11250 \text{ lbf}$
 $= 14370 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$

Nb of shafts = 1

 $L = 3.223 \text{ m}$
 $= 126.9 \text{ in}$
Cruise:
 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Avon RA.24R Mk.202

Manufacturer: Rolls-Royce

Application: Scimitar F.1

Composition: - / - / 15 / 2 / - / -

$D_{fan} = m = in$ $D = 1.067 m$

$W_{eng} = kg = lb$ $= 42 in$

Static Sea Level:

$T_{ssl} = 50042 N$ $T_{ssl}^{AB} = 63921 N$

$= 11250 lbf$ $= 14370 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 7.8

FPR = TET = °K

Nb of shafts = 1

$L = 3.223 m$

$= 126.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.24R Mk.206

Manufacturer: Rolls-Royce

Application: Canberra PR.9/T.17/TT.18/T.19/T.22

Composition: - / - / 15 / 2 / - / -

$D_{fan} = m = in$ $D = 1.067 m$

$W_{eng} = kg = lb$ $= 42 in$

Static Sea Level:

$T_{ssl} = 50042 N$ $T_{ssl}^{AB} = 63921 N$

$= 11250 lbf$ $= 14370 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 8.2

FPR = TET = °K

Nb of shafts = 1

$L = 3.223 m$

$= 126.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.24R Mk.208

Manufacturer: Rolls-Royce

Application: Sea Vixen F(AW).1/F(AW).2

Composition: - / - / 15 / 2 / - / -

$D_{fan} = m = in$ $D = 1.067 m$

$W_{eng} = kg = lb$ $= 42 in$

Static Sea Level:

$T_{ssl} = 50042 N$ $T_{ssl}^{AB} = 63921 N$

$= 11250 lbf$ $= 14370 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 7.8

FPR = TET = °K

Nb of shafts = 1

$L = 3.223 m$

$= 126.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.24R Mk.210R

Manufacturer: Rolls-Royce

Application: Lightning F.2/T.4/F.52/T.54

Composition: - / - / 15 / 2 / - / -

$D_{fan} = m = in$ $D = 1.067 m$

$W_{eng} = kg = lb$ $= 42 in$

Static Sea Level:

$T_{ssl} = 50042 N$ $T_{ssl}^{AB} = 63921 N$
 $= 11250 lbf$ $= 14370 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 8.2

FPR = TET = °K

Nb of shafts = 1

$L = 3.223 m$

$= 126.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.24R Mk.211R

Manufacturer: Rolls-Royce

Application: Lightning F.2A

Composition: - / - / 15 / 2 / - / -

$D_{fan} = m = in$ $D = 1.067 m$

$W_{eng} = kg = lb$ $= 42 in$

Static Sea Level:

$T_{ssl} = 50042 N$ $T_{ssl}^{AB} = 63921 N$
 $= 11250 lbf$ $= 14370 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 8.2

FPR = TET = °K

Nb of shafts = 1

$L = 3.223 m$

$= 126.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.25 Mk.502

Manufacturer: Rolls-Royce

Application: Comet 2

Composition: - / - / ?? / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28913 N$ $T_{ssl}^{AB} = N$
 $= 6500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.25 Mk.503

Manufacturer: Rolls-Royce

Application: Comet 2

Composition: - / - / ?? / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28913 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.25 Mk.504

Manufacturer: Rolls-Royce

Application: Comet 2E

Composition: - / - / ?? / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28913 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.26 Mk.522

Manufacturer: Rolls-Royce

Application: Comet 4

Composition: - / - / ?? / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$ $T_{ssl}^{AB} = N$

$= 10000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.28 Mk.203

Manufacturer: Rolls-Royce

Application: Hunter F.6/FGA.9/FR.10/GR.11/PR.11/T.53/F.56/F.58/T.66/T.68

Composition: - / - / 15 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = 1.054 \text{ m}$

$L = 3.124 \text{ m}$

$W_{eng} = kg = lb$

$= 41.5 \text{ in}$

$= 123 \text{ in}$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 10000 \text{ lbf}$

$= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR = 7.8

OPR_{cr}=

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Avon RA.28 Mk.204

Manufacturer: Rolls-Royce

Application: Valiant B.1/B(K).1/B(PR).1/B.PR(K).1

Composition: - / - / 15 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = 1.054 \text{ m}$

$L = 3.124 \text{ m}$

$W_{eng} = kg = lb$

$= 41.5 \text{ in}$

$= 123 \text{ in}$

Static Sea Level:

$T_{ssl} = 44704 \text{ N}$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 10050 \text{ lbf}$

$= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR = 7.8

OPR_{cr}=

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Avon RA.28 Mk.205

Manufacturer: Rolls-Royce

Application: Valiant B.1/B(K).1/B(PR).1/B.PR(K).1, Valiant B.2 (not produced)

Composition: - / - / 15 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = 1.054 \text{ m}$

$L = 3.124 \text{ m}$

$W_{eng} = kg = lb$

$= 41.5 \text{ in}$

$= 123 \text{ in}$

Static Sea Level:

$T_{ssl} = 44704 \text{ N}$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 10050 \text{ lbf}$

$= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR = 7.8

OPR_{cr}=

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Avon RA.28 Mk.207

Manufacturer: Rolls-Royce

Application: Hunter F.6A/FGA.9/FR.10/GR.11/PR.11/T.53/F.56/F.58/T.66/T.68

Composition: - / - / 15 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 1.054 m$

$L = 3.124 m$

$W_{eng} = 1301 kg = 2868 lb$ $= 41.5 in$

$= 123 in$

Static Sea Level:

$T_{ssl} = 44704 N$ $T_{ssl}^{AB} = N$

$= 10050 lbf$ $= lbf$

$SFC_{ssl} = 2.49 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.88 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 7.8

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.29 Mk.522

Manufacturer: Rolls-Royce

Application: Caravelle 1

Composition: - / - / ?? / 3 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 46706 N$ $T_{ssl}^{AB} = N$

$= 10500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.29 Mk.523

Manufacturer: Rolls-Royce

Application: Comet 3

Composition: - / - / ?? / 3 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 46706 N$ $T_{ssl}^{AB} = N$

$= 10500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.29/1 Mk.524

Manufacturer: Rolls-Royce

Application: Comet 2E/4

Composition: - / - / 16 / 3 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = 1516 kg = 3342 lb$ $= 39 in$

Static Sea Level:

$T_{ssl} = 45594 N$ $T_{ssl}^{AB} = N$
 $= 10250 lbf$ $= lbf$

$SFC_{ssl} = 2.23 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.79 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 77.1 kg/s = 170 lb/s$

BPR = OPR = 8.8

FPR = TET = °K

Nb of shafts = 1

$L = 3.2 m$

$= 126 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.29/1 Mk.524B

Manufacturer: Rolls-Royce

Year: 1957

Application:

Composition: / / / /

$D_{fan} = 0.991 m = 39 in$ $D = m$

$W_{eng} = 1516 kg = 3342 lb$ $= in$

Static Sea Level:

$T_{ssl} = 46696 N$ $T_{ssl}^{AB} = N$
 $= 10498 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 83 kg/s = 183 lb/s$

BPR = 0 OPR = 8.7

FPR = TET = 1100 °K

Nb of shafts =

$L = 3.2 m$

$= 126 in$

Cruise:

$T_{cr} = N$

$= 0 lbf$

$SFC_{cr} = (kg/s)/N$

$= 0 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 11000 m$

Avon RA.29/1 Mk.525B

Manufacturer: Rolls-Royce

Application: Comet 4B/4C, Comet C.4

Composition: - / - / 16 / 3 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = kg = lb$ $= 39 in$

Static Sea Level:

$T_{ssl} = 45594 N$ $T_{ssl}^{AB} = N$
 $= 10250 lbf$ $= lbf$

$SFC_{ssl} = 2.23 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.79 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 77.1 kg/s = 170 lb/s$

BPR = OPR = 8.8

FPR = TET = °K

Nb of shafts = 1

$L = 3.2 m$

$= 126 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.29/1 Mk.526

Manufacturer: Rolls-Royce

Application: Caravelle 1A

Composition: - / - / 16 / 3 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = 1516 kg = 3342 lb$ $= 39 in$

Static Sea Level:

$T_{ssl} = 45594 N$ $T_{ssl}^{AB} = N$
 $= 10250 lbf$ $= lbf$
 $SFC_{ssl} = 2.23 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.79 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 77.1 kg/s = 170 lb/s$
 $BPR =$ $OPR = 8.8$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 3.2 m$

$= 126 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Avon RA.29/3 Mk.527B

Manufacturer: Rolls-Royce

Application: Caravelle 3

Composition: - / - / 16 / 3 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = 1518 kg = 3347 lb$ $= 39 in$

Static Sea Level:

$T_{ssl} = 50709 N$ $T_{ssl}^{AB} = N$
 $= 11400 lbf$ $= lbf$
 $SFC_{ssl} = 2.42 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.85 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 3.2 m$

$= 126 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Avon RA.29/6 Mk.531B

Manufacturer: Rolls-Royce

Application: Caravelle 6N

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = 1582 kg = 3488 lb$ $= 39 in$

Static Sea Level:

$T_{ssl} = 54268 N$ $T_{ssl}^{AB} = N$
 $= 12200 lbf$ $= lbf$
 $SFC_{ssl} = 2.27 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.8 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 3.404 m$

$= 134 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Avon RA.29/6 Mk.533R

Manufacturer: Rolls-Royce

Application: Caravelle 6R

Composition: / / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = kg = lb$ $= 39 in$

Static Sea Level:

$T_{ssl} = 56047 N$ $T_{ssl}^{AB} = N$

$= 12600 lbf$ $= lbf$

$SFC_{ssl} = 2.22 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.79 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 3.404 m$

$= 134 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.29/6 Mk.535R

Manufacturer: Rolls-Royce

Application: Caravelle 6R

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = kg = lb$ $= 39 in$

Static Sea Level:

$T_{ssl} = 56047 N$ $T_{ssl}^{AB} = N$

$= 12600 lbf$ $= lbf$

$SFC_{ssl} = 2.22 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.79 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 83.9 kg/s = 185 lb/s$

BPR = OPR = 10.3

FPR = TET = °K

Nb of shafts = 1

$L = 3.404 m$

$= 134 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.3 Mk.100

Manufacturer: Rolls-Royce

Application: F.D.2, Valiant prototype, Sperrin prototype

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28913 N$ $T_{ssl}^{AB} = N$

$= 6500 lbf$ $= lbf$

$SFC_{ssl} = 2.5 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.88 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 53.5 kg/s = 117.9 lb/s$

BPR = OPR = 6.2

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.3 Mk.101-2

Manufacturer: Rolls-Royce

Application: Canberra B.1

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26689 N$ $T_{ssl}^{AB} = N$

$= 6000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.3 Mk.101-3

Manufacturer: Rolls-Royce

Application: CF-100 Mk.1, Canberra B.2/T.11

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28913 N$ $T_{ssl}^{AB} = N$

$= 6500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.3 Mk.103

Manufacturer: Rolls-Royce

Application: Canberra B.XX, Hunter prototype

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28913 N$ $T_{ssl}^{AB} = N$

$= 6500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.3 Mk.104

Manufacturer: Rolls-Royce

Application:

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 7500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.3 Mk.107

Manufacturer: Rolls-Royce

Application:

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 7500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.3 Mk.108

Manufacturer: Rolls-Royce

Application: Swift FR.5

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 40479 \text{ N}$
 $= lbf$ $= 9100 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.3 Mk.109

Manufacturer: Rolls-Royce

Application: Canberra B.6/B(I).8/B.9/B.15/B.16

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32917 N$ $T_{ssl}^{AB} = N$

$= 7400 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.4 Mk.107

Manufacturer: Rolls-Royce

Application: Hunter prototype

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33362 N$ $T_{ssl}^{AB} = N$

$= 7500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.7 Mk.113

Manufacturer: Rolls-Royce

Application: Hunter F.1/F.4, Valiant prototype

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33362 N$ $T_{ssl}^{AB} = N$

$= 7500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.7 Mk.114

Manufacturer: Rolls-Royce

Application: Swift FR.5

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 42035 N$

$= lbf$ $= 9450 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.7 Mk.116

Manufacturer: Rolls-Royce

Application: Swift F.7

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 44260 N$

$= lbf$ $= 9950 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.7 Mk.117

Manufacturer: Rolls-Royce

Application: Comet 2R, Comet C.2/T.2

Composition: - / - / ?? / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32694 N$ $T_{ssl}^{AB} = N$

$= 7350 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.7 Mk.122

Manufacturer: Rolls-Royce

Application: Hunter T.7/T.7A/T.7B/T.8/T.8M

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 33028 \text{ N}$

$T_{ssl}^{AB} = N$

$= 7425 \text{ lbf}$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.7 Mk.20

Manufacturer: Rolls-Royce

Application: CA-27 Sabre Mk.31

Composition: - / - / / / - / -

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$

$T_{ssl}^{AB} = N$

$= 7500 \text{ lbf}$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.7 Mk.26

Manufacturer: Rolls-Royce

Application: CA-27 Sabre Mk.32

Composition: - / - / / / - / -

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$

$T_{ssl}^{AB} = N$

$= 7500 \text{ lbf}$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Avon RA.7R Mk.114

Manufacturer: Rolls-Royce

Application: Mystère IVB/-N prototypes, Super Mystère B1, Hunter F.3 (not produced)

Composition: - / - / 12 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 33406 N$ $T_{ssl}^{AB} = 42258 N$

$T_{cr} = N$

$= 7510 lbf$ $= 9500 lbf$

$= lbf$

$SFC_{ssl} = 2.44 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.39 \cdot 10^{-5} (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.86 (lb/h)/lbf$ $= 1.9 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 58.5 kg/s = 129 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR = 7

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

Avon RB.146 Mk.301

Manufacturer: Rolls-Royce

Application: Lightning F.3/F.3A/T.5

Composition: - / - / 16 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 53823 N$ $T_{ssl}^{AB} = 69903 N$

$T_{cr} = N$

$= 12100 lbf$ $= 15715 lbf$

$= lbf$

$SFC_{ssl} = 2.64 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.25 \cdot 10^{-5} (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.93 (lb/h)/lbf$ $= 1.85 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 77.1 kg/s = 170 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR = 8.4

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

Avon RB.146 Mk.302

Manufacturer: Rolls-Royce

Application: Lightning F.6

Composition: - / - / 16 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 56448 N$ $T_{ssl}^{AB} = 72773 N$

$T_{cr} = N$

$= 12690 lbf$ $= 16360 lbf$

$= lbf$

$SFC_{ssl} = 2.41 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.85 (lb/h)/lbf$ $= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 79.4 kg/s = 175 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR = 8.4

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

Avon RB.146 Mk.302C

Manufacturer: Rolls-Royce

Application: Lightning F.53/T.55

Composition: - / - / 16 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 56448 N$ $T_{ssl}^{AB} = 72773 N$

$= 12690 lbf$ $= 16360 lbf$

$SFC_{ssl} = 2.41 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.85 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 79.4 kg/s = 175 lb/s$

BPR = OPR = 8.4

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Bastafan

Manufacturer: Turboméca

Application:

Composition: 1G / - / 2 + 1C / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7851 N$ $T_{ssl}^{AB} = N$

$= 1765 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

BR710

Manufacturer: BMW/Rolls-Royce

Year: 1996

Application: Gulfstream V, Global Express, TU334, ARJ 21, SL-200/-300 (not produced)

Composition: 1 / - / 10 / 2 / - / 2

$D_{fan} = 1.344 m = 52.9 in$ $D = m$

$W_{eng} = 1597 kg = 3521 lb$ $= in$

Static Sea Level:

$T_{ssl} = 66034 N$ $T_{ssl}^{AB} = N$

$= 14845 lbf$ $= lbf$

$SFC_{ssl} = 1.1 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.39 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 201.8 kg/s = 444.9 lb/s$

BPR = 4 OPR = 25.7

FPR = TET = °K

Nb of shafts = 2

$L = 2.21 m$

$= 87 in$

Cruise:

$T_{cr} = 15480 N$

$= 3480 lbf$

$SFC_{cr} = 1.81 \cdot 10^{-5} (kg/s)/N$

$= 0.64 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} = 31

$M_{cr} = 0.8 , h_{cr} = 10668 m$

BR710-48

Manufacturer: BMW/Rolls-Royce

Application: Tu-334-120

Composition: 1 / - / 10 / 2 / - / 2

$D_{fan} = 1.219 \text{ m} = 48 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 71171 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 16000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 4.2$ $\text{OPR} =$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

BR710A1-10

Manufacturer: BMW/Rolls-Royce

Application: G500 (Gulfstream V), G550 (Gulfstream V-SP), C-37A

Composition: 1 / - / 10 / 2 / - / 2

$D_{fan} = 1.219 \text{ m} = 48 \text{ in}$ $D = 1.344 \text{ m}$

$W_{eng} = 1597 \text{ kg} = 3521 \text{ lb}$ $= 52.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 65611 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 14750 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.11 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.39 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 197.3 \text{ kg/s} = 435 \text{ lb/s}$

$\text{BPR} = 4.2$ $\text{OPR} = 25.7$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.21 \text{ m}$

$= 87 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

BR710A2-20

Manufacturer: BMW/Rolls-Royce

Application: Global Express, Global Express XRS, Global 5000

Composition: 1 / - / 10 / 2 / - / 2

$D_{fan} = 1.219 \text{ m} = 48 \text{ in}$ $D = 1.344 \text{ m}$

$W_{eng} = 1597 \text{ kg} = 3521 \text{ lb}$ $= 52.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 65611 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 14750 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.11 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.39 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 197.3 \text{ kg/s} = 435 \text{ lb/s}$

$\text{BPR} = 4.2$ $\text{OPR} = 25.7$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.21 \text{ m}$

$= 87 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

BR710B3-40 Mk.101

Manufacturer: BMW/Rolls-Royce

Application: Nimrod MRA.4

Composition: 1 / - / 10 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 66278 N$ $T_{ssl}^{AB} = N$

$= 14900 lbf$ $= lbf$

$SFC_{ssl} = 1.11 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.39 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 4.2 OPR = 25.5

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

BR710C4-11

Manufacturer: BMW/Rolls-Royce

Application: G500 (Gulfstream V), G550 (Gulfstream V-SP)

Composition: 1 / - / 10 / 2 / - / 2

$D_{fan} = 1.219 m = 48 in$ $D = 1.344 m$

$W_{eng} = 1597 kg = 3521 lb$ $= 52.9 in$

Static Sea Level:

$T_{ssl} = 65611 N$ $T_{ssl}^{AB} = N$

$= 14750 lbf$ $= lbf$

$SFC_{ssl} = 1.11 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.39 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 197.3 kg/s = 435 lb/s$

BPR = 4.2 OPR = 25.7

FPR = TET = °K

Nb of shafts = 2

$L = 2.21 m$

$= 87 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

BR715-55

Manufacturer: BMW/Rolls-Royce

Application: MD95, Tu-354 (Tu-334-200) (proposed)

Composition: 1 / 2B / 10 / 2 / - / 3

$D_{fan} = 1.53 m = 60.2 in$ $D = m$

$W_{eng} = 2062 kg = 4546 lb$ $= in$

Static Sea Level:

$T_{ssl} = 88444 N$ $T_{ssl}^{AB} = N$

$= 19883 lbf$ $= lbf$

$SFC_{ssl} = 1.05 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.37 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 278.5 kg/s = 614 lb/s$

BPR = 4.7 OPR = 32.1

FPR = TET = °K

Year:

Nb of shafts = 2

$L = 2.588 m$

$= 101.9 in$

Cruise:

$T_{cr} = 19483 N$

$= 4380 lbf$

$SFC_{cr} = 1.76 \cdot 10^{-5} (kg/s)/N$

$= 0.62 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 10668 m$

BR715A1-30

Manufacturer: BMW/Rolls-Royce

Application: B717-200

Composition: 1 / 2B / 10 / 2 / - / 3

$D_{fan} = 1.422 \text{ m} = 56 \text{ in}$ $D = 1.529 \text{ m}$

$W_{eng} = 2085 \text{ kg} = 4597 \text{ lb}$ $= 60.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 82292 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 18500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 278.5 \text{ kg/s} = 614 \text{ lb/s}$

BPR = 4.7 OPR = 32.1

FPR = TET = °K

Nb of shafts = 2

$L = 2.362 \text{ m}$

$= 93 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

BR715B1-30

Manufacturer: BMW/Rolls-Royce

Application: B717-200 (option)

Composition: 1 / 2B / 10 / 2 / - / 3

$D_{fan} = 1.422 \text{ m} = 56 \text{ in}$ $D = 1.58 \text{ m}$

$W_{eng} = 2114 \text{ kg} = 4661 \text{ lb}$ $= 62.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 88964 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 20000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.4 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.607 \text{ m}$

$= 142 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

BR715C1-30

Manufacturer: BMW/Rolls-Royce

Application: B717-200 HGW

Composition: 1 / 2B / 10 / 2 / - / 3

$D_{fan} = 1.422 \text{ m} = 56 \text{ in}$ $D = 1.529 \text{ m}$

$W_{eng} = 2085 \text{ kg} = 4597 \text{ lb}$ $= 60.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 93412 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 21000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 312.5 \text{ kg/s} = 688.9 \text{ lb/s}$

BPR = 5 OPR = 32.6

FPR = TET = °K

Nb of shafts = 2

$L = 2.362 \text{ m}$

$= 93 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF34-10A

Manufacturer: GE : General Electric

Application: ARJ21

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.346 \text{ m} = 53 \text{ in}$ $D = \text{m}$

$W_{eng} = 1701 \text{ kg} = 3750 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 80068 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 18000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 2.286 \text{ m}$

$= 90 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF34-10D5

Manufacturer: GE : General Electric

Application: 928-100 (not produced)

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = \text{m} = \text{in}$ $D = 1.448 \text{ m}$

$W_{eng} = 1724 \text{ kg} = 3801 \text{ lb}$ $= 57 \text{ in}$

Static Sea Level:

$T_{ssl} = 77199 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 17355 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.08 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.38 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5

OPR = 29

FPR =

TET = °K

Nb of shafts = 2

$L = 2.286 \text{ m}$

$= 90 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF34-10D6

Manufacturer: GE : General Electric

Application: 928-200 (not produced)

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = \text{m} = \text{in}$ $D = 1.448 \text{ m}$

$W_{eng} = 1724 \text{ kg} = 3801 \text{ lb}$ $= 57 \text{ in}$

Static Sea Level:

$T_{ssl} = 83404 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 18750 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.08 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.38 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5

OPR = 29

FPR =

TET = °K

Nb of shafts = 2

$L = 2.286 \text{ m}$

$= 90 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF34-10E5

Manufacturer: GE : General Electric

Application: ERJ-190/-190AR, ERJ-195/-195AR

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.346 \text{ m} = 53 \text{ in}$ $D = 1.448 \text{ m}$

$W_{eng} = 1724 \text{ kg} = 3801 \text{ lb}$ $= 57 \text{ in}$

Static Sea Level:

$T_{ssl} = 82292 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 18500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.08 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.38 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 2.286 \text{ m}$

$= 90 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF34-1A

Manufacturer: GE : General Electric

Application: Challenger 601-1A

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = 1.118 \text{ m} = 44 \text{ in}$ $D = 1.245 \text{ m}$

$W_{eng} = 737 \text{ kg} = 1625 \text{ lb}$ $= 49 \text{ in}$

Static Sea Level:

$T_{ssl} = 38477 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 8650 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 6.2

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 2.616 \text{ m}$

$= 103 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF34-3A

Manufacturer: GE : General Electric

Year: 1996

Application: Canadair Regional Jet, Canadair Challenger 601-3A

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = 1.118 \text{ m} = 44 \text{ in}$ $D = 1.245 \text{ m}$

$W_{eng} = 737 \text{ kg} = 1625 \text{ lb}$ $= 49 \text{ in}$

Static Sea Level:

$T_{ssl} = 41013 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 9220 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 147 \text{ kg/s} = 324.1 \text{ lb/s}$

BPR = 6.2

OPR = 21

FPR = 1.5

TET = 1477 °K

Nb of shafts = 2

$L = 2.616 \text{ m}$

$= 103 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= 0 \text{ lbf}$

$SFC_{cr} = 1.99 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.7 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.7, h_{cr} = 11280 \text{ m}$

CF34-3A1

Manufacturer: GE : General Electric

Application: Canadair CRJ100/200, Challenger 601

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = 1.118 \text{ m} = 44 \text{ in}$ $D = 1.245 \text{ m}$

$W_{eng} = 751 \text{ kg} = 1656 \text{ lb}$ $= 49 \text{ in}$

Static Sea Level:

$T_{ssl} = 41012 \text{ N}$

$= 9220 \text{ lbf}$

$SFC_{ssl} = 1.01 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 150.6 \text{ kg/s} = 332 \text{ lb/s}$

$BPR = 6.3$

$FPR =$

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$OPR = 21$

$TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.616 \text{ m}$

$= 103 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-3B

Manufacturer: GE : General Electric

Application: Canadair CRJ100/200, Challenger 604, Challenger 800

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = 1.118 \text{ m} = 44 \text{ in}$ $D = 1.245 \text{ m}$

$W_{eng} = 757 \text{ kg} = 1669 \text{ lb}$ $= 49 \text{ in}$

Static Sea Level:

$T_{ssl} = 41012 \text{ N}$

$= 9220 \text{ lbf}$

$SFC_{ssl} = 0.98 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 6.3$

$FPR =$

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$OPR = 21$

$TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.616 \text{ m}$

$= 103 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-3B1

Manufacturer: GE : General Electric

Application: Canadair CRJ100/200/200ER/200LR, Challenger 604, Challenger 800

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = 1.118 \text{ m} = 44 \text{ in}$ $D = 1.245 \text{ m}$

$W_{eng} = 757 \text{ kg} = 1669 \text{ lb}$ $= 49 \text{ in}$

Static Sea Level:

$T_{ssl} = 41012 \text{ N}$

$= 9220 \text{ lbf}$

$SFC_{ssl} = 0.98 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 6.3$

$FPR =$

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$OPR = 21$

$TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.616 \text{ m}$

$= 103 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-8C1

Manufacturer: GE : General Electric

Application: Canadair CRJ700-701/-701ER

Composition: 1 / - / 10 / 2 / - / 4

$D_{fan} = 1.173 \text{ m} = 46.2 \text{ in}$ $D = 1.321 \text{ m}$

$W_{eng} = 1066 \text{ kg} = 2350 \text{ lb}$ $= 52 \text{ in}$

Static Sea Level:

$T_{ssl} = 61341 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 13790 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.05 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.37 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 4.9$ $\text{OPR} = 27$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.251 \text{ m}$

$= 128 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-8C5

Manufacturer: GE : General Electric

Application: Canadair CRJ700-705/-705ER, Canadair CRJ900/900ER

Composition: 1 / - / 10 / 2 / - / 4

$D_{fan} = 1.173 \text{ m} = 46.2 \text{ in}$ $D = 1.321 \text{ m}$

$W_{eng} = 1120 \text{ kg} = 2469 \text{ lb}$ $= 52 \text{ in}$

Static Sea Level:

$T_{ssl} = 64499 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 14500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.11 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.39 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 4.9$ $\text{OPR} =$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.251 \text{ m}$

$= 128 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-8C5B1

Manufacturer: GE : General Electric

Application: Canadair CRJ700-705LR

Composition: 1 / - / 10 / 2 / - / 4

$D_{fan} = 1.173 \text{ m} = 46.2 \text{ in}$ $D = 1.321 \text{ m}$

$W_{eng} = 1120 \text{ kg} = 2469 \text{ lb}$ $= 52 \text{ in}$

Static Sea Level:

$T_{ssl} = 63409 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 14255 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 4.9$ $\text{OPR} =$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.251 \text{ m}$

$= 128 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-8D1

Manufacturer: GE : General Electric

Application: 728-100, 528-100 (not produced)

Composition: 1 / - / 10 / 2 / - / 4

$D_{fan} = 1.173 \text{ m} = 46.2 \text{ in}$ $D = 1.321 \text{ m}$

$W_{eng} = 1120 \text{ kg} = 2469 \text{ lb}$ $= 52 \text{ in}$

Static Sea Level:

$T_{ssl} = 55603 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 12500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.11 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 3.251 \text{ m}$

$= 128 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-8D3

Manufacturer: GE : General Electric

Application: 728-200 (not produced)

Composition: 1 / - / 10 / 2 / - / 4

$D_{fan} = 1.173 \text{ m} = 46.2 \text{ in}$ $D = 1.321 \text{ m}$

$W_{eng} = 1120 \text{ kg} = 2469 \text{ lb}$ $= 52 \text{ in}$

Static Sea Level:

$T_{ssl} = 57271 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 12875 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.11 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.9

OPR = 27

FPR =

TET = °K

Nb of shafts = 2

$L = 3.251 \text{ m}$

$= 128 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-8D6

Manufacturer: GE : General Electric

Application: Envoy 7 (not produced)

Composition: 1 / - / 10 / 2 / - / 4

$D_{fan} = 1.173 \text{ m} = 46.2 \text{ in}$ $D = 1.321 \text{ m}$

$W_{eng} = 1120 \text{ kg} = 2469 \text{ lb}$ $= 52 \text{ in}$

Static Sea Level:

$T_{ssl} = 58049 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 13050 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.11 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 3.251 \text{ m}$

$= 128 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF34-8E2

Manufacturer: GE : General Electric

Application: ERJ-170, ERJ-170LR (option)

Composition: 1 / - / 10 / 2 / - / 4

$D_{fan} = 1.173 \text{ m} = 46.2 \text{ in}$ $D = 1.321 \text{ m}$

$W_{eng} = 1120 \text{ kg} = 2469 \text{ lb}$ $= 52 \text{ in}$

Static Sea Level:

$T_{ssl} = 62275 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 14000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.11 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5$ $\text{OPR} = 27$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.251 \text{ m}$

$= 128 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-45A

Manufacturer: GE : General Electric

Application: B747-100SR/-100SR(SF)

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3977 \text{ kg} = 8768 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 206841 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 46500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 631.9 \text{ kg/s} = 1393.1 \text{ lb/s}$

$\text{BPR} = 4.64$ $\text{OPR} = 26.3$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 50042 \text{ N}$

$= 11250 \text{ lbf}$

$\text{SFC}_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-45A2

Manufacturer: GE : General Electric

Application: B747-100SR/-100SR(SF)

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3977 \text{ kg} = 8768 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 206841 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 46500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 631.9 \text{ kg/s} = 1393.1 \text{ lb/s}$

$\text{BPR} = 4.64$ $\text{OPR} = 26.3$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 50042 \text{ N}$

$= 11250 \text{ lbf}$

$\text{SFC}_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-45B

Manufacturer: GE : General Electric

Application: B747-100SR/-100SR(SF)

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3977 \text{ kg} = 8768 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 206841 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 46500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 631.9 \text{ kg/s} = 1393.1 \text{ lb/s}$
 $BPR = 4.64$ $OPR = 26.3$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 50042 \text{ N}$
 $= 11250 \text{ lbf}$
 $SFC_{cr} = 1.79 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.63 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-45B2

Manufacturer: GE : General Electric

Application: B747-100SR/-100SR(SF), A300B10 (A310) (candidate engine)

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3977 \text{ kg} = 8768 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 206841 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 46500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 631.9 \text{ kg/s} = 1393.1 \text{ lb/s}$
 $BPR = 4.64$ $OPR = 26.3$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 50042 \text{ N}$
 $= 11250 \text{ lbf}$
 $SFC_{cr} = 1.79 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.63 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50

Manufacturer: GE : General Electric

Application: DC-10-30/-30F

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.337 \text{ m} = 92 \text{ in}$ $D = \text{m}$

$W_{eng} = 3674 \text{ kg} = 8100 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 217962 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 49000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = 1.83 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.65 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50A

Manufacturer: GE : General Electric

Application: DC-10-30/-30F, A300B1, A300B2-1A

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.337 \text{ m}$

$W_{eng} = 3720 \text{ kg} = 8201 \text{ lb}$ $= 92 \text{ in}$

Static Sea Level:

$T_{ssl} = 215000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 48334 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.1 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 655 \text{ kg/s} = 1444 \text{ lb/s}$

$\text{BPR} = 4.4$ $\text{OPR} = 28.6$

$\text{FPR} = 1.69$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = 1.85 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.65 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50B

Manufacturer: GE : General Electric

Application:

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.337 \text{ m}$

$W_{eng} = 3720 \text{ kg} = 8201 \text{ lb}$ $= 92 \text{ in}$

Static Sea Level:

$T_{ssl} = 217962 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 49000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.1 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 655 \text{ kg/s} = 1444 \text{ lb/s}$

$\text{BPR} = 4.4$ $\text{OPR} = 28.6$

$\text{FPR} = 1.69$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = 1.85 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.65 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50C

Manufacturer: GE : General Electric

Application: A300B1, A300B2-1C/-101, A300B4-2C/-203, DC-10-30/-30CF/-30F

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3956 \text{ kg} = 8721 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 224000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50357 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.12 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 658.2 \text{ kg/s} = 1451.1 \text{ lb/s}$

$\text{BPR} = 4.26$ $\text{OPR} = 29.3$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 49375 \text{ N}$

$= 11100 \text{ lbf}$

$\text{SFC}_{cr} = 1.86 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.66 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50C1

Manufacturer: GE : General Electric

Application: DC-10-30, A300B2-202, A300B4-102

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3956 \text{ kg} = 8721 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 230500 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 51818 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 666.8 \text{ kg/s} = 1470 \text{ lb/s}$

$\text{BPR} = 4.24$ $\text{OPR} = 30.1$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 51399 \text{ N}$

$= 11555 \text{ lbf}$

$\text{SFC}_{cr} = 1.86 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.66 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50C2

Manufacturer: GE : General Electric

Application: A300B2-203, A300B4-103/-103F/-2C/-203/-203F, A300C4-203, A300F4-203, DC-10-30/-30F/-30F(CF), A300B1 (option), KC-10A

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3960 \text{ kg} = 8730 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 230500 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 51818 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 669.5 \text{ kg/s} = 1476 \text{ lb/s}$

$\text{BPR} = 4.31$ $\text{OPR} = 30.4$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 51399 \text{ N}$

$= 11555 \text{ lbf}$

$\text{SFC}_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50C2B

Manufacturer: GE : General Electric

Application: DC-10-30/-30ER

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3960 \text{ kg} = 8730 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 240203 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 54000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.09 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 682.2 \text{ kg/s} = 1504 \text{ lb/s}$

$\text{BPR} = 4.25$ $\text{OPR} = 31.1$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 51399 \text{ N}$

$= 11555 \text{ lbf}$

$\text{SFC}_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50C2F

Manufacturer: GE : General Electric

Application: DC-10-15

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3960 \text{ kg} = 8730 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 206841 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 46500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 631.9 \text{ kg/s} = 1393.1 \text{ lb/s}$
 $BPR = 4.64$ $OPR = 26.3$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 51399 \text{ N}$
 $= 11555 \text{ lbf}$
 $SFC_{cr} = 1.79 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.63 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50C2R

Manufacturer: GE : General Electric

Application: A300B2-1C/-101, A300B2K-3C, A300B4-2C, DC-10-30

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3960 \text{ kg} = 8730 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 224000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50357 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.04 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.37 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR = 4.31$ $OPR = 29.2$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.65 \text{ m}$

$= 183.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

CF6-50D

Manufacturer: GE : General Electric

Application: DC-10-10

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3776 \text{ kg} = 8325 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 226858 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 51000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

CF6-50D1

Manufacturer: GE : General Electric

Application: YC-14

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 226858 N$ $T_{ssl}^{AB} = N$

$= 51000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CF6-50E

Manufacturer: GE : General Electric

Application: B747-200B

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 m = 86.4 in$ $D = 2.667 m$

$W_{eng} = 3851 kg = 8490 lb$ $= 105 in$

Static Sea Level:

$T_{ssl} = 233531 N$ $T_{ssl}^{AB} = N$

$= 52500 lbf$ $= lbf$

$SFC_{ssl} = 1.07 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.38 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 666.8 kg/s = 1470 lb/s$

BPR = 4.24 OPR = 30.1

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = 51399 N$

$= 11555 lbf$

$SFC_{cr} = 1.86 \cdot 10^{-5} (kg/s)/N$

$= 0.66 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 m$

CF6-50E1

Manufacturer: GE : General Electric

Application: B747-200B

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 m = 86.4 in$ $D = 2.667 m$

$W_{eng} = 3851 kg = 8490 lb$ $= 105 in$

Static Sea Level:

$T_{ssl} = 233531 N$ $T_{ssl}^{AB} = N$

$= 52500 lbf$ $= lbf$

$SFC_{ssl} = 1.05 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.37 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 666.8 kg/s = 1470 lb/s$

BPR = 4.24 OPR = 30.1

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = 51399 N$

$= 11555 lbf$

$SFC_{cr} = 1.86 \cdot 10^{-5} (kg/s)/N$

$= 0.66 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 m$

CF6-50E2

Manufacturer: GE : General Electric

Application: B747-200B/-200B(M)/-200B(SF)/-200C(M)/-200F/-300/-300(M)/-300(SF), E-4B

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3977 \text{ kg} = 8768 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 233531 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 52500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 669.5 \text{ kg/s} = 1476 \text{ lb/s}$

BPR = 4.31 OPR = 30.4

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 51399 \text{ N}$

$= 11555 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-50E2B

Manufacturer: GE : General Electric

Application: B747-200/-300 (option)

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3977 \text{ kg} = 8768 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 240203 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 54000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.06 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 682.2 \text{ kg/s} = 1504 \text{ lb/s}$

BPR = 4.24 OPR = 30.9

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 52177 \text{ N}$

$= 11730 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-6

Manufacturer: GE : General Electric

Application: DC-10-10 (option)

Composition: 1 / 1B / 16 / 2 / - / 5

$D_{fan} = \text{m} = \text{in}$ $D = 2.337 \text{ m}$

$W_{eng} = 3334 \text{ kg} = 7350 \text{ lb}$ $= 92 \text{ in}$

Static Sea Level:

$T_{ssl} = 177928 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 40000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 609.2 \text{ kg/s} = 1343.1 \text{ lb/s}$

BPR = 6.2 OPR = 26.6

FPR = 1.64 TET = °K

Nb of shafts = 2

$L = 4.382 \text{ m}$

$= 172.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-6D

Manufacturer: GE : General Electric

Application: DC-10-10/-10F/-10F(CF)

Composition: 1 / 1B / 16 / 2 / - / 5

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3582 \text{ kg} = 7897 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 177928 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 40000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.10 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 591 \text{ kg/s} = 1302.9 \text{ lb/s}$

$\text{BPR} = 5.72$ $\text{OPR} = 24.3$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 40390 \text{ N}$

$= 9080 \text{ lbf}$

$\text{SFC}_{cr} = 1.83 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.65 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-6D1

Manufacturer: GE : General Electric

Application: DC-10-10/-10F/-10F(AF)

Composition: 1 / 1B / 16 / 2 / - / 5

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3582 \text{ kg} = 7897 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 184600 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 41500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 602.4 \text{ kg/s} = 1328.1 \text{ lb/s}$

$\text{BPR} = 5.76$ $\text{OPR} = 25.2$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 41012 \text{ N}$

$= 9220 \text{ lbf}$

$\text{SFC}_{cr} = 1.83 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.65 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-6D1A

Manufacturer: GE : General Electric

Application: DC-10-10/-10F/-10F(AF)

Composition: 1 / 1B / 16 / 2 / - / 5

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3582 \text{ kg} = 7897 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 184600 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 41500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 602.4 \text{ kg/s} = 1328.1 \text{ lb/s}$

$\text{BPR} = 5.76$ $\text{OPR} = 25.2$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 41012 \text{ N}$

$= 9220 \text{ lbf}$

$\text{SFC}_{cr} = 1.83 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.65 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-6E

Manufacturer: GE : General Electric

Application: DC-10-10/-10F (option)

Composition: 1 / 1B / 16 / 2 / - / 5

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 180597 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 40600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-6F

Manufacturer: GE : General Electric

Application: DC-10-10/-10F (option)

Composition: 1 / 1B / 16 / 2 / - / 5

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 186824 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 42000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-6K

Manufacturer: GE : General Electric

Application: DC-10-10/-10F

Composition: 1 / 1B / 16 / 2 / - / 5

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3709 \text{ kg} = 8177 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 184600 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 41500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.98 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.35 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 25

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-6K2

Manufacturer: GE : General Electric

Application: DC-10-10/-10F (option)

Composition: 1 / 1B / 16 / 2 / - / 5

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.667 \text{ m}$

$W_{eng} = 3709 \text{ kg} = 8177 \text{ lb}$ $= 105 \text{ in}$

Static Sea Level:

$T_{ssl} = 184600 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 41500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.98 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 25

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-80A

Manufacturer: GE : General Electric

Application: B767-200/-200ER/-200PC

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.489 \text{ m}$

$W_{eng} = 3854 \text{ kg} = 8497 \text{ lb}$ $= 98 \text{ in}$

Static Sea Level:

$T_{ssl} = 213514 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 48000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 650.9 \text{ kg/s} = 1435 \text{ lb/s}$

BPR = 4.66 OPR = 27.3

FPR = TET = °K

Nb of shafts = 2

$L = 3.998 \text{ m}$

$= 157.4 \text{ in}$

Cruise:

$T_{cr} = 49130 \text{ N}$

$= 11045 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80A1

Manufacturer: GE : General Electric

Application: B767-200/-200ER (option)

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.489 \text{ m}$

$W_{eng} = 3819 \text{ kg} = 8419 \text{ lb}$ $= 98 \text{ in}$

Static Sea Level:

$T_{ssl} = 213514 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 48000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 650.9 \text{ kg/s} = 1435 \text{ lb/s}$

BPR = 4.66 OPR = 27.3

FPR = TET = °K

Nb of shafts = 2

$L = 3.998 \text{ m}$

$= 157.4 \text{ in}$

Cruise:

$T_{cr} = 49130 \text{ N}$

$= 11045 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80A2

Manufacturer: GE : General Electric

Year: 1981

Application: A310-200, B767-200/-200ER/-300

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.489 \text{ m}$

$W_{eng} = 3854 \text{ kg} = 8497 \text{ lb}$ $= 98 \text{ in}$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 662.2 \text{ kg/s} = 1459.9 \text{ lb/s}$

BPR = 4.59 OPR = 28.4

FPR = 1.7 TET = °K

Nb of shafts = 2

$L = 3.998 \text{ m}$

$= 157.4 \text{ in}$

Cruise:

$T_{cr} = 49130 \text{ N}$

$= 11045 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80A3

Manufacturer: GE : General Electric

Application: A310-203/-203F

Composition: 1 / 3B / 14 / 2 / - / 4

$D_{fan} = 2.195 \text{ m} = 86.4 \text{ in}$ $D = 2.489 \text{ m}$

$W_{eng} = 3819 \text{ kg} = 8419 \text{ lb}$ $= 98 \text{ in}$

Static Sea Level:

$T_{ssl} = 217900 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 48986 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.01 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 662.2 \text{ kg/s} = 1459.9 \text{ lb/s}$

BPR = 4.59 OPR = 28.4

FPR = 1.7 TET = °K

Nb of shafts = 2

$L = 3.998 \text{ m}$

$= 157.4 \text{ in}$

Cruise:

$T_{cr} = 49130 \text{ N}$

$= 11045 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80C2

Manufacturer: GE : General Electric

Application: B767-200ER/-300 (option)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = \text{m}$

$W_{eng} = 4144 \text{ kg} = 9136 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 233531 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 52500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 802.4 \text{ kg/s} = 1769 \text{ lb/s}$

BPR = 5.2 OPR = 30.4

FPR = TET = °K

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = 50398 \text{ N}$

$= 11330 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

CF6-80C2A1

Manufacturer: GE : General Electric

Application: A300B4-601

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4246 \text{ kg} = 9361 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 257400 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 57866 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.95 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 795.6 \text{ kg/s} = 1754 \text{ lb/s}$

$\text{BPR} = 5.15$ $\text{OPR} = 30.4$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = 52533 \text{ N}$

$= 11810 \text{ lbf}$

$\text{SFC}_{cr} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80C2A2

Manufacturer: GE : General Electric

Application: A310-204/-304/-304ET/-304F, CC-150 Polarix

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4246 \text{ kg} = 9361 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 233353 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 52460 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.9 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 802.4 \text{ kg/s} = 1769 \text{ lb/s}$

$\text{BPR} = 5.05$ $\text{OPR} = 27.8$

$\text{FPR} = 1.66$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = 50398 \text{ N}$

$= 11330 \text{ lbf}$

$\text{SFC}_{cr} = 1.64 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80C2A3

Manufacturer: GE : General Electric

Application: A300B4-603, MD-11 (option)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4246 \text{ kg} = 9361 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 262221 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 58950 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 802.4 \text{ kg/s} = 1769 \text{ lb/s}$

$\text{BPR} = 5.05$ $\text{OPR} = 31.1$

$\text{FPR} = 1.73$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = 50443 \text{ N}$

$= 11340 \text{ lbf}$

$\text{SFC}_{cr} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80C2A5

Manufacturer: GE : General Electric

Year: 1987

Application: A300B4-605R, A300C4-605R, A300F4-605R

Composition: 1 / 4B / 14 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$L = 4.087 \text{ m}$

$W_{eng} = 4259 \text{ kg} = 9389 \text{ lb}$ $= 106 \text{ in}$

$= 160.9 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 267337 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = 50443 \text{ N}$

$= 60100 \text{ lbf}$ $= \text{lbf}$

$= 11340 \text{ lbf}$

$\text{SFC}_{ssl} = 0.96 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = 1.64 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 802.4 \text{ kg/s} = 1769 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.05$ $\text{OPR} = 31.5$

$\text{OPR}_{cr} =$

$\text{FPR} =$ $\text{TET} = 1608 \text{ }^\circ\text{K}$

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CF6-80C2A5F

Manufacturer: GE : General Electric

Application: A300B4-605R, A300C4-605R, A300F4-605R

Composition: 1 / 4B / 14 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$L = 4.087 \text{ m}$

$W_{eng} = 4259 \text{ kg} = 9389 \text{ lb}$ $= 106 \text{ in}$

$= 160.9 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 267337 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 60100 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = 0.96 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.05$ $\text{OPR} = 31.5$

$\text{OPR}_{cr} =$

$\text{FPR} =$ $\text{TET} = \text{ }^\circ\text{K}$

$M_{cr} =$, $h_{cr} = \text{m}$

CF6-80C2A6

Manufacturer: GE : General Electric

Application: A300-600

Composition: 1 / 4B / 14 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$L = 4.087 \text{ m}$

$W_{eng} = 4300 \text{ kg} = 9480 \text{ lb}$ $= 106 \text{ in}$

$= 160.9 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 284685 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 64000 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.05$ $\text{OPR} =$

$\text{OPR}_{cr} =$

$\text{FPR} =$ $\text{TET} = \text{ }^\circ\text{K}$

$M_{cr} =$, $h_{cr} = \text{m}$

CF6-80C2A6F

Manufacturer: GE : General Electric

Application:

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4300 \text{ kg} = 9480 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 280237 \text{ N}$

$= 63000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.05

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2A7

Manufacturer: GE : General Electric

Application: A310-308, A310-308ET (option)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4259 \text{ kg} = 9389 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 262444 \text{ N}$

$= 59000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.05

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2A8

Manufacturer: GE : General Electric

Application: A300B4-608ST, A310-308/-308ET

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4259 \text{ kg} = 9389 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 257400 \text{ N}$

$= 57866 \text{ lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.34 (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 802.4 \text{ kg/s} = 1769 \text{ lb/s}$

BPR = 5.05

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

OPR = 30.4

TET = °K

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B1

Manufacturer: GE : General Electric

Application: B747-300/-300(M), VC-25A

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4258 \text{ kg} = 9387 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 252213 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 56700 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 775.6 \text{ kg/s} = 1709.9 \text{ lb/s}$

$\text{BPR} = 5.19$ $\text{OPR} = 29.3$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = 57026 \text{ N}$

$= 12820 \text{ lbf}$

$\text{SFC}_{cr} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80C2B1F

Manufacturer: GE : General Electric

Application: B747-400/-400D/-400ER/-400(M)/-400F, YAL-1A

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4309 \text{ kg} = 9500 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 254259 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 57160 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.9 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 800.1 \text{ kg/s} = 1763.9 \text{ lb/s}$

$\text{BPR} = 5.15$ $\text{OPR} = 30.4$

$\text{FPR} =$ $\text{TET} = 1608 ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = 57026 \text{ N}$

$= 12820 \text{ lbf}$

$\text{SFC}_{cr} = 1.6 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.56 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80C2B1F2

Manufacturer: GE : General Electric

Application: B747-400/-400D/-400ER/-400(M)/-400F

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4309 \text{ kg} = 9500 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 257551 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 57900 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.19$ $\text{OPR} =$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B2

Manufacturer: GE : General Electric

Year: 1986

Application: B767-200ER/-300/-300ER, B737-200 (option)

Composition: 1 / 4B / 14 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$L = 4.087 \text{ m}$

$W_{eng} = 4258 \text{ kg} = 9387 \text{ lb}$ $= 106 \text{ in}$

$= 160.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 229483 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 51590 \text{ lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = 0.9 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 748.4 \text{ kg/s} = 1649.9 \text{ lb/s}$

BPR = 5.31

OPR = 27.1

FPR =

TET = 1608 °K

Cruise:

$T_{cr} = 53378 \text{ N}$

$= 12000 \text{ lbf}$

$\text{SFC}_{cr} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CF6-80C2B2F

Manufacturer: GE : General Electric

Application: B767-200/-200ER/-300/-300ER (option)

Composition: 1 / 4B / 14 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$L = 4.087 \text{ m}$

$W_{eng} = 4309 \text{ kg} = 9500 \text{ lb}$ $= 106 \text{ in}$

$= 160.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 231351 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 52010 \text{ lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$

$\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.31

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B3

Manufacturer: GE : General Electric

Application: B747-300/-400 (option)

Composition: 1 / 4B / 14 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$L = 4.087 \text{ m}$

$W_{eng} = 4258 \text{ kg} = 9387 \text{ lb}$ $= 106 \text{ in}$

$= 160.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 231351 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 52010 \text{ lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$

$\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B3F

Manufacturer: GE : General Electric

Application: B747-300/-400 (option)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4309 \text{ kg} = 9500 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 231351 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 52010 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} =$ $\text{OPR} =$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B4

Manufacturer: GE : General Electric

Application: B767-200ER/-300/-300ER

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4263 \text{ kg} = 9398 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 254348 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 57180 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.92 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.33 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.15$ $\text{OPR} = 29.9$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B4F

Manufacturer: GE : General Electric

Application: B767-200ER/-300/-300ER

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4427 \text{ kg} = 9760 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 254793 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 57280 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.9 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.32 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.14$ $\text{OPR} = 29.9$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B5F

Manufacturer: GE : General Electric

Application: B747-400/-400ER/-400F/-400FER

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4427 \text{ kg} = 9760 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 276233 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 62100 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} =$ $\text{OPR} = 31.4$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

$\text{Nb of shafts} = 2$

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B6

Manufacturer: GE : General Electric

Application: B767-300/-300ER/-200ER (option), An-218-200/-300 (proposed)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4386 \text{ kg} = 9669 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 267203 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 60070 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.95 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.06$ $\text{OPR} = 31.1$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

$\text{Nb of shafts} = 2$

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B6F

Manufacturer: GE : General Electric

Application: B767-300ER, B767-200ER (option), Italian KC-767A

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4427 \text{ kg} = 9760 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 267025 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 60030 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.06$ $\text{OPR} = 31.4$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

$\text{Nb of shafts} = 2$

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B6FA

Manufacturer: GE : General Electric

Application: B767-200ER

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4427 \text{ kg} = 9760 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 267025 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 60030 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 5.06$ $\text{OPR} = 31.4$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B7F

Manufacturer: GE : General Electric

Application: B767-300ER/-300F/-200ER (option)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4427 \text{ kg} = 9760 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 276233 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 62100 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} =$ $\text{OPR} = 31.4$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B8F

Manufacturer: GE : General Electric

Application: B767-400ER/-400FER, E-10A, E-767A AWACS (proposed)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4522 \text{ kg} = 9969 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 282461 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 63500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} =$ $\text{OPR} = 31.4$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2B9F

Manufacturer: GE : General Electric

Application: B747-400XQLR/-XQLRF

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = \text{kg} = \text{lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 281571 \text{ N}$

$= 63300 \text{ lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 31.4

TET = °K

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr}=

$M_{cr} = , h_{cr} = \text{m}$

CF6-80C2D1F

Manufacturer: GE : General Electric

Application: MD-11/-11F/-11F(AF)/-11F(C)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.362 \text{ m} = 93 \text{ in}$ $D = 2.692 \text{ m}$

$W_{eng} = 4468 \text{ kg} = 9850 \text{ lb}$ $= 106 \text{ in}$

Static Sea Level:

$T_{ssl} = 269961 \text{ N}$

$= 60690 \text{ lbf}$

$\text{SFC}_{ssl} = 0.91 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.32 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.03

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

OPR = 31.8

TET = °K

Nb of shafts = 2

$L = 4.087 \text{ m}$

$= 160.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr}=

$M_{cr} = , h_{cr} = \text{m}$

CF6-80E1

Manufacturer: GE : General Electric

Application: A330-200/-300 (option)

Composition: 1 / 4B / 14 / 2 / - / 4

$D_{fan} = \text{m} = \text{in}$ $D = 2.896 \text{ m}$

$W_{eng} = 5063 \text{ kg} = 11162 \text{ lb}$ $= 114 \text{ in}$

Static Sea Level:

$T_{ssl} = 291357 \text{ N}$

$= 65500 \text{ lbf}$

$\text{SFC}_{ssl} = 0.93 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.33 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 867.7 \text{ kg/s} = 1913 \text{ lb/s}$

BPR = 5.3

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

OPR = 32.4

TET = °K

Nb of shafts = 2

$L = 4.173 \text{ m}$

$= 164.3 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr}=

$M_{cr} = , h_{cr} = \text{m}$

CF6-80E1A1

Manufacturer: GE : General Electric

Application: A330-200/-300 (option)

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = m = in$ $D = 2.896 m$

$W_{eng} = 5063 kg = 11162 lb$ $= 114 in$

Static Sea Level:

$T_{ssl} = 291357 N$ $T_{ssl}^{AB} = N$

$= 65500 lbf$ $= lbf$

$SFC_{ssl} = 0.93 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.33 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 867.7 kg/s = 1913 lb/s$

BPR = 5.3 OPR = 32.4

FPR = TET = °K

Nb of shafts = 2

$L = 4.173 m$

$= 164.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CF6-80E1A2

Manufacturer: GE : General Electric

Application: A330-201

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = 2.794 m = 110 in$ $D = 2.896 m$

$W_{eng} = 4865 kg = 10725 lb$ $= 114 in$

Static Sea Level:

$T_{ssl} = 287055 N$ $T_{ssl}^{AB} = N$

$= 64533 lbf$ $= lbf$

$SFC_{ssl} = 0.94 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.33 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 873.6 kg/s = 1926 lb/s$

BPR = 5.3 OPR = 32.4

FPR = TET = °K

Nb of shafts = 2

$L = 4.343 m$

$= 171 in$

Cruise:

$T_{cr} = N$

$= 0 lbf$

$SFC_{cr} = 1.59 \cdot 10^{-5} (kg/s)/N$

$= 0.56 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CF6-80E1A3

Manufacturer: GE : General Electric

Application: A330-203

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = m = in$ $D = 2.896 m$

$W_{eng} = 4865 kg = 10725 lb$ $= 114 in$

Static Sea Level:

$T_{ssl} = 304840 N$ $T_{ssl}^{AB} = N$

$= 68531 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 5 OPR = 33.7

FPR = TET = °K

Nb of shafts = 2

$L = 4.343 m$

$= 171 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CF6-80E1A4

Manufacturer: GE : General Electric

Application: A330-202

Composition: 1 / 4B / 14 / 2 / - / 5

$D_{fan} = m = in$ $D = 2.896 m$

$W_{eng} = 4865 kg = 10725 lb$ $= 114 in$

Static Sea Level:

$T_{ssl} = 297451 N$ $T_{ssl}^{AB} = N$

$= 66870 lbf$ $= lbf$

$SFC_{ssl} = 0.96 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.34 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 5 OPR = 33.7

FPR = TET = °K

Nb of shafts = 2

$L = 4.343 m$

$= 171 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CF700-2B

Manufacturer: GE : General Electric

Application: Falcon 20

Composition: 1 aft / - / 8 / 2 / - / 1

$D_{fan} = 0.913 m = 35.9 in$ $D = 0.843 m$

$W_{eng} = 334 kg = 736 lb$ $= 33.2 in$

Static Sea Level:

$T_{ssl} = 19130 N$ $T_{ssl}^{AB} = N$

$= 4301 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 38.1 kg/s = 84 lb/s$

BPR = 1.9 OPR = 6.8

FPR = TET = °K

Year: 1962

Nb of shafts = 2

$L = 1.361 m$

$= 53.6 in$

Cruise:

$T_{cr} = 4199 N$

$= 944 lbf$

$SFC_{cr} = 2.63 \cdot 10^{-5} (kg/s)/N$

$= 0.93 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 11000 m$

CF700-2C

Manufacturer: GE : General Electric

Application: Falcon 20C

Composition: 1 aft / - / 8 / 2 / - / 1

$D_{fan} = m = in$ $D = 0.843 m$

$W_{eng} = 329 kg = 725 lb$ $= 33.2 in$

Static Sea Level:

$T_{ssl} = 18349 N$ $T_{ssl}^{AB} = N$

$= 4125 lbf$ $= lbf$

$SFC_{ssl} = 1.85 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.65 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 38.1 kg/s = 84 lb/s$

BPR = 1.9 OPR = 6.9

FPR = TET = °K

Nb of shafts = 2

$L = 1.361 m$

$= 53.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CF700-2D

Manufacturer: GE : General Electric

Application: Mystere 20, Falcon 20D

Composition: 1 aft / - / 8 / 2 / - / 1

$D_{fan} = m = in$ $D = 0.843 m$

$W_{eng} = 334 kg = 736 lb$ $= 33.2 in$

Static Sea Level:

$T_{ssl} = 18905 N$ $T_{ssl}^{AB} = N$
 $= 4250 lbf$ $= lbf$

$SFC_{ssl} = 1.85 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.65 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 38.1 kg/s = 84 lb/s$

BPR = 1.9 OPR = 6.2

FPR = TET = °K

Nb of shafts = 2

$L = 1.361 m$

$= 53.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CF700-2D2

Manufacturer: GE : General Electric

Application: Falcon 20E/F, Sabreliner 75A/80A

Composition: 1 aft / - / 8 / 2 / - / 1

$D_{fan} = m = in$ $D = 0.94 m$

$W_{eng} = 348 kg = 767 lb$ $= 37 in$

Static Sea Level:

$T_{ssl} = 19194 N$ $T_{ssl}^{AB} = N$
 $= 4315 lbf$ $= lbf$

$SFC_{ssl} = 1.82 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.64 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 38.1 kg/s = 84 lb/s$

BPR = 1.9 OPR = 6.8

FPR = TET = °K

Nb of shafts = 2

$L = 1.361 m$

$= 53.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CFE738

Manufacturer: CFE : GE + ASE

Year: 1992

Application: Falcon 2000

Composition: 1 / / / /

$D_{fan} = 0.902 m = 35.5 in$ $D = m$

$W_{eng} = 551 kg = 1215 lb$ $= in$

Static Sea Level:

$T_{ssl} = 26325 N$ $T_{ssl}^{AB} = N$
 $= 5918 lbf$ $= lbf$

$SFC_{ssl} = 1.05 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.37 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 108.9 kg/s = 240.1 lb/s$

BPR = 5.3 OPR = 23

FPR = TET = 1643 °K

Nb of shafts =

$L = 1.734 m$

$= 68.3 in$

Cruise:

$T_{cr} = 5827 N$

$= 1310 lbf$

$SFC_{cr} = 1.83 \cdot 10^{-5} (kg/s)/N$

$= 0.65 (lb/h)/lbf$

$\dot{w}_{cr} = 112 kg/s = 246.9 lb/s$

OPR_{cr} = 32

$M_{cr} = 0.8 , h_{cr} = 12192 m$

CFE738-1-1B

Manufacturer: CFE : GE + ASE

Application: Falcon 2000

Composition: 1 / - / 5 + 1C / 2 / - / 3

$D_{fan} = 0.902 \text{ m} = 35.5 \text{ in}$ $D = 1.219 \text{ m}$

$W_{eng} = 601 \text{ kg} = 1325 \text{ lb}$ $= 48 \text{ in}$

Static Sea Level:

$T_{ssl} = 25466 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 5725 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 95.3 \text{ kg/s} = 210.1 \text{ lb/s}$

$\text{BPR} = 5.3$ $\text{OPR} = 23$

$\text{FPR} = 1.7$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.515 \text{ m}$

$= 99 \text{ in}$

Cruise:

$T_{cr} = 6512 \text{ N}$

$= 1464 \text{ lbf}$

$\text{SFC}_{cr} = 1.83 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.65 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8$, $h_{cr} = 12192 \text{ m}$

CFM56-2A2

Manufacturer: CFM International : GE + Snecma

Year:

Application: E-3D, KE-3A, KC-3, E-6A/B

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 2186 \text{ kg} = 4819 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 106757 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 24000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 370.6 \text{ kg/s} = 817 \text{ lb/s}$

$\text{BPR} = 5.9$ $\text{OPR} = 25.4$

$\text{FPR} = 1.45$ $\text{TET} = 1628 ^\circ\text{K}$

Nb of shafts = 2

$L = 2.431 \text{ m}$

$= 95.7 \text{ in}$

Cruise:

$T_{cr} = 26900 \text{ N}$

$= 6047 \text{ lbf}$

$\text{SFC}_{cr} = 1.88 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.66 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} = 31.7$

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CFM56-2B1

Manufacturer: CFM International : GE + Snecma

Application: KC-135R/T, C-135FR, RC-135RE

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 2119 \text{ kg} = 4672 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 22000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 355.6 \text{ kg/s} = 784 \text{ lb/s}$

$\text{BPR} = 6$ $\text{OPR} = 23.7$

$\text{FPR} =$ $\text{TET} = 1560 ^\circ\text{K}$

Nb of shafts = 2

$L = 2.431 \text{ m}$

$= 95.7 \text{ in}$

Cruise:

$T_{cr} = 22108 \text{ N}$

$= 4970 \text{ lbf}$

$\text{SFC}_{cr} = 1.84 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.65 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} = 30.5$

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CFM56-2C1

Manufacturer: CFM International : GE + Snecma

Year: 1979

Application: DC-8-71F/-72/-72F/-73F, DC-8-71/-73 (option)

Composition: 1 / 3B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$L = 2.431 \text{ m}$

$W_{eng} = 2102 \text{ kg} = 4634 \text{ lb}$ $= 72 \text{ in}$

$= 95.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 22000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 357.4 \text{ kg/s} = 787.9 \text{ lb/s}$

BPR = 6 OPR = 24.7

FPR = 1.45 TET = 1543 °K

Cruise:

$T_{cr} = 22152 \text{ N}$

$= 4980 \text{ lbf}$

$\text{SFC}_{cr} = 1.9 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.67 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 31.2

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-2C2

Manufacturer: CFM International : GE + Snecma

Application: Trident

Composition: 1 / 3B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$L = 2.431 \text{ m}$

$W_{eng} = \text{kg} = \text{lb}$ $= 72 \text{ in}$

$= 95.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 106757 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 24000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 26.5

FPR = TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-3B1

Manufacturer: CFM International : GE + Snecma

Application: B737-300/-300(QC)/-500, B737-400 (option)

Composition: 1 / 3B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.524 \text{ m} = 60 \text{ in}$ $D = 1.6 \text{ m}$

$L = 2.365 \text{ m}$

$W_{eng} = 1940 \text{ kg} = 4277 \text{ lb}$ $= 63 \text{ in}$

$= 93.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 88964 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 20000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.08 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.38 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 297.1 \text{ kg/s} = 655 \text{ lb/s}$

BPR = 6 OPR = 22.6

FPR = TET = °K

Cruise:

$T_{cr} = 20684 \text{ N}$

$= 4650 \text{ lbf}$

$\text{SFC}_{cr} = 1.89 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.67 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 27.5

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-3B2

Manufacturer: CFM International : GE + Snecma

Year: 1984

Application: B737-300/-300(QC)/-300F/-400

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.524 \text{ m} = 60 \text{ in}$ $D = 1.6 \text{ m}$

$W_{eng} = 1951 \text{ kg} = 4301 \text{ lb}$ $= 63 \text{ in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 22000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.11 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 309.8 \text{ kg/s} = 683 \text{ lb/s}$

BPR = 5.9 OPR = 24.3

FPR = TET = 1642 °K

Nb of shafts = 2

$L = 2.365 \text{ m}$

$= 93.1 \text{ in}$

Cruise:

$T_{cr} = 22419 \text{ N}$

$= 5040 \text{ lbf}$

$SFC_{cr} = 1.89 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.67 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 28.8

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-3C1

Manufacturer: CFM International : GE + Snecma

Year: 1986

Application: B737-300/-300(QC)/-300F/-400/-500

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.524 \text{ m} = 60 \text{ in}$ $D = 1.6 \text{ m}$

$W_{eng} = 1951 \text{ kg} = 4301 \text{ lb}$ $= 63 \text{ in}$

Static Sea Level:

$T_{ssl} = 104533 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 23500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 322 \text{ kg/s} = 709.9 \text{ lb/s}$

BPR = 6 OPR = 25.2

FPR = TET = 1646 °K

Nb of shafts = 2

$L = 2.365 \text{ m}$

$= 93.1 \text{ in}$

Cruise:

$T_{cr} = 23887 \text{ N}$

$= 5370 \text{ lbf}$

$SFC_{cr} = 1.89 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.67 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 30.6

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5A1

Manufacturer: CFM International : GE + Snecma

Year: 1987

Application: A320-211/-311

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2266 \text{ kg} = 4996 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 111205 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 25000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 386.5 \text{ kg/s} = 852.1 \text{ lb/s}$

BPR = 6 OPR = 26.5

FPR = 1.55 TET = 1537 °K

Nb of shafts = 2

$L = 2.423 \text{ m}$

$= 95.4 \text{ in}$

Cruise:

$T_{cr} = 22241 \text{ N}$

$= 5000 \text{ lbf}$

$SFC_{cr} = 1.69 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 31.3

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5A3

Manufacturer: CFM International : GE + Snecma

Application: A320-212

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2266 \text{ kg} = 4996 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 117877 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 26500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 397.3 \text{ kg/s} = 875.9 \text{ lb/s}$

$BPR = 6$ $OPR = 27.8$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.423 \text{ m}$

$= 95.4 \text{ in}$

Cruise:

$T_{cr} = 22241 \text{ N}$

$= 5000 \text{ lbf}$

$SFC_{cr} = 1.69 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.6 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5A4

Manufacturer: CFM International : GE + Snecma

Application: A319-113

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2257 \text{ kg} = 4976 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 22000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 370.1 \text{ kg/s} = 815.9 \text{ lb/s}$

$BPR = 6.2$ $OPR = 24.1$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.423 \text{ m}$

$= 95.4 \text{ in}$

Cruise:

$T_{cr} = 22241 \text{ N}$

$= 5000 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5A5

Manufacturer: CFM International : GE + Snecma

Application: A319-114

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2257 \text{ kg} = 4976 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 104533 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 23500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 381.9 \text{ kg/s} = 841.9 \text{ lb/s}$

$BPR = 6.2$ $OPR = 25.4$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.423 \text{ m}$

$= 95.4 \text{ in}$

Cruise:

$T_{cr} = 22241 \text{ N}$

$= 5000 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5B1

Manufacturer: CFM International : GE + Snecma

Year: 1994

Application: A321-111

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 133446 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 30000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 427.7 \text{ kg/s} = 942.9 \text{ lb/s}$

BPR = 5.5 OPR = 32

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = 25977 \text{ N}$

$= 5840 \text{ lbf}$

$\text{SFC}_{cr} = 1.69 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.6 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 35.4

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CFM56-5B1/2

Manufacturer: CFM International : GE + Snecma

Year: 1994

Application: A321-111

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 133446 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 30000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 427.7 \text{ kg/s} = 942.9 \text{ lb/s}$

BPR = 5.5 OPR = 32

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

CFM56-5B1/P

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A321-111

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 133446 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 30000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 427.7 \text{ kg/s} = 942.9 \text{ lb/s}$

BPR = 5.5 OPR = 32

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

CFM56-5B2

Manufacturer: CFM International : GE + Snecma

Year: 1993

Application: A321-112

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 137894 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 31000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 433.6 \text{ kg/s} = 955.9 \text{ lb/s}$

BPR = 5.5 OPR = 32.9

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = 25977 \text{ N}$

$= 5840 \text{ lbf}$

$SFC_{cr} = 1.54 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.55 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 35.5

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5B2/P

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A321-112

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 137894 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 31000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 433.6 \text{ kg/s} = 955.9 \text{ lb/s}$

BPR = 5.5 OPR = 32.9

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B3

Manufacturer: CFM International : GE + Snecma

Application: A321-211

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 142342 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 32000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 433.6 \text{ kg/s} = 955.9 \text{ lb/s}$

BPR = 5.4 OPR = 33.7

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = 25977 \text{ N}$

$= 5840 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 35.5

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5B3/2P

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A321-211

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 142342 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 32000 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $\text{BPR} = 5.4$ $\text{OPR} = 33.7$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2
 $L = 2.601 \text{ m}$
 $= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

CFM56-5B3/P

Manufacturer: CFM International : GE + Snecma

Year: 2003

Application: A321-211

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 142342 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 32000 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 433.6 \text{ kg/s} = 955.9 \text{ lb/s}$
 $\text{BPR} = 5.4$ $\text{OPR} = 33.7$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2
 $L = 2.601 \text{ m}$
 $= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

CFM56-5B4

Manufacturer: CFM International : GE + Snecma

Year: 1994

Application: A320-214

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 120101 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 27000 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 0.96 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 406.9 \text{ kg/s} = 897.1 \text{ lb/s}$
 $\text{BPR} = 5.7$ $\text{OPR} = 29.1$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2
 $L = 2.601 \text{ m}$
 $= 102.4 \text{ in}$

Cruise:

$T_{cr} = 22241 \text{ N}$
 $= 5000 \text{ lbf}$
 $\text{SFC}_{cr} = 1.54 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.55 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} = 32.6$
 $M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5B4/2

Manufacturer: CFM International : GE + Snecma

Year: 1994

Application: A320-214

Composition: 1 / 4B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$L = 2.601 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

$= 102.4 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 120101 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 27000 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = 0.96 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 406.9 \text{ kg/s} = 897.1 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 5.7 OPR = 29.1

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B4/2P

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A320-214

Composition: 1 / 4B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$L = 2.601 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

$= 102.4 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 120101 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 27000 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = 0.96 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 406.9 \text{ kg/s} = 897.1 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 5.7 OPR = 29.1

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B4/P

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A320-214

Composition: 1 / 4B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$L = 2.601 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

$= 102.4 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 120101 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 27000 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = 0.96 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 406.9 \text{ kg/s} = 897.1 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 5.7 OPR = 29.1

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B5

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A319-111

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 22000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 371 \text{ kg/s} = 817.9 \text{ lb/s}$
 $BPR = 6$ $OPR = 24.4$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2
 $L = 2.601 \text{ m}$
 $= 102.4 \text{ in}$

Cruise:

$T_{cr} = 22330 \text{ N}$
 $= 5020 \text{ lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} = 32.6$
 $M_{cr} = 0.8, h_{cr} = 10670 \text{ m}$

CFM56-5B5/P

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A319-111

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 22000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 371 \text{ kg/s} = 817.9 \text{ lb/s}$
 $BPR = 6$ $OPR = 24.4$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2
 $L = 2.601 \text{ m}$
 $= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

CFM56-5B6

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A319-112

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 104533 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 23500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 382.8 \text{ kg/s} = 843.9 \text{ lb/s}$
 $BPR = 5.9$ $OPR = 25.8$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2
 $L = 2.601 \text{ m}$
 $= 102.4 \text{ in}$

Cruise:

$T_{cr} = 22330 \text{ N}$
 $= 5020 \text{ lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} = 32.6$
 $M_{cr} = 0.8, h_{cr} = 10670 \text{ m}$

CFM56-5B6/2

Manufacturer: CFM International : GE + Snecma

Year: 1995

Application: A319-112

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 104533 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 23500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 382.8 \text{ kg/s} = 843.9 \text{ lb/s}$

BPR = 5.9 OPR = 25.8

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B6/2P

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A319-112

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 104533 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 23500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 382.8 \text{ kg/s} = 843.9 \text{ lb/s}$

BPR = 5.9 OPR = 25.8

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B6/P

Manufacturer: CFM International : GE + Snecma

Year: 1996

Application: A319-112

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 104533 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 23500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 382.8 \text{ kg/s} = 843.9 \text{ lb/s}$

BPR = 5.9 OPR = 25.8

FPR = TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B7

Manufacturer: CFM International : GE + Snecma

Year: 1999

Application: A319, A319 CJ

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 120102 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 27000 \text{ lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$

$\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 406.9 \text{ kg/s} = 897.1 \text{ lb/s}$

BPR = 5.7

OPR = 29.1

FPR =

TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = 25978 \text{ N}$

$= 5840 \text{ lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 35.5

$M_{cr} = 0.8, h_{cr} = 10670 \text{ m}$

CFM56-5B7/P

Manufacturer: CFM International : GE + Snecma

Year: 1999

Application: A319-115/-115CJ/-115XCJ

Composition: 1 / 4B / 9 / 1 / - / 4

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

Static Sea Level:

$T_{ssl} = 120101 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 27000 \text{ lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = 0.96 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.34 (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR = 29.1

FPR =

TET = °K

Nb of shafts = 2

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B8

Manufacturer: CFM International : GE + Snecma

Application: A318

Composition: / / / / /

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 96082 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 21600 \text{ lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$

$\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 367.9 \text{ kg/s} = 811.1 \text{ lb/s}$

BPR = 6

OPR =

FPR =

TET = °K

Nb of shafts =

$L = 2.601 \text{ m}$

$= 102.4 \text{ in}$

Cruise:

$T_{cr} = 22330 \text{ N}$

$= 5020 \text{ lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 32.6

$M_{cr} = 0.8, h_{cr} = 10670 \text{ m}$

CFM56-5B8/P

Manufacturer: CFM International : GE + Snecma

Year: 2002

Application: A318-111

Composition: 1 / 4B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$L = 2.601 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

$= 102.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 96080 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 21600 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 6

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5B9

Manufacturer: CFM International : GE + Snecma

Application: A318

Composition: / / / /

Nb of shafts =

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = \text{m}$

$L = 2.601 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= \text{in}$

$= 102.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 103644 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 23300 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 381.5 \text{ kg/s} = 841.1 \text{ lb/s}$

BPR = 5.9

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = 22330 \text{ N}$

$= 5020 \text{ lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 32.6

$M_{cr} = 0.8, h_{cr} = 10670 \text{ m}$

CFM56-5B9/P

Manufacturer: CFM International : GE + Snecma

Year: 2002

Application: A318-112

Composition: 1 / 4B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.735 \text{ m} = 68.3 \text{ in}$ $D = 1.829 \text{ m}$

$L = 2.601 \text{ m}$

$W_{eng} = 2381 \text{ kg} = 5249 \text{ lb}$ $= 72 \text{ in}$

$= 102.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 103644 \text{ N}$

$T_{ssl}^{AB} = \text{N}$

$= 23300 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 6

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-5C2

Manufacturer: CFM International : GE + Snecma

Year: 1991

Application: A340-211/-311

Composition: 1 / 4B / 9 / 1 / - / 5

Nb of shafts = 2

$D_{fan} = 1.836 \text{ m} = 72.3 \text{ in}$ $D = 1.946 \text{ m}$

$L = 2.616 \text{ m}$

$W_{eng} = 2585 \text{ kg} = 5699 \text{ lb}$ $= 76.6 \text{ in}$

$= 103 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 138784 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = 30759 \text{ N}$

$= 31200 \text{ lbf}$ $= \text{lbf}$

$= 6915 \text{ lbf}$

$SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$SFC_{cr} = 1.54 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= 0.55 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 465.8 \text{ kg/s} = 1026.9 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 6.6 OPR = 31.5

OPR_{cr} =

FPR = 1.58 TET = 1633 °K

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CFM56-5C3

Manufacturer: CFM International : GE + Snecma

Year: 1991

Application: A340-212/-312

Composition: 1 / 4B / 9 / 1 / - / 5

Nb of shafts = 2

$D_{fan} = 1.836 \text{ m} = 72.3 \text{ in}$ $D = 1.946 \text{ m}$

$L = 2.616 \text{ m}$

$W_{eng} = 2585 \text{ kg} = 5699 \text{ lb}$ $= 76.6 \text{ in}$

$= 103 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 144567 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = 30737 \text{ N}$

$= 32500 \text{ lbf}$ $= \text{lbf}$

$= 6910 \text{ lbf}$

$SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$SFC_{cr} = 1.54 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= 0.55 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 474 \text{ kg/s} = 1045 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 6.5 OPR = 32.6

OPR_{cr} = 34.7

FPR = TET = °K

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CFM56-5C3/F

Manufacturer: CFM International : GE + Snecma

Year: 1993

Application: A340-312

Composition: 1 / 4B / 9 / 1 / - / 5

Nb of shafts = 2

$D_{fan} = 1.836 \text{ m} = 72.3 \text{ in}$ $D = 1.946 \text{ m}$

$L = 2.616 \text{ m}$

$W_{eng} = 2585 \text{ kg} = 5699 \text{ lb}$ $= 76.6 \text{ in}$

$= 103 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 144567 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 32500 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$SFC_{cr} = \text{(kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 474 \text{ kg/s} = 1045 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 6.5 OPR = 32.6

OPR_{cr} =

FPR = TET = °K

$M_{cr} =$, $h_{cr} = \text{m}$

CFM56-5C4

Manufacturer: CFM International : GE + Snecma

Year: 1994

Application: A340-213/-213X/-313/-313X/-300E

Composition: 1 / 4B / 9 / 1 / - / 5

Nb of shafts = 2

$D_{fan} = 1.836 \text{ m} = 72.3 \text{ in}$ $D = 1.946 \text{ m}$

$L = 2.616 \text{ m}$

$W_{eng} = 2585 \text{ kg} = 5699 \text{ lb}$ $= 76.6 \text{ in}$

$= 103 \text{ in}$

Static Sea Level:

$T_{ssl} = 151239 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 34000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 483.1 \text{ kg/s} = 1065.1 \text{ lb/s}$

BPR = 6.4 OPR = 33.9

FPR = TET = °K

Cruise:

$T_{cr} = 31582 \text{ N}$

$= 7100 \text{ lbf}$

$SFC_{cr} = 1.54 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.55 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 38.3

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-5C4/P

Manufacturer: CFM International : GE + Snecma

Year: 2003

Application: A340-300X

Composition: 1 / 5B / 9 / 1 / - / 5

Nb of shafts = 2

$D_{fan} = 1.836 \text{ m} = 72.3 \text{ in}$ $D = 1.946 \text{ m}$

$L = 2.616 \text{ m}$

$W_{eng} = 2585 \text{ kg} = 5699 \text{ lb}$ $= 76.6 \text{ in}$

$= 103 \text{ in}$

Static Sea Level:

$T_{ssl} = 151239 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 34000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 483.1 \text{ kg/s} = 1065.1 \text{ lb/s}$

BPR = 6.4 OPR =

FPR = TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CFM56-7B18

Manufacturer: CFM International : GE + Snecma

Application: B737-600

Composition: 1 / 3B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.549 \text{ m} = 61 \text{ in}$ $D = 1.651 \text{ m}$

$L = 2.511 \text{ m}$

$W_{eng} = 2366 \text{ kg} = 5216 \text{ lb}$ $= 65 \text{ in}$

$= 98.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 82292 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 18500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 302.5 \text{ kg/s} = 666.9 \text{ lb/s}$

BPR = 5.6 OPR = 21.7

FPR = TET = °K

Cruise:

$T_{cr} = 24109 \text{ N}$

$= 5420 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 32.8

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-7B20

Manufacturer: CFM International : GE + Snecma

Year: 1997

Application: B737-600/-700

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.549 \text{ m} = 61 \text{ in}$ $D = 1.651 \text{ m}$

$W_{eng} = 2366 \text{ kg} = 5216 \text{ lb}$ $= 65 \text{ in}$

Static Sea Level:

$T_{ssl} = 91633 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 20600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 311.2 \text{ kg/s} = 686.1 \text{ lb/s}$

BPR = 5.6 OPR = 22.7

FPR = TET = °K

Nb of shafts = 2

$L = 2.511 \text{ m}$

$= 98.9 \text{ in}$

Cruise:

$T_{cr} = 24243 \text{ N}$

$= 5450 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 32.3

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CFM56-7B22

Manufacturer: CFM International : GE + Snecma

Application: B737-600/-700/-700BBJ/-800/-800BBJ2

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.549 \text{ m} = 61 \text{ in}$ $D = 1.651 \text{ m}$

$W_{eng} = 2366 \text{ kg} = 5216 \text{ lb}$ $= 65 \text{ in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 22000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 329.3 \text{ kg/s} = 726 \text{ lb/s}$

BPR = 5.4 OPR = 24.6

FPR = TET = °K

Nb of shafts = 2

$L = 2.511 \text{ m}$

$= 98.9 \text{ in}$

Cruise:

$T_{cr} = 24243 \text{ N}$

$= 5450 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 32.8

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CFM56-7B24

Manufacturer: CFM International : GE + Snecma

Application: B737-700/-800/-900/-700BBJ/-800BBJ2

Composition: 1 / 3B / 9 / 1 / - / 4

$D_{fan} = 1.549 \text{ m} = 61 \text{ in}$ $D = 1.651 \text{ m}$

$W_{eng} = 2366 \text{ kg} = 5216 \text{ lb}$ $= 65 \text{ in}$

Static Sea Level:

$T_{ssl} = 106757 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 24000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 342 \text{ kg/s} = 754 \text{ lb/s}$

BPR = 5.3 OPR = 26

FPR = TET = °K

Nb of shafts = 2

$L = 2.511 \text{ m}$

$= 98.9 \text{ in}$

Cruise:

$T_{cr} = 24376 \text{ N}$

$= 5480 \text{ lbf}$

$SFC_{cr} = 1.78 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 32.8

$M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

CFM56-7B26

Manufacturer: CFM International : GE + Snecma

Application: B737-700/-700BBJ/-800/-800BBJ2/-900, C-40A/B/C

Composition: 1 / 3B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.549 \text{ m} = 61 \text{ in}$ $D = 1.651 \text{ m}$

$L = 2.511 \text{ m}$

$W_{eng} = 2366 \text{ kg} = 5216 \text{ lb}$ $= 65 \text{ in}$

$= 98.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 117432 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 26400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.08 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.38 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 355.2 \text{ kg/s} = 783.1 \text{ lb/s}$

BPR = 5.1 OPR = 27.9

FPR = TET = °K

Cruise:

$T_{cr} = 24376 \text{ N}$

$= 5480 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 32.8

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

CFM56-7B27

Manufacturer: CFM International : GE + Snecma

Application: B737-600/-700/-800/-900/-BBJ

Composition: 1 / 3B / 9 / 1 / - / 4

Nb of shafts = 2

$D_{fan} = 1.549 \text{ m} = 61 \text{ in}$ $D = 1.651 \text{ m}$

$L = 2.511 \text{ m}$

$W_{eng} = 2366 \text{ kg} = 5216 \text{ lb}$ $= 65 \text{ in}$

$= 98.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 121436 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 27300 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.08 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.38 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 354.7 \text{ kg/s} = 782 \text{ lb/s}$

BPR = 5.1 OPR = 28.9

FPR = TET = °K

Cruise:

$T_{cr} = 24376 \text{ N}$

$= 5480 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 32.8

$M_{cr} = 0.8, h_{cr} = 10670 \text{ m}$

CFM56-9

Manufacturer: CFM International : GE + Snecma

Application: A316/A317 (A31X), BRJ-X, AE-100, N-2130 (not produced)

Composition: 1 / 2B / 9 / 1 / - / 3

Nb of shafts = 2

$D_{fan} = \text{m} = \text{in}$ $D = 1.422 \text{ m}$

$L = 2.329 \text{ m}$

$W_{eng} = 1929 \text{ kg} = 4253 \text{ lb}$ $= 56 \text{ in}$

$= 91.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 88964 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 20000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.08 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.38 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 282 \text{ kg/s} = 621.7 \text{ lb/s}$

BPR = 5.08 OPR = 23.2

FPR = TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

CJ610-1

Manufacturer: GE : General Electric

Application: Learjet 23, HFB 320, 1121A Commdore

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.45 m$

$W_{eng} = 181 kg = 399 lb$ $= 17.7 in$

Static Sea Level:

$T_{ssl} = 12677 N$ $T_{ssl}^{AB} = N$

$= 2850 lbf$ $= lbf$

$SFC_{ssl} = 2.8 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.99 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 1.298 m$

$= 51.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ610-4

Manufacturer: GE : General Electric

Application: Learjet 23/24

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.45 m$

$W_{eng} = 176 kg = 388 lb$ $= 17.7 in$

Static Sea Level:

$T_{ssl} = 12677 N$ $T_{ssl}^{AB} = N$

$= 2850 lbf$ $= lbf$

$SFC_{ssl} = 2.8 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.99 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 1.153 m$

$= 45.4 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ610-5

Manufacturer: GE : General Electric

Application: HFB 320, 1121B/1122 Commodore

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.45 m$

$W_{eng} = 182 kg = 401 lb$ $= 17.7 in$

Static Sea Level:

$T_{ssl} = 13122 N$ $T_{ssl}^{AB} = N$

$= 2950 lbf$ $= lbf$

$SFC_{ssl} = 2.78 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.98 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR = 6.8

FPR = TET = °K

Nb of shafts = 1

$L = 1.298 m$

$= 51.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ610-6

Manufacturer: GE : General Electric

Application: Learjet 24B/D, Learjet 24C (not produced)

Composition: - / - / 8 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 0.45 \text{ m}$

$L = 1.153 \text{ m}$

$W_{eng} = 178 \text{ kg} = 392 \text{ lb}$ $= 17.7 \text{ in}$

$= 45.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 13122 \text{ N}$ $T_{ssl}^{AB} = N$

$= 2950 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.78 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.98 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$

BPR = OPR = 6.8

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ610-8

Manufacturer: GE : General Electric

Application: HFB 320

Composition: - / - / 8 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 0.45 \text{ m}$

$L = 1.153 \text{ m}$

$W_{eng} = 185 \text{ kg} = 408 \text{ lb}$ $= 17.7 \text{ in}$

$= 45.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 13122 \text{ N}$ $T_{ssl}^{AB} = N$

$= 2950 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ610-8A

Manufacturer: GE : General Electric

Application: Learjet 24E/F/25B/25C/25D/28/29

Composition: - / - / 8 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 0.45 \text{ m}$

$L = 1.153 \text{ m}$

$W_{eng} = 185 \text{ kg} = 408 \text{ lb}$ $= 17.7 \text{ in}$

$= 45.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 13122 \text{ N}$ $T_{ssl}^{AB} = N$

$= 2950 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ610-9

Manufacturer: GE : General Electric

Application: HFB 320, 1123 Commodore

Composition: - / - / 8 / 2 / - / -

 $D_{fan} = m = in$ $D = 0.45 \text{ m}$
 $W_{eng} = 189 \text{ kg} = 417 \text{ lb}$ $= 17.7 \text{ in}$

Static Sea Level:

 $T_{ssl} = 13789 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 3100 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 2.83 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 1 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$

BPR = OPR = 6.8

FPR = TET = °K

Nb of shafts = 1

 $L = 1.298 \text{ m}$
 $= 51.1 \text{ in}$

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$
CJ805-21

Manufacturer: GE : General Electric

Year: 1960

Application:

Composition: / / / /

 $D_{fan} = 0.813 \text{ m} = 32 \text{ in}$ $D = m$
 $W_{eng} = 1680 \text{ kg} = 3704 \text{ lb}$ $= in$

Static Sea Level:

 $T_{ssl} = 66708 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 14997 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 188 \text{ kg/s} = 414.5 \text{ lb/s}$

BPR = 1.5 OPR = 12

FPR = TET = °K

Nb of shafts =

 $L = 3.66 \text{ m}$
 $= 144.1 \text{ in}$

Cruise:

 $T_{cr} = 12753 \text{ N}$
 $= 2867 \text{ lbf}$
 $SFC_{cr} = 2.15 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.76 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = 0.8 , h_{cr} = 11000 \text{ m}$
CJ805-23B

Manufacturer: GE : General Electric

Application: Convair CV-990/-990A

Composition: 1 aft / - / 17 / 3 / - / 1

 $D_{fan} = m = in$ $D = m$
 $W_{eng} = \text{kg} = \text{lb}$ $= in$

Static Sea Level:

 $T_{ssl} = 71616 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 16100 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.5 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.53 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 77.6 \text{ kg/s} = 171.1 \text{ lb/s}$

BPR = OPR = 13

FPR = TET = °K

Nb of shafts = 2

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$

CJ805-23C

Manufacturer: GE : General Electric

Application: Caravelle 7/10A

Composition: 1 aft / - / 17 / 3 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 71616 \text{ N}$ $T_{ssl}^{AB} = N$

$= 16100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ805-3

Manufacturer: GE : General Electric

Application: Convair CV-880

Composition: 1 aft / - / 17 / 3 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 49820 \text{ N}$ $T_{ssl}^{AB} = N$

$= 11200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ805-3A

Manufacturer: GE : General Electric

Application: Convair CV-880

Composition: 1 aft / - / 17 / 3 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 49820 \text{ N}$ $T_{ssl}^{AB} = N$

$= 11200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

CJ805-3B

Manufacturer: GE : General Electric

Application: Convair CV-880

Composition: 1 aft / - / 17 / 3 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 51822 \text{ N}$ $T_{ssl}^{AB} = N$

$= 11650 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Conway RB.80 RCo.11 Mk.101

Manufacturer: Rolls-Royce

Application: Victor B.2

Composition: 7 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.067 \text{ m}$

$W_{eng} = kg = lb$ $= 42 \text{ in}$

Static Sea Level:

$T_{ssl} = 77844 \text{ N}$ $T_{ssl}^{AB} = N$

$= 17500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.3 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.454 \text{ m}$

$= 136 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Conway RB.80 RCo.12 Mk.508

Manufacturer: Rolls-Royce

Application: E-6A

Composition: 7 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.067 \text{ m}$

$W_{eng} = 2061 \text{ kg} = 4544 \text{ lb}$ $= 42 \text{ in}$

Static Sea Level:

$T_{ssl} = 77844 \text{ N}$ $T_{ssl}^{AB} = N$

$= 17500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.73 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 127 \text{ kg/s} = 280 \text{ lb/s}$

BPR = 0.3 OPR = 14.1

FPR = TET = °K

Nb of shafts = 2

$L = 3.363 \text{ m}$

$= 132.4 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Conway RB.80 RCo.17 Mk.201

Manufacturer: Rolls-Royce

Application: Victor B.2A/K.2/SR.2

Composition: 7 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.067 \text{ m}$
 $W_{eng} = kg = lb$ $= 42 \text{ in}$

Static Sea Level:

$T_{ssl} = 91633 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 20600 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR = 0.3$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2
 $L = 3.454 \text{ m}$
 $= 136 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Conway RB.80 RCo.43D Mk.301

Manufacturer: Rolls-Royce

Application: VC.10 C(K).1/K.2/K.3/K.4

Composition: ?? / ?? / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.27 \text{ m}$
 $W_{eng} = 2314 \text{ kg} = 5101 \text{ lb}$ $= 50 \text{ in}$

Static Sea Level:

$T_{ssl} = 96971 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 21800 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2
 $L = 3.912 \text{ m}$
 $= 154 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Conway RCo.12 Mk.508

Manufacturer: Rolls-Royce

Application: B707-420/-420F

Composition: 7 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.067 \text{ m}$
 $W_{eng} = 2061 \text{ kg} = 4544 \text{ lb}$ $= 42 \text{ in}$

Static Sea Level:

$T_{ssl} = 77844 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 17500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 2.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.73 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 127 \text{ kg/s} = 280 \text{ lb/s}$
 $BPR = 0.3$ $OPR = 14.1$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2
 $L = 3.363 \text{ m}$
 $= 132.4 \text{ in}$

Cruise:

$T_{cr} = 20573 \text{ N}$
 $= 4625 \text{ lbf}$
 $SFC_{cr} = 2.33 \cdot 10^{-5} (kg/s)/N$
 $= 0.82 (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = 0.83, h_{cr} = 10973 \text{ m}$

Conway RCo.12 Mk.508A

Manufacturer: Rolls-Royce

Application: B707-420

Composition: 7 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.067$ m

$W_{eng} = 2061$ kg = 4544 lb = 42 in

Static Sea Level:

$T_{ssl} = 80068$ N $T_{ssl}^{AB} = N$

= 18000 lbf = lbf

$SFC_{ssl} = 2.08 \cdot 10^{-5}$ (kg/s)/N $SFC_{ssl}^{AB} = (kg/s)/N$

= 0.74 (lb/h)/lbf = (lb/h)/lbf

$\dot{w}_{ssl} = 129.3$ kg/s = 285.1 lb/s

BPR = 0.3 OPR = 14

FPR = TET = °K

Nb of shafts = 2

$L = 3.363$ m

= 132.4 in

Cruise:

$T_{cr} = 20573$ N

= 4625 lbf

$SFC_{cr} = 2.33 \cdot 10^{-5}$ (kg/s)/N

= 0.82 (lb/h)/lbf

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.83, h_{cr} = 10973$ m

Conway RCo.12 Mk.509

Manufacturer: Rolls-Royce

Application: DC-8-41/-42/-43/-43F

Composition: 7 / - / 9 / 1 / - / 2

$D_{fan} = 0.955$ m = 37.6 in $D = 1.067$ m

$W_{eng} = 2061$ kg = 4544 lb = 42 in

Static Sea Level:

$T_{ssl} = 77844$ N $T_{ssl}^{AB} = N$

= 17500 lbf = lbf

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

= (lb/h)/lbf = (lb/h)/lbf

$\dot{w}_{ssl} = 127$ kg/s = 280 lb/s

BPR = 0.3 OPR = 14.1

FPR = TET = 1315 °K

Nb of shafts = 2

$L = 3.363$ m

= 132.4 in

Cruise:

$T_{cr} = 20573$ N

= 4625 lbf

$SFC_{cr} = 2.33 \cdot 10^{-5}$ (kg/s)/N

= 0.82 (lb/h)/lbf

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.83, h_{cr} = 10973$ m

Conway RCo.12 Mk.509A

Manufacturer: Rolls-Royce

Application: DC-8-41/-42/-43/-43F

Composition: 7 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.067$ m

$W_{eng} = 2061$ kg = 4544 lb = 42 in

Static Sea Level:

$T_{ssl} = 80068$ N $T_{ssl}^{AB} = N$

= 18000 lbf = lbf

$SFC_{ssl} = 2.08 \cdot 10^{-5}$ (kg/s)/N $SFC_{ssl}^{AB} = (kg/s)/N$

= 0.74 (lb/h)/lbf = (lb/h)/lbf

$\dot{w}_{ssl} = 129.3$ kg/s = 285.1 lb/s

BPR = 0.3 OPR = 14

FPR = TET = °K

Nb of shafts = 2

$L = 3.363$ m

= 132.4 in

Cruise:

$T_{cr} = 20573$ N

= 4625 lbf

$SFC_{cr} = 2.33 \cdot 10^{-5}$ (kg/s)/N

= 0.82 (lb/h)/lbf

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.83, h_{cr} = 10973$ m

Conway RCo.42 Mk.540

Manufacturer: Rolls-Royce

Application: VC.10 Type 1101/1102/1103/1109

Composition: 4 / 3B / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.27 m$

$W_{eng} = 2268 kg = 5000 lb$ $= 50 in$

Static Sea Level:

$T_{ssl} = 90610 N$ $T_{ssl}^{AB} = N$

$= 20370 lbf$ $= lbf$

$SFC_{ssl} = 1.86 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.66 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 166.5 kg/s = 367.1 lb/s$

BPR = 0.6 OPR = 14.8

FPR = TET = °K

Nb of shafts = 2

$L = 3.912 m$

$= 154 in$

Cruise:

$T_{cr} = 23353 N$

$= 5250 lbf$

$SFC_{cr} = 2.38 \cdot 10^{-5} (kg/s)/N$
 $= 0.84 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.83, h_{cr} = 10973 m$

Conway RCo.42-3

Manufacturer: Rolls-Royce

Year: 1960

Application:

Composition: / / / /

$D_{fan} = 1.142 m = 45 in$ $D = m$

$W_{eng} = 2310 kg = 5093 lb$ $= in$

Static Sea Level:

$T_{ssl} = 97119 N$ $T_{ssl}^{AB} = N$

$= 21833 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 165 kg/s = 363.8 lb/s$

BPR = 0.6 OPR = 15.1

FPR = TET = °K

Nb of shafts =

$L = 3.9 m$

$= 153.5 in$

Cruise:

$T_{cr} = 23740 N$

$= 5337 lbf$

$SFC_{cr} = 2.32 \cdot 10^{-5} (kg/s)/N$
 $= 0.82 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 11000 m$

Conway RCo.43D Mk.550B

Manufacturer: Rolls-Royce

Application: Super VC.10 Type 1151/1154

Composition: 4 / 4B / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.27 m$

$W_{eng} = 2314 kg = 5101 lb$ $= 50 in$

Static Sea Level:

$T_{ssl} = 96971 N$ $T_{ssl}^{AB} = N$

$= 21800 lbf$ $= lbf$

$SFC_{ssl} = 1.67 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.59 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 170.1 kg/s = 375 lb/s$

BPR = 0.6 OPR = 15.8

FPR = TET = °K

Nb of shafts = 2

$L = 3.912 m$

$= 154 in$

Cruise:

$T_{cr} = 23776 N$

$= 5345 lbf$

$SFC_{cr} = 2.32 \cdot 10^{-5} (kg/s)/N$
 $= 0.82 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.83, h_{cr} = 10973 m$

D-100

Manufacturer: Perm Aviadvigatel - Soloviev

Application:

Composition: 1 / 2B / 13 / 2 / - / 4

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 186824 \text{ N}$ $T_{ssl}^{AB} = N$

$= 42000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 8$ $OPR = 35$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

D-110

Manufacturer: Perm Aviadvigatel - Soloviev

Application:

Composition: 2G / 2B / 13 / 2 / - / 4

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 196121 \text{ N}$ $T_{ssl}^{AB} = N$

$= 44090 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 3$ $OPR = 31$

$FPR = 1$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

D-15

Manufacturer: Perm Aviadvigatel - Soloviev

Application: M-50 'Bounder-A'

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 127485 \text{ N}$ $T_{ssl}^{AB} = N$

$= 28660 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

D-18A

Manufacturer: IL : Instytut Lotnictwa

Application:

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = 0.75 \text{ m} = 29.5 \text{ in}$ $D = 0.9 \text{ m}$

$W_{eng} = 380 \text{ kg} = 838 \text{ lb}$ $= 35.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 17650 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3968 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.1 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.74 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 38.4 \text{ kg/s} = 84.7 \text{ lb/s}$

BPR = 0.7 OPR = 8

FPR = 2.07 TET = °K

Nb of shafts = 2

$L = 1.94 \text{ m}$

$= 76.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

D-18T

Manufacturer: PROGRESS

Year: 1982

Application: AN-124-100 'Condor', AN-225 'Mriya'

Composition: 1 / 7 / 7 / 1 / 1 / 4

$D_{fan} = 2.33 \text{ m} = 91.7 \text{ in}$ $D = 2.936 \text{ m}$

$W_{eng} = 4100 \text{ kg} = 9039 \text{ lb}$ $= 115.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 229794 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 51660 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 765.2 \text{ kg/s} = 1687 \text{ lb/s}$

BPR = 5.6 OPR = 25

FPR = 1.56 TET = 1600 °K

Nb of shafts = 3

$L = 5.4 \text{ m}$

$= 212.6 \text{ in}$

Cruise:

$T_{cr} = 47667 \text{ N}$

$= 10716 \text{ lbf}$

$SFC_{cr} = 1.62 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.57 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 27.5

$M_{cr} = 0.75, h_{cr} = 11003 \text{ m}$

D-18T-1

Manufacturer: PROGRESS

Application: An-218-100

Composition: 1 / 7 / 7 / 1 / 1 / 4

$D_{fan} = 2.33 \text{ m} = 91.7 \text{ in}$ $D = 2.936 \text{ m}$

$W_{eng} = 4100 \text{ kg} = 9039 \text{ lb}$ $= 115.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 214172 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 48148 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.6 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = 5.4 \text{ m}$

$= 212.6 \text{ in}$

Cruise:

$T_{cr} = 51581 \text{ N}$

$= 11596 \text{ lbf}$

$SFC_{cr} = 1.74 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.61 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 11003 \text{ m}$

D-18T-3

Manufacturer: PROGRESS

Application: An-124-100M (proposed)

Composition: 1 / 7 / 7 / 1 / 1 / 4

$D_{fan} = 2.33 \text{ m} = 91.7 \text{ in}$ $D = 2.936 \text{ m}$

$W_{eng} = 4100 \text{ kg} = 9039 \text{ lb}$ $= 115.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 229794 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 51660 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $\text{BPR} =$ $\text{OPR} =$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 3

$L = 5.4 \text{ m}$

$= 212.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

D-18TM

Manufacturer: PROGRESS

Application: An-218 (proposed)

Composition: 1 / 7 / 7 / 1 / 1 / 3

$D_{fan} = \text{m} = \text{in}$ $D = 2.987 \text{ m}$

$W_{eng} = 4750 \text{ kg} = 10472 \text{ lb}$ $= 117.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 248107 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 55777 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 770.2 \text{ kg/s} = 1698 \text{ lb/s}$
 $\text{BPR} = 5.5$ $\text{OPR} =$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 3

$L = 5.702 \text{ m}$

$= 224.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

D-18TR

Manufacturer: PROGRESS

Application: An-218-200/-300 (proposed)

Composition: 1 / 7 / 7 / 1 / 1 / 3

$D_{fan} = \text{m} = \text{in}$ $D = 2.987 \text{ m}$

$W_{eng} = 4750 \text{ kg} = 10472 \text{ lb}$ $= 117.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 269681 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 60627 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $\text{BPR} =$ $\text{OPR} =$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 3

$L = 5.702 \text{ m}$

$= 224.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

D-20

Manufacturer: Perm Aviadvigatel - Soloviev

Application:

Composition: 3 / - / 8 / 1 / - / 2

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 52956 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 11905 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

D-20P

Manufacturer: Perm Aviadvigatel - Soloviev

Year: 1960

Application: Tu-124K/K2/V

Composition: 3 / - / 8 / 1 / - / 2

$D_{fan} = 0.93 \text{ m} = 36.6 \text{ in}$ $D = 0.973 \text{ m}$ $L = 3.302 \text{ m}$
 $W_{eng} = 1468 \text{ kg} = 3236 \text{ lb}$ $= 38.3 \text{ in}$ $= 130 \text{ in}$

Static Sea Level:

$T_{ssl} = 52956 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 11905 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.76 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.62 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 112.9 \text{ kg/s} = 248.9 \text{ lb/s}$
 $BPR = 1$ $OPR = 13.6$
 $FPR = 2.6$ $TET = ^\circ K$

Cruise:

$T_{cr} = 10791 \text{ N}$
 $= 2426 \text{ lbf}$
 $SFC_{cr} = 2.21 \cdot 10^{-5} (kg/s)/N$
 $= 0.78 (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = 0.82 , h_{cr} = 10000 \text{ m}$

D-21A1

Manufacturer: Perm Aviadvigatel - Soloviev

Application: S-21

Composition: 5 / - / 10 / 2 / - / 2

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = 2100 \text{ kg} = 4630 \text{ lb}$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 52266 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 11750 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR = 0.83$ $OPR = 20.2$
 $FPR = 2.99$ $TET = ^\circ K$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

D-30-1

Manufacturer: Perm Aviadvigatel - Soloviev

Application: Tu-134/-134K/-134LK, Tu-134/-134N/-134S 'Crusty'

Composition: 4 / - / 10 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 1.049 m$

$L = 3.983 m$

$W_{eng} = 1550 kg = 3417 lb$ $= 41.3 in$

$= 156.8 in$

Static Sea Level:

$T_{ssl} = 66679 N$ $T_{ssl}^{AB} = N$

$= 14990 lbf$ $= lbf$

$SFC_{ssl} = 1.7 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.6 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 127 kg/s = 280 lb/s$

BPR = 1 OPR = 18.6

FPR = 2.65 TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

D-30-2

Manufacturer: Perm Aviadvigatel - Soloviev

Application: Tu-134A/AK/AN/B/B-1, Tu-134AN/UB-L/UB-K (Tu-134UB-KM) 'Crusty'

Composition: 4 / - / 10 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 66679 N$ $T_{ssl}^{AB} = N$

$= 14990 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 1 OPR =

FPR = 2.65 TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

D-30-3

Manufacturer: Perm Aviadvigatel - Soloviev

Application: Tu-134A-3/B-3/BW, Tu-134Sch/Sch-1/Sch-2/Sch-SL 'Crusty'

Composition: 5 / - / 10 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 1.049 m$

$L = 3.983 m$

$W_{eng} = 1550 kg = 3417 lb$ $= 41.3 in$

$= 156.8 in$

Static Sea Level:

$T_{ssl} = 66679 N$ $T_{ssl}^{AB} = N$

$= 14990 lbf$ $= lbf$

$SFC_{ssl} = 1.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.61 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 127 kg/s = 280 lb/s$

BPR = 1 OPR = 17.7

FPR = 2.65 TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

D-30F6

Manufacturer: Perm Aviadvigatel - Soloviev

Application: MiG-31 'Foxhound-A', S-37 'Berkut'

Composition: 5 / - / 10 / 2 / - / 2

D_{fan} = m = in D = 1.021 m L = 7.041 m
 W_{eng} = 2416 kg = 5326 lb = 40.2 in = 277.2 in

Static Sea Level:

T_{ssl} = 93163 N T_{ssl}^{AB} = 186126 N
 = 20944 lbf = 41843 lbf
 SFC_{ssl} = $2.03 \cdot 10^{-5}$ (kg/s)/N SFC_{ssl}^{AB} = $5.28 \cdot 10^{-5}$ (kg/s)/N
 = 0.72 (lb/h)/lbf = 1.86 (lb/h)/lbf
 \dot{w}_{ssl} = 150.1 kg/s = 330.9 lb/s
 BPR = 0.57 OPR = 21.5
 FPR = 3 TET = °K

Nb of shafts = 2

L = 7.041 m

= 277.2 in

Cruise:

T_{cr} = N

= lbf

SFC_{cr} = (kg/s)/N

= (lb/h)/lbf

\dot{w}_{cr} = kg/s = lb/s

OPR_{cr} =

M_{cr} = , h_{cr} = m

D-30K

Manufacturer: Perm Aviadvigatel - Soloviev

Year:

Application:

Composition: / / / /

D_{fan} = 1.455 m = 57.3 in D = m L = 4.61 m
 W_{eng} = 2150 kg = 4740 lb = in = 181.5 in

Static Sea Level:

T_{ssl} = 112815 N T_{ssl}^{AB} = N
 = 25362 lbf = lbf
 SFC_{ssl} = (kg/s)/N SFC_{ssl}^{AB} = (kg/s)/N
 = 0 (lb/h)/lbf = (lb/h)/lbf
 \dot{w}_{ssl} = 272 kg/s = 599.7 lb/s
 BPR = 2.3 OPR = 20
 FPR = TET = °K

Nb of shafts =

L = 4.61 m

= 181.5 in

Cruise:

T_{cr} = 26978 N

= 6065 lbf

SFC_{cr} = $1.9 \cdot 10^{-5}$ (kg/s)/N

= 0.67 (lb/h)/lbf

\dot{w}_{cr} = kg/s = lb/s

OPR_{cr} =

M_{cr} = 0.8 , h_{cr} = 11000 m

D-30KP

Manufacturer: Perm Aviadvigatel - Soloviev

Application: Il-76T, Il-76 'Candid-A', Il-76K/M 'Candid-B'*

Composition: 3 / - / 11 / 2 / - / 4

D_{fan} = m = in D = m L = m
 W_{eng} = kg = lb = in = in

Static Sea Level:

T_{ssl} = 117699 N T_{ssl}^{AB} = N
 = 26460 lbf = lbf
 SFC_{ssl} = $1.36 \cdot 10^{-5}$ (kg/s)/N SFC_{ssl}^{AB} = (kg/s)/N
 = 0.48 (lb/h)/lbf = (lb/h)/lbf
 \dot{w}_{ssl} = 290.3 kg/s = 640 lb/s
 BPR = 2.42 OPR = 18.4
 FPR = TET = °K

Nb of shafts = 2

L = m

= in

Cruise:

T_{cr} = N

= lbf

SFC_{cr} = (kg/s)/N

= (lb/h)/lbf

\dot{w}_{cr} = kg/s = lb/s

OPR_{cr} =

M_{cr} = , h_{cr} = m

D-30KP-2

Manufacturer: Perm Aviadvigatel - Soloviev

Application: Il-76TD/MDP/LL, Il-76MD/MDK 'Candid-B', Il-76SK/VPK, Il-78/-78M 'Midas'

Composition: 3 / - / 11 / 2 / - / 4

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 117699 \text{ N}$ $T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 26460 \text{ lbf}$ $= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = 2.42

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

D-30KPV

Manufacturer: Perm Aviadvigatel - Soloviev

Application: A-40 'Mermaid'

Composition: 3 / - / 11 / 2 / - / 4

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 117699 \text{ N}$ $T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 26460 \text{ lbf}$ $= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

D-30KU

Manufacturer: Perm Aviadvigatel - Soloviev

Application: Il-62M (Il-62-200)

Composition: 3 / - / 11 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 1.56 \text{ m}$

$L = 5.69 \text{ m}$

$W_{eng} = 2668 \text{ kg} = 5882 \text{ lb}$ $= 61.4 \text{ in}$

$= 224 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 107869 \text{ N}$ $T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 24250 \text{ lbf}$ $= lbf$

$= lbf$

$SFC_{ssl} = 1.4 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.49 (lb/h)/lbf$ $= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 269 \text{ kg/s} = 593 \text{ lb/s}$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = 2.35

OPR = 17.4

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

D-30KU-2

Manufacturer: Perm Aviadvigatel - Soloviev

Year: 1982

Application: Tu-154M, Il-62,96, Il-62M (Il-62-200)

Composition: 3 / - / 11 / 2 / - / 2

$D_{fan} = 1.455 \text{ m} = 57.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 2318 \text{ kg} = 5110 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 106090 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 23850 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 269 \text{ kg/s} = 593 \text{ lb/s}$

BPR = 2.35 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 5.2 \text{ m}$

$= 204.7 \text{ in}$

Cruise:

$T_{cr} = 26970 \text{ N}$

$= 6063 \text{ lbf}$

$SFC_{cr} = 1.98 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.7 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8$, $h_{cr} = \text{m}$

D-30KU-90

Manufacturer: Perm Aviadvigatel - Soloviev

Application:

Composition: 3 / - / 11 / 2 / - / 2

$D_{fan} = \text{m} = \text{in}$ $D = 1.56 \text{ m}$

$W_{eng} = 2400 \text{ kg} = 5291 \text{ lb}$ $= 61.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 117677 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 26455 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.44 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 5.7 \text{ m}$

$= 224.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

D-30P

Manufacturer: Perm Aviadvigatel - Soloviev

Year: 1965

Application:

Composition: / / / / /

$D_{fan} = 0.985 \text{ m} = 38.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 1520 \text{ kg} = 3351 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 66708 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 14997 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 125 \text{ kg/s} = 275.6 \text{ lb/s}$

BPR = 1 OPR = 18.6

FPR = TET = 1300 °K

Nb of shafts =

$L = 3.93 \text{ m}$

$= 154.7 \text{ in}$

Cruise:

$T_{cr} = 12753 \text{ N}$

$= 2867 \text{ lbf}$

$SFC_{cr} = 2.18 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.77 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.75$, $h_{cr} = 11000 \text{ m}$

D-30U-154

Manufacturer: Perm Aviadvigatel - Soloviev

Application: Tu-154M

Composition: 4 / - / 10 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.049$ m

$W_{eng} = 1550$ kg = 3417 lb = 41.3 in

Static Sea Level:

$T_{ssl} = 66679$ N $T_{ssl}^{AB} = N$

= 14990 lbf = lbf

$SFC_{ssl} = 1.7 \cdot 10^{-5}$ (kg/s)/N $SFC_{ssl}^{AB} = (kg/s)/N$

= 0.6 (lb/h)/lbf = (lb/h)/lbf

$\dot{w}_{ssl} = 127$ kg/s = 280 lb/s

BPR = 1 OPR = 18.6

FPR = 2.65 TET = °K

Nb of shafts = 2

$L = 3.983$ m

= 156.8 in

Cruise:

$T_{cr} = N$

= lbf

$SFC_{cr} = (kg/s)/N$

= (lb/h)/lbf

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr}=

$M_{cr} = , h_{cr} = m$

D-36-1

Manufacturer: PROGRESS

Application: An-74

Composition: 1 / 6 / 7 / 1 / 1 / 3

$D_{fan} = m = in$ $D = 1.373$ m

$W_{eng} = 1109$ kg = 2445 lb = 54.1 in

Static Sea Level:

$T_{ssl} = 63743$ N $T_{ssl}^{AB} = N$

= 14330 lbf = lbf

$SFC_{ssl} = 1.02 \cdot 10^{-5}$ (kg/s)/N $SFC_{ssl}^{AB} = (kg/s)/N$

= 0.36 (lb/h)/lbf = (lb/h)/lbf

$\dot{w}_{ssl} = 254.9$ kg/s = 562 lb/s

BPR = 6.3 OPR = 18.7

FPR = TET = °K

Nb of shafts = 3

$L = 3.47$ m

= 136.6 in

Cruise:

$T_{cr} = 15689$ N

= 3527 lbf

$SFC_{cr} = 1.84 \cdot 10^{-5}$ (kg/s)/N

= 0.65 (lb/h)/lbf

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr}=

$M_{cr} = 0.75, h_{cr} = 8001$ m

D-36-3A

Manufacturer: PROGRESS

Application: An-74-200, An-74T-100/-200A, An-74TK-100/200, An-74D-200, An-74VIP, An-72 'Coaler-A', An-74 'Coaler-B'

Composition: 1 / 6 / 7 / 1 / 1 / 3

$D_{fan} = m = in$ $D = 1.373$ m

$W_{eng} = 1109$ kg = 2445 lb = 54.1 in

Static Sea Level:

$T_{ssl} = 63743$ N $T_{ssl}^{AB} = N$

= 14330 lbf = lbf

$SFC_{ssl} = 1.02 \cdot 10^{-5}$ (kg/s)/N $SFC_{ssl}^{AB} = (kg/s)/N$

= 0.36 (lb/h)/lbf = (lb/h)/lbf

$\dot{w}_{ssl} = 254.9$ kg/s = 562 lb/s

BPR = 6.3 OPR = 18.7

FPR = TET = °K

Nb of shafts = 3

$L = 3.47$ m

= 136.6 in

Cruise:

$T_{cr} = N$

= lbf

$SFC_{cr} = (kg/s)/N$

= (lb/h)/lbf

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr}=

$M_{cr} = , h_{cr} = m$

D-36-4A

Manufacturer: PROGRESS

Application: AN-74T-300, An-74TK-300

Composition: 1 / 6 / 7 / 1 / 1 / 3

$D_{fan} = m = in$ $D = 1.373 \text{ m}$
 $W_{eng} = 1109 \text{ kg} = 2445 \text{ lb}$ $= 54.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 63743 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 14330 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/N$ $SFC_{ssl}^{AB} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR = 6.3$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 3

$L = 3.47 \text{ m}$
 $= 136.6 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

D-436K

Manufacturer: PROGRESS

Application: An-71 'Madcap' (not produced)

Composition: 1 / 6 / 7 / 1 / 1 / 3

$D_{fan} = m = in$ $D = m$
 $W_{eng} = \text{kg} = \text{lb}$ $= in$

Static Sea Level:

$T_{ssl} = 73551 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 16535 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.05 \cdot 10^{-5} (\text{kg/s})/N$ $SFC_{ssl}^{AB} = (\text{kg/s})/N$
 $= 0.37 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR = 6.2$ $OPR = 21$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 3

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

D-436T1

Manufacturer: PROGRESS

Year: 1996

Application: Tu-334-100, AN-72,74

Composition: 1 + 1 / 6 / 7 / 1 / 1 / 3

$D_{fan} = 1.373 \text{ m} = 54.1 \text{ in}$ $D = m$
 $W_{eng} = 1450 \text{ kg} = 3197 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 75019 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 16865 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.06 \cdot 10^{-5} (\text{kg/s})/N$ $SFC_{ssl}^{AB} = (\text{kg/s})/N$
 $= 0.37 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 275 \text{ kg/s} = 606.3 \text{ lb/s}$
 $BPR = 4.95$ $OPR = 25.2$
 $FPR =$ $TET = 1550 ^\circ K$

Nb of shafts = 3

$L = 3.03 \text{ m}$
 $= 119.3 \text{ in}$

Cruise:

$T_{cr} = 14710 \text{ N}$
 $= 3307 \text{ lbf}$
 $SFC_{cr} = 1.73 \cdot 10^{-5} (\text{kg/s})/N$
 $= 0.61 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.75 , h_{cr} = 11000 \text{ m}$

D-436T2

Manufacturer: PROGRESS

Application: Tu-334-100D, Tu-354 (Tu-334-200)

Composition: 1 + 1 / 6 / 7 / 1 / 1 / 3

$D_{fan} = 1.373 \text{ m} = 54.1 \text{ in}$ $D = \text{m}$

$W_{eng} = 1450 \text{ kg} = 3197 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 80415 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 18078 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 264.9 \text{ kg/s} = 584 \text{ lb/s}$

$\text{BPR} = 4.9$ $\text{OPR} = 26.2$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

D-436TM

Manufacturer: PROGRESS

Application: Yak-42-200 (Yak-42M) (proposed)

Composition: 1 + 1 / 6 / 7 / 1 / 1 / 3

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = 1450 \text{ kg} = 3197 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 75019 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 16865 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 4.95$ $\text{OPR} = 25.2$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

D-436TP

Manufacturer: PROGRESS

Application: Be-200

Composition: 1 / 6 / 7 / 1 / 1 / 3

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 73551 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 16535 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.05 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.37 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} =$ $\text{OPR} =$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Derwent RB.37 5/17

Manufacturer: Rolls-Royce

Application: C-102 Jetliner

Composition: - / - / / / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16014 N$ $T_{ssl}^{AB} = N$

$= 3600 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Derwent RB.37 Mk.1

Manufacturer: Rolls-Royce

Application: Meteor III

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8896 N$ $T_{ssl}^{AB} = N$

$= 2000 lbf$ $= lbf$

$SFC_{ssl} = 3.33 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.18 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 29 kg/s = 63.9 lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Derwent RB.37 Mk.5

Manufacturer: Rolls-Royce

Application: Meteor F.4/U.15, Nord 1601, I.Ae.27

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24020 N$ $T_{ssl}^{AB} = N$

$= 5400 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 36.3 kg/s = 80 lb/s$

BPR = OPR = 4.3

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Derwent RB.37 Mk.8

Manufacturer: Rolls-Royce

Application: Meteor T.7/F.8/FR.9/PR.10/NF.11/NF.13/U.16/U.21, S.14

Composition: - / - / / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$ $L = m$

$W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 15444 \text{ N}$ $T_{ssl}^{AB} = N$

$= 3472 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Derwent RB.37 Mk.9

Manufacturer: Rolls-Royce

Application: Meteor NF.12/NF.14/NF(T).14/TT.20, Sagittario II

Composition: - / - / / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$ $L = m$

$W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 16014 \text{ N}$ $T_{ssl}^{AB} = N$

$= 3600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

DV-2

Manufacturer: PROGRESS

Application: L-39E/-39MS/-39T/L-59

Composition: 1 / 2B / 7 / 1 / - / 2

Nb of shafts = 2

$D_{fan} = 0.645 \text{ m} = 25.4 \text{ in}$ $D = 1.036 \text{ m}$ $L = 1.721 \text{ m}$

$W_{eng} = 450 \text{ kg} = 992 \text{ lb}$ $= 40.8 \text{ in}$ $= 67.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 21583 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4852 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.59 (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = 49.4 \text{ kg/s} = 108.9 \text{ lb/s}$

BPR = 1.46 OPR = 13.5

FPR = 2.3 TET = 1463 °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

DV-22/AI-22

Manufacturer: PROGRESS

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 37952 N$ $T_{ssl}^{AB} = N$

$= 8532 lbf$ $= lbf$

$SFC_{ssl} = 1.05 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.37 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 140.2 kg/s = 309.1 lb/s$

BPR = 5 OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

DV-2F

Manufacturer: PROGRESS

Application: Yak-130D

Composition: 1 / 2B / 7 / 1 / - / 2

$D_{fan} = 0.645 m = 25.4 in$ $D = m$

$W_{eng} = 630 kg = 1389 lb$ $= in$

Static Sea Level:

$T_{ssl} = 24501 N$ $T_{ssl}^{AB} = 36088 N$

$= 5508 lbf$ $= 8113 lbf$

$SFC_{ssl} = 1.67 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{cr} = (kg/s)/N$
 $= 0.59 (lb/h)/lbf$ $= 2.28 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 53.1 kg/s = 117.1 lb/s$

BPR = 1.46 OPR = 15.5

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

EJ200 Mk.100

Manufacturer: EUROJET

Application: EF-2000, Typhoon

Composition: 3 / - / 5 / 1 / - / 1

$D_{fan} = 0.74 m = 29.1 in$ $D = m$

$W_{eng} = 1037 kg = 2286 lb$ $= in$

Static Sea Level:

$T_{ssl} = 58939 N$ $T_{ssl}^{AB} = 88964 N$

$= 13250 lbf$ $= 20000 lbf$

$SFC_{ssl} = 2.22 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 4.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{cr} = (kg/s)/N$
 $= 0.79 (lb/h)/lbf$ $= 1.67 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 73.9 kg/s = 162.9 lb/s$

BPR = 0.4 OPR = 25

FPR = 4.2 TET = 1755 °K

Nb of shafts = 2

$L = 3.988 m$

$= 157 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

EJ22-1

Manufacturer: Williams

Application: Eclipse 500 (candidate engine)

Composition: ?? / - / ?? / ?? / - / ??

$D_{fan} = m = in$ $D = 0.368 m$

$W_{eng} = 39 kg = 86 lb$ $= 14.5 in$

Static Sea Level:

$T_{ssl} = 3114 N$ $T_{ssl}^{AB} = N$

$= 700 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 1.041 m$

$= 41 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F100-IHI-100

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application: F-15J/DJ

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.181 m$

$W_{eng} = 1442 kg = 3179 lb$ $= 46.5 in$

Static Sea Level:

$T_{ssl} = 65255 N$ $T_{ssl}^{AB} = 103865 N$

$= 14670 lbf$ $= 23350 lbf$

$SFC_{ssl} = 2.08 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$

$= 0.74 (lb/h)/lbf$ $= 2.5 (lb/h)/lbf$

$\dot{w}_{ssl} = 102.1 kg/s = 225.1 lb/s$

BPR = 0.71 OPR = 23

FPR = TET = °K

Nb of shafts = 2

$L = 4.986 m$

$= 196.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F100-IHI-220E

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application: F-15J/DJ

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.181 m$

$W_{eng} = 1464 kg = 3228 lb$ $= 46.5 in$

Static Sea Level:

$T_{ssl} = 65255 N$ $T_{ssl}^{AB} = 104310 N$

$= 14670 lbf$ $= 23450 lbf$

$SFC_{ssl} = 2.07 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.95 \cdot 10^{-5} (kg/s)/N$

$= 0.73 (lb/h)/lbf$ $= 2.1 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 24

FPR = TET = °K

Nb of shafts = 2

$L = 4.986 m$

$= 196.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F100-PW-100

Manufacturer: Pratt & Whitney

Application: F-15

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = 0.884 \text{ m} = 34.8 \text{ in}$ $D = 1.181 \text{ m}$

$W_{eng} = 1375 \text{ kg} = 3031 \text{ lb}$ $= 46.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 65255 \text{ N}$ $T_{ssl}^{AB} = 106001 \text{ N}$

$= 14670 \text{ lbf}$ $= 23830 \text{ lbf}$

$SFC_{ssl} = 2.04 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.72 \text{ (lb/h)/lbf}$ $= 2.5 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 102.1 \text{ kg/s} = 225.1 \text{ lb/s}$

BPR = 0.71 OPR = 24.8

FPR = TET = 1553 °K

Nb of shafts = 2

$L = 4.986 \text{ m}$

$= 196.3 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

F100-PW-200

Manufacturer: Pratt & Whitney

Application: F-16A/B

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = 0.884 \text{ m} = 34.8 \text{ in}$ $D = 1.181 \text{ m}$

$W_{eng} = 1375 \text{ kg} = 3031 \text{ lb}$ $= 46.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 65255 \text{ N}$ $T_{ssl}^{AB} = 106001 \text{ N}$

$= 14670 \text{ lbf}$ $= 23830 \text{ lbf}$

$SFC_{ssl} = 2.03 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5.95 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.72 \text{ (lb/h)/lbf}$ $= 2.1 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 105.2 \text{ kg/s} = 231.9 \text{ lb/s}$

BPR = 0.71 OPR = 25

FPR = TET = 1553 °K

Nb of shafts = 2

$L = 4.986 \text{ m}$

$= 196.3 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

F100-PW-220

Manufacturer: Pratt & Whitney

Application: F-15C/D/E, F-16A/B/C/D, YA-7F, A-7F (not produced)

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = \text{m} = \text{in}$ $D = 1.181 \text{ m}$

$W_{eng} = 1451 \text{ kg} = 3199 \text{ lb}$ $= 46.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 65255 \text{ N}$ $T_{ssl}^{AB} = 106001 \text{ N}$

$= 14670 \text{ lbf}$ $= 23830 \text{ lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = 5.95 \cdot 10^{-5} \text{ (kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= 2.1 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 103.4 \text{ kg/s} = 228 \text{ lb/s}$

BPR = 0.71 OPR = 25

FPR = TET = °K

Nb of shafts = 2

$L = 5.283 \text{ m}$

$= 208 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

F100-PW-220E

Manufacturer: Pratt & Whitney

Application: F-15C/D, F-16A/B/C/D

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.181 m$

$W_{eng} = 1429 kg = 3150 lb$ $= 46.5 in$

Static Sea Level:

$T_{ssl} = 65255 N$ $T_{ssl}^{AB} = 106001 N$

$= 14670 lbf$ $= 23830 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = 5.95 \cdot 10^{-5} (kg/s)/N$

$= (lb/h)/lbf$ $= 2.1 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 25

FPR = TET = °K

Nb of shafts = 2

$L = 4.986 m$

$= 196.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F100-PW-220P

Manufacturer: Pratt & Whitney

Application:

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.181 m$

$W_{eng} = 1526 kg = 3364 lb$ $= 46.5 in$

Static Sea Level:

$T_{ssl} = 74285 N$ $T_{ssl}^{AB} = 120101 N$

$= 16700 lbf$ $= 27000 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.36 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 5.283 m$

$= 208 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F100-PW-229

Manufacturer: Pratt & Whitney

Application: F-15E/I/S, F-16C/D

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = 0.884 m = 34.8 in$ $D = 1.194 m$

$W_{eng} = 1377 kg = 3036 lb$ $= 47 in$

Static Sea Level:

$T_{ssl} = 79178 N$ $T_{ssl}^{AB} = 128998 N$

$= 17800 lbf$ $= 29000 lbf$

$SFC_{ssl} = 2.1 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.81 \cdot 10^{-5} (kg/s)/N$

$= 0.74 (lb/h)/lbf$ $= 2.05 (lb/h)/lbf$

$\dot{w}_{ssl} = 112.5 kg/s = 248 lb/s$

BPR = 0.36 OPR = 32.4

FPR = 3.8 TET = 1755 °K

Nb of shafts = 2

$L = 4.851 m$

$= 191 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} = 23

$M_{cr} = , h_{cr} = m$

F100-PW-229A

Manufacturer: Pratt & Whitney

Application: F-15E/I/S, F-16C/D

Composition: 3 / - / 10 / 2 / - / 2

D_{fan} = m = in D = 1.181 m L = 5.283 m
 W_{eng} = kg = lb = 46.5 in = 208 in

Static Sea Level:

T_{ssl} = 79178 N T_{ssl}^{AB} = 144567 N T_{cr} = N
 = 17800 lbf = 32500 lbf = lbf
 SFC_{ssl} = (kg/s)/N SFC_{ssl}^{AB} = 5.41 10⁻⁵ (kg/s)/N SFC_{cr} = (kg/s)/N
 = (lb/h)/lbf = 1.91 (lb/h)/lbf = (lb/h)/lbf
 \dot{w}_{ssl} = kg/s = lb/s \dot{w}_{cr} = kg/s = lb/s
 BPR = OPR = 35 OPR_{cr} =
 FPR = TET = °K M_{cr} = , h_{cr} = m

F101-GE-100

Manufacturer: GE : General Electric

Application: YB-1A, B-1B

Composition: 2 / - / 9 / 1 / - / 2

D_{fan} = m = in D = m L = m
 W_{eng} = kg = lb = in = in

Static Sea Level:

T_{ssl} = 75619 N T_{ssl}^{AB} = 133446 N T_{cr} = N
 = 17000 lbf = 30000 lbf = lbf
 SFC_{ssl} = 1.61 10⁻⁵ (kg/s)/N SFC_{ssl}^{AB} = 7.67 10⁻⁵ (kg/s)/N SFC_{cr} = (kg/s)/N
 = 0.57 (lb/h)/lbf = 2.71 (lb/h)/lbf = (lb/h)/lbf
 \dot{w}_{ssl} = 158.8 kg/s = 350.1 lb/s \dot{w}_{cr} = kg/s = lb/s
 BPR = 2.1 OPR = 26.5 OPR_{cr} =
 FPR = 2.31 TET = °K M_{cr} = , h_{cr} = m

F101-GE-102

Manufacturer: GE : General Electric

Year: 1983

Application: B-1B, Lockheed U2/TR-1 ?

Composition: 2 / - / 9 / 1 / - / 2

D_{fan} = 1.135 m = 44.7 in D = 1.402 m L = 4.59 m
 W_{eng} = 2018 kg = 4449 lb = 55.2 in = 180.7 in

Static Sea Level:

T_{ssl} = 77355 N T_{ssl}^{AB} = 136916 N T_{cr} = N
 = 17390 lbf = 30780 lbf = lbf
 SFC_{ssl} = 1.59 10⁻⁵ (kg/s)/N SFC_{ssl}^{AB} = 6.97 10⁻⁵ (kg/s)/N SFC_{cr} = (kg/s)/N
 = 0.56 (lb/h)/lbf = 2.46 (lb/h)/lbf = (lb/h)/lbf
 \dot{w}_{ssl} = 161.5 kg/s = 356 lb/s \dot{w}_{cr} = kg/s = lb/s
 BPR = 1.91 OPR = 26.8 OPR_{cr} =
 FPR = 2.31 TET = 1672 °K M_{cr} = , h_{cr} = m

F102-LD-100

Manufacturer: Avco Lycoming

Application: YA-9A, A-10A, S-3A (candidate engines)

Composition: 1 / / 7 + 1C / 2 / - / 2

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 31137 N$

$T_{ssl}^{AB} = N$

$= 7000 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F103-GE-101

Manufacturer: GE : General Electric

Application: KC-10A

Composition: / / / /

$D_{fan} = m = in$

$D = 2.195 m$

Nb of shafts =

$L = 4.394 m$

$W_{eng} = 3977 kg = 8768 lb$

$= 86.4 in$

$= 173 in$

Static Sea Level:

$T_{ssl} = 230022 N$

$T_{ssl}^{AB} = N$

$= 51711 lbf$

$= lbf$

$SFC_{ssl} = 1.13 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.4 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 669.5 kg/s = 1476 lb/s$

BPR = 4.31

OPR = 30.2

FPR =

TET = 1639 °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F104-GA-100

Manufacturer: ASE : AlliedSignal Engines

Application: HU-25A/B/C, GQM-98

Composition: 1 / 5 / 1C / 1 / 3 / 2

$D_{fan} = m = in$

$D = m$

Nb of shafts = 3

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 18015 N$

$T_{ssl}^{AB} = N$

$= 4050 lbf$

$= lbf$

$SFC_{ssl} = 1.25 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.44 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 63.5 kg/s = 140 lb/s$

BPR = 3

OPR = 17

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F107-WR-101

Manufacturer: Williams/Rolls-Royce

Application: Air Launch Cruise Missile AGM-86B/C/D

Composition: 4 / - / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 0.305\ m$

$L = 1.232\ m$

$W_{eng} = 66\ kg = 146\ lb$ $= 12\ in$

$= 48.5\ in$

Static Sea Level:

$T_{ssl} = 2825\ N$ $T_{ssl}^{AB} = N$
 $= 635\ lbf$ $= lbf$

$SFC_{ssl} = 1.94\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.68\ (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 6.2\ kg/s = 13.6\ lb/s$

BPR = 1 OPR = 13.8

FPR = 2.1 TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F107-WR-400

Manufacturer: Williams/Rolls-Royce

Application: BGM-109G, RGM-109A/B/C/D, UGM-109A/B/C/D

Composition: 4 / - / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 0.305\ m$

$L = 0.937\ m$

$W_{eng} = kg = lb$ $= 12\ in$

$= 36.9\ in$

Static Sea Level:

$T_{ssl} = 2669\ N$ $T_{ssl}^{AB} = N$
 $= 600\ lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F107-WR-402

Manufacturer: Williams/Rolls-Royce

Application: RGM-109C-III/D-III, UGM-109C-III/D-III, BGM-109E/F (not produced)

Composition: 4 / - / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 0.305\ m$

$L = 0.937\ m$

$W_{eng} = kg = lb$ $= 12\ in$

$= 36.9\ in$

Static Sea Level:

$T_{ssl} = 3114\ N$ $T_{ssl}^{AB} = N$
 $= 700\ lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F108-CF-100

Manufacturer: CFM International : GE + Snecma

Application: KC-135R Stratotanker

Composition: / / / /

$D_{fan} = m = in$ $D = 1.829 m$
 $W_{eng} = 2091 kg = 4610 lb$ $= 72 in$

Nb of shafts =
 $L = 2.931 m$
 $= 115.4 in$

Static Sea Level:

$T_{ssl} = 96233 N$ $T_{ssl}^{AB} = N$
 $= 21634 lbf$ $= lbf$
 $SFC_{ssl} = 1.03 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.36 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 356.1 kg/s = 785.1 lb/s$
 $BPR = 6$ $OPR =$
 $FPR = 1.5$ $TET = 1493 ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

F109-GA-100

Manufacturer: ASE : AlliedSignal Engines

Application: T-46A, YT-48 (not produced) (see also TFE109-1)

Composition: 2 / - / 2 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.78 m$
 $W_{eng} = 199 kg = 439 lb$ $= 30.7 in$

Nb of shafts = 2
 $L = 1.13 m$
 $= 44.5 in$

Static Sea Level:

$T_{ssl} = 5916 N$ $T_{ssl}^{AB} = N$
 $= 1330 lbf$ $= lbf$
 $SFC_{ssl} = 1.11 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.39 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 20.7$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

F110-GE-100

Manufacturer: GE : General Electric

Application: F-16C/D, A-7F (not produced)

Composition: 3 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.181 m$
 $W_{eng} = 1767 kg = 3896 lb$ $= 46.5 in$

Nb of shafts = 2
 $L = 4.623 m$
 $= 182 in$

Static Sea Level:

$T_{ssl} = 81536 N$ $T_{ssl}^{AB} = 127308 N$
 $= 18330 lbf$ $= 28620 lbf$
 $SFC_{ssl} = 2.11 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.89 \cdot 10^{-5} (kg/s)/N$
 $= 0.74 (lb/h)/lbf$ $= 2.08 (lb/h)/lbf$
 $\dot{w}_{ssl} = 115.2 kg/s = 254 lb/s$
 $BPR = 0.87$ $OPR = 30.4$
 $FPR = 2.98$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

F110-GE-129

Manufacturer: GE : General Electric

Year: 1987

Application: F-15E, F-16C/D

Composition: 3 / - / 9 / 1 / - / 2

Nb of shafts = 2

 $D_{fan} = 0.905 \text{ m} = 35.6 \text{ in}$
 $D = 1.181 \text{ m}$
 $L = 4.62 \text{ m}$
 $W_{eng} = 1805 \text{ kg} = 3979 \text{ lb}$
 $= 46.5 \text{ in}$
 $= 181.9 \text{ in}$

Static Sea Level:

 $T_{ssl} = 75619 \text{ N}$
 $T_{ssl}^{AB} = 128998 \text{ N}$
 $= 17000 \text{ lbf}$
 $= 29000 \text{ lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$
 $SFC_{ssl}^{AB} = 5.38 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $= 1.9 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 122.5 \text{ kg/s} = 270.1 \text{ lb/s}$
 $BPR = 0.76$
 $OPR = 30.7$
 $FPR =$
 $TET = ^\circ\text{K}$

Cruise:

 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$
F110-GE-132

Manufacturer: GE : General Electric

Application: F-16C Block 60

Composition: 3 / - / 9 / 1 / - / 2

Nb of shafts = 2

 $D_{fan} = \text{m} = \text{in}$
 $D = 1.181 \text{ m}$
 $L = 4.62 \text{ m}$
 $W_{eng} = 1837 \text{ kg} = 4050 \text{ lb}$
 $= 46.5 \text{ in}$
 $= 181.9 \text{ in}$

Static Sea Level:

 $T_{ssl} = \text{N}$
 $T_{ssl}^{AB} = 142342 \text{ N}$
 $= \text{lbf}$
 $= 32000 \text{ lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$
 $SFC_{ssl}^{AB} = 5.92 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $= 2.09 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR = 0.76$
 $OPR = 33.3$
 $FPR =$
 $TET = ^\circ\text{K}$

Cruise:

 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$
F110-GE-400

Manufacturer: GE : General Electric

Year: 1992

Application: F-14B/D

Composition: 3 / - / 9 / 1 / - / 2

Nb of shafts = 2

 $D_{fan} = 0.905 \text{ m} = 35.6 \text{ in}$
 $D = 1.181 \text{ m}$
 $L = 5.08 \text{ m}$
 $W_{eng} = 1526 \text{ kg} = 3364 \text{ lb}$
 $= 46.5 \text{ in}$
 $= 200 \text{ in}$

Static Sea Level:

 $T_{ssl} = 75600 \text{ N}$
 $T_{ssl}^{AB} = 124500 \text{ N}$
 $= 16996 \text{ lbf}$
 $= 27989 \text{ lbf}$
 $SFC_{ssl} = 1.86 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $SFC_{ssl}^{AB} = 5.69 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.66 (\text{lb/h})/\text{lbf}$
 $= 2.01 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 121.6 \text{ kg/s} = 268.1 \text{ lb/s}$
 $BPR = 0.87$
 $OPR = 30.3$
 $FPR = 3.2$
 $TET = 1643 ^\circ\text{K}$

Cruise:

 $T_{cr} = \text{N}$
 $= 0 \text{ lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= 0 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

F110-GE-X

Manufacturer: GE : General Electric

Application: Growth demonstrator

Composition: 3 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = 162359 \text{ N}$

$= 22000 \text{ lbf}$ $= 36500 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F110-IHI-129

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application: F-2A/B

Composition: 3 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.181 \text{ m}$

$W_{eng} = 1787 \text{ kg} = 3940 \text{ lb}$ $= 46.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 75619 \text{ N}$ $T_{ssl}^{AB} = 128998 \text{ N}$

$= 17000 \text{ lbf}$ $= 29000 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = 5.38 \cdot 10^{-5} (kg/s)/N$

$= (lb/h)/lbf$ $= 1.9 (lb/h)/lbf$

$\dot{w}_{ssl} = 122.5 \text{ kg/s} = 270.1 \text{ lb/s}$

BPR = 0.76 OPR = 30.7

FPR = TET = °K

Nb of shafts = 2

$L = 4.62 \text{ m}$

$= 181.9 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F112-WR-100

Manufacturer: Williams/Rolls-Royce

Application: AGM-129A, X-36A, X-50A

Composition: 4 / - / 1C / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = 73 \text{ kg} = 161 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 3256 \text{ N}$ $T_{ssl}^{AB} = N$

$= 732 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F117-PW-100

Manufacturer: Pratt & Whitney

Application: C-17A

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = m = in$ $D = 2.146 m$

$W_{eng} = 3221 kg = 7101 lb$ $= 84.5 in$

Static Sea Level:

$T_{ssl} = 185490 N$ $T_{ssl}^{AB} = N$
 $= 41700 lbf$ $= lbf$

$SFC_{ssl} = 0.96 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.34 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 607.8 kg/s = 1340 lb/s$

BPR = 5.8 OPR = 27.6

FPR = TET = °K

Nb of shafts = 2

$L = 3.729 m$

$= 146.8 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F118-GE-100

Manufacturer: GE : General Electric

Application: B-2A

Composition: 3 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.181 m$

$W_{eng} = 1451 kg = 3199 lb$ $= 46.5 in$

Static Sea Level:

$T_{ssl} = 84516 N$ $T_{ssl}^{AB} = N$
 $= 19000 lbf$ $= lbf$

$SFC_{ssl} = 1.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.37 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 130.2 kg/s = 287 lb/s$

BPR = OPR = 35.1

FPR = TET = °K

Nb of shafts = 2

$L = 2.553 m$

$= 100.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F118-GE-101

Manufacturer: GE : General Electric

Application: U-2S

Composition: 3 / - / 9 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.194 m$

$W_{eng} = 1429 kg = 3150 lb$ $= 47 in$

Static Sea Level:

$T_{ssl} = 84516 N$ $T_{ssl}^{AB} = N$
 $= 19000 lbf$ $= lbf$

$SFC_{ssl} = 1.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.37 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 130.2 kg/s = 287 lb/s$

BPR = OPR = 35.1

FPR = TET = °K

Nb of shafts = 2

$L = 2.794 m$

$= 110 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F119-PW-100

Manufacturer: Pratt & Whitney

Application: Raptor F/A-22A, YF-23

Composition: 3 / - / 9 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 155687 N$

$= lbf$ $= 35000 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.45 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F121-WR-100

Manufacturer: Williams/Rolls-Royce

Application:

Composition: 1 / - / 6 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.211 m$

$W_{eng} = 19 kg = 42 lb$ $= 8.3 in$

Static Sea Level:

$T_{ssl} = 667 N$ $T_{ssl}^{AB} = N$

$= 150 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 0.66 m$

$= 26 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F121-WR-110

Manufacturer: Williams/Rolls-Royce

Application:

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.343 m$

$W_{eng} = kg = lb$ $= 13.5 in$

Static Sea Level:

$T_{ssl} = 4448 N$ $T_{ssl}^{AB} = N$

$= 1000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F121-WR-115

Manufacturer: Williams/Rolls-Royce

Application: TAURUS

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.343 m$

$W_{eng} = kg = lb$ $= 13.5 in$

Static Sea Level:

$T_{ssl} = 6672 N$ $T_{ssl}^{AB} = N$

$= 1500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 0.699 m$

$= 27.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F124-GA-100

Manufacturer: ASE : AlliedSignal Engines (Honeywell)

Application: X-45A, L-159A/B

Composition: 3 / - / 4 + 1C / 1 / - / 1

$D_{fan} = m = in$ $D = 0.914 m$

$W_{eng} = 499 kg = 1100 lb$ $= 36 in$

Static Sea Level:

$T_{ssl} = 28024 N$ $T_{ssl}^{AB} = N$

$= 6300 lbf$ $= lbf$

$SFC_{ssl} = 2.29 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.81 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 42.6 kg/s = 93.9 lb/s$

BPR = 0.4 OPR = 19.4

FPR = TET = °K

Nb of shafts = 2

$L = 1.697 m$

$= 66.8 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F124-GA-X

Manufacturer: ASE : AlliedSignal Engines (Honeywell)

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 36119 N$ $T_{ssl}^{AB} = N$

$= 8120 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F124-GA-XX

Manufacturer: ASE : AlliedSignal Engines (Honeywell)

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 51154 N$ $T_{ssl}^{AB} = N$

$= 11500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F125

Manufacturer: ASE : AlliedSignal Engines

Year:

Application: Ching Kuo (IDF)

Composition: / / / /

$D_{fan} = 0.591 m = 23.3 in$ $D = m$

$W_{eng} = 617 kg = 1360 lb$ $= in$

Static Sea Level:

$T_{ssl} = 28000 N$ $T_{ssl}^{AB} = 41100 N$

$= 6295 lbf$ $= 9240 lbf$

$SFC_{ssl} = 2.28 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.83 \cdot 10^{-5} (kg/s)/N$

$= 0.8 (lb/h)/lbf$ $= 2.06 (lb/h)/lbf$

$\dot{w}_{ssl} = 41.9 kg/s = 92.4 lb/s$

BPR = 0.49 OPR = 18.5

FPR = TET = 1645 °K

Nb of shafts =

$L = 3.56 m$

$= 140.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F125-GA-100

Manufacturer: ASE : AlliedSignal Engines (Honeywell)

Application: L-39

Composition: 3 / - / 4 + 1C / 1 / - / 1

$D_{fan} = m = in$ $D = 0.591 m$

$W_{eng} = 617 kg = 1360 lb$ $= 23.3 in$

Static Sea Level:

$T_{ssl} = 26800 N$ $T_{ssl}^{AB} = 41146 N$

$= 6025 lbf$ $= 9250 lbf$

$SFC_{ssl} = 2.27 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.84 \cdot 10^{-5} (kg/s)/N$

$= 0.8 (lb/h)/lbf$ $= 2.06 (lb/h)/lbf$

$\dot{w}_{ssl} = 43.3 kg/s = 95.5 lb/s$

BPR = 0.3 OPR = 18.5

FPR = TET = °K

Nb of shafts = 2

$L = 3.561 m$

$= 140.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F125-GA-X

Manufacturer: ASE : AlliedSignal Engines (Honeywell)

Application:

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = N$

$T_{ssl}^{AB} = 54490 N$

Cruise:

$T_{cr} = N$

$= lbf$

$= 12250 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

F125-GA-XX

Manufacturer: ASE : AlliedSignal Engines (Honeywell)

Application:

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = N$

$T_{ssl}^{AB} = 71171 N$

Cruise:

$T_{cr} = N$

$= lbf$

$= 16000 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

F136-GE-100

Manufacturer: GE : General Electric

Application: F-35A/B/C (proposed)

Composition: 2 / - / ?? / 1 / - / 1

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = N$

$T_{ssl}^{AB} = 177928 N$

Cruise:

$T_{cr} = N$

$= lbf$

$= 40000 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

F137-AD-100

Manufacturer: Allison

Application: RQ-4A (Global Hawk)

Composition: 1 / - / 14 / 3 / - / 2

$D_{fan} = m = in$ $D = 1.105 m$

$W_{eng} = 717 kg = 1581 lb$ $= 43.5 in$

Static Sea Level:

$T_{ssl} = 36876 N$ $T_{ssl}^{AB} = N$

$= 8290 lbf$ $= lbf$

$SFC_{ssl} = 1.11 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.39 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 117.9 kg/s = 259.9 lb/s$

BPR = 5 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 2.705 m$

$= 106.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F199-PW-100

Manufacturer: Pratt & Whitney

Year:

Application: F22 Raptor

Composition: / / / /

$D_{fan} = m = 0 in$ $D = m$

$W_{eng} = 1360 kg = 2998 lb$ $= in$

Static Sea Level:

$T_{ssl} = 98000 N$ $T_{ssl}^{AB} = 156000 N$

$= 22031 lbf$ $= 35070 lbf$

$SFC_{ssl} = 1.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.67 \cdot 10^{-5} (kg/s)/N$
 $= 0.61 (lb/h)/lbf$ $= 2.35 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = 0 lb/s$

BPR = 0.2 OPR =

FPR = TET = °K

Nb of shafts =

$L = 4.826 m$

$= 190 in$

Cruise:

$T_{cr} = N$

$= 0 lbf$

$SFC_{cr} = (kg/s)/N$

$= 0 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F2/1

Manufacturer: Vickers

Application: F9/40 (Meteor prototype)

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8007 N$ $T_{ssl}^{AB} = N$

$= 1800 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F3-IHI-30

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application: T-4

Composition: 2 / - / 5 / 1 / - / 2

$D_{fan} = m = in$ $D = 0.63 m$

$W_{eng} = 208 kg = 459 lb$ $= 24.8 in$

Static Sea Level:

$T_{ssl} = 16369 N$ $T_{ssl}^{AB} = N$

$= 3680 lbf$ $= lbf$

$SFC_{ssl} = 1.98 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.7 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 34 kg/s = 75 lb/s$

$BPR = 0.9$ $OPR = 11$

$FPR = 2.6$ $TET = ^\circ K$

Nb of shafts = 2

$L = 2.007 m$

$= 79 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

F3-IHI-30

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application:

Composition: / / / /

$D_{fan} = 0.56 m = 22 in$ $D = m$

$W_{eng} = 340 kg = 750 lb$ $= in$

Static Sea Level:

$T_{ssl} = 16370 N$ $T_{ssl}^{AB} = N$

$= 3680 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 34 kg/s = 75 lb/s$

$BPR = 0.9$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = 1.34 m$

$= 52.8 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

F401-PW-400

Manufacturer: Pratt & Whitney

Application: XFV-12A, F-14B (not produced)

Composition: 3 / - / 10 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 124950 N$

$= lbf$ $= 28090 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

F402-RR-406A

Manufacturer: Rolls-Royce

Application: AV-8B

Composition: 3 / - / 8 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.219 m$

$W_{eng} = 1796 kg = 3960 lb$ $= 48 in$

Static Sea Level:

$T_{ssl} = 95414 N$ $T_{ssl}^{AB} = N$

$= 21450 lbf$ $= lbf$

$SFC_{ssl} = 2.1 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.74 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 15.3

FPR = TET = °K

Nb of shafts = 2

$L = 3.485 m$

$= 137.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F402-RR-408

Manufacturer: Rolls-Royce

Application: AV-8B, AV-8B+

Composition: 3 / - / 8 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.219 m$

$W_{eng} = 1932 kg = 4259 lb$ $= 48 in$

Static Sea Level:

$T_{ssl} = 105867 N$ $T_{ssl}^{AB} = N$

$= 23800 lbf$ $= lbf$

$SFC_{ssl} = 2.15 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.76 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 208.2 kg/s = 459 lb/s$

BPR = 1.2 OPR = 16.3

FPR = TET = °K

Nb of shafts = 2

$L = 3.485 m$

$= 137.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-100

Manufacturer: GE : General Electric

Application: F-5G (F-20A)

Composition: 3 / - / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 75619 N$

$= lbf$ $= 17000 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 24

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-100D

Manufacturer: GE : General Electric

Application: A-4S, TA-4S

Composition: 3 / - / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.881 m$

$W_{eng} = 826 kg = 1821 lb$ $= 34.7 in$

Static Sea Level:

$T_{ssl} = 48930 N$ $T_{ssl}^{AB} = N$

$= 11000 lbf$ $= lbf$

$SFC_{ssl} = 2.27 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.8 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 24

FPR = TET = °K

Nb of shafts = 2

$L = 2.261 m$

$= 89 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-102

Manufacturer: GE : General Electric

Application: KTX-2

Composition: 3 / - / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.881 m$

$W_{eng} = 1035 kg = 2282 lb$ $= 34.7 in$

Static Sea Level:

$T_{ssl} = 48930 N$ $T_{ssl}^{AB} = 78733 N$

$= 11000 lbf$ $= 17700 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = 4.93 \cdot 10^{-5} (kg/s)/N$

$= (lb/h)/lbf$ $= 1.74 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 26

FPR = TET = °K

Nb of shafts = 2

$L = 4.034 m$

$= 158.8 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-102D

Manufacturer: GE : General Electric

Application: X-45B

Composition: 3 / - / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 48930 N$ $T_{ssl}^{AB} = N$

$= 11000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-400

Manufacturer: GE : General Electric

Application: F/A-18A/B, CF-18A/B Hornet, F-5G, X-29A, X-31A

Composition: 3 / - / 7 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = m = in$ $D = 0.889 \text{ m}$ $L = 3.912 \text{ m}$

$W_{eng} = 996 \text{ kg} = 2196 \text{ lb}$ $= 35 \text{ in}$ $= 154 \text{ in}$

Static Sea Level:

$T_{ssl} = 47151 \text{ N}$ $T_{ssl}^{AB} = 71172 \text{ N}$

$= 10600 \text{ lbf}$ $= 16000 \text{ lbf}$

$SFC_{ssl} = 2.42 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5.24 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.85 \text{ (lb/h)/lbf}$ $= 1.85 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 64.4 \text{ kg/s} = 142 \text{ lb/s}$

BPR = 0.34 OPR = 26

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-400D

Manufacturer: GE : General Electric

Application: A-6F (not produced)

Composition: 3 / - / 7 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$ $L = m$

$W_{eng} = \text{kg} = \text{lb}$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 47151 \text{ N}$ $T_{ssl}^{AB} = N$

$= 10600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 26

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-402

Manufacturer: GE : General Electric

Year: 1991

Application: F/A-18C/D

Composition: 3 / - / 7 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = 0.709 \text{ m} = 27.9 \text{ in}$ $D = 0.884 \text{ m}$ $L = 4.034 \text{ m}$

$W_{eng} = 1035 \text{ kg} = 2282 \text{ lb}$ $= 34.8 \text{ in}$ $= 158.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 53156 \text{ N}$ $T_{ssl}^{AB} = 78733 \text{ N}$

$= 11950 \text{ lbf}$ $= 17700 \text{ lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = 4.93 \cdot 10^{-5} \text{ (kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= 1.74 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 66.2 \text{ kg/s} = 145.9 \text{ lb/s}$

BPR = 0.31 OPR = 26

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = ; h_{cr} = m$

F404-GE-F1D2

Manufacturer: GE : General Electric

Application: F-117A

Composition: 3 / - / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.889 m$

$W_{eng} = 785 kg = 1731 lb$ $= 35 in$

Static Sea Level:

$T_{ssl} = 46884 N$ $T_{ssl}^{AB} = N$

$= 10540 lbf$ $= lbf$

$SFC_{ssl} = 2.29 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.81 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 64.9 kg/s = 143.1 lb/s$

BPR = OPR = 24

FPR = TET = °K

Nb of shafts = 2

$L = 2.108 m$

$= 83 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-F2J3

Manufacturer: GE : General Electric

Application: Tejas (interim engine)

Composition: 3 / - / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 81402 N$

$= lbf$ $= 18300 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 27

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F404-GE-IN20

Manufacturer: GE : General Electric

Application: Tejas

Composition: 3 / - / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 89854 N$

$= lbf$ $= 20200 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F405-RR-400

Manufacturer: Rolls-Royce/Turboméca

Application: T-45A

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.785 m$

$W_{eng} = 568 kg = 1252 lb$ $= 30.9 in$

Static Sea Level:

$T_{ssl} = 23131 N$

$= 5200 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

$L = 1.948 m$

$= 76.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F405-RR-400L

Manufacturer: Rolls-Royce/Turboméca

Application: T-45A

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.785 m$

$W_{eng} = kg = lb$ $= 30.9 in$

Static Sea Level:

$T_{ssl} = 24243 N$

$= 5450 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

$L = 1.948 m$

$= 76.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F405-RR-401

Manufacturer: Rolls-Royce/Turboméca

Application: T-45A

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.785 m$

$W_{eng} = 592 kg = 1305 lb$ $= 30.9 in$

Static Sea Level:

$T_{ssl} = 26000 N$

$= 5845 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 44 kg/s = 97 lb/s$

BPR = 0.8

FPR =

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

$L = 1.948 m$

$= 76.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

F412-GE-400

Manufacturer: GE : General Electric

Application: A-12 (not produced)

Composition: 3 / - / 7 / 1 / - / 2

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 62275 \text{ N}$
 $T_{ssl}^{AB} = N$
 $= 14000 \text{ lbf}$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$

Nb of shafts = 2

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
F414

Manufacturer: GE : General Electric

Year: 1996

Application: F18 E,F

Composition: / / / / /

 $D_{fan} = 0.777 \text{ m} = 30.6 \text{ in}$
 $D = m$
 $W_{eng} = 1110 \text{ kg} = 2447 \text{ lb}$
 $= in$

Static Sea Level:

 $T_{ssl} = 64900 \text{ N}$
 $T_{ssl}^{AB} = 97700 \text{ N}$
 $= 14590 \text{ lbf}$
 $= 21964 \text{ lbf}$
 $SFC_{ssl} = 2.38 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = 5.22 \cdot 10^{-5} (kg/s)/N$
 $= 0.84 (lb/h)/lbf$
 $= 1.84 (lb/h)/lbf$
 $\dot{w}_{ssl} = 78 \text{ kg/s} = 172 \text{ lb/s}$
 $BPR = 0.37$
 $OPR = 30$
 $FPR =$
 $TET = ^\circ K$

Nb of shafts =

 $L = 3.922 \text{ m}$
 $= 154.4 \text{ in}$

Cruise:

 $T_{cr} = N$
 $= 0 \text{ lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= 0 (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
F414-GE-400

Manufacturer: GE : General Electric

Application: F/A-18E/F

Composition: 3 / - / 7 / 1 / - / 1

 $D_{fan} = m = in$
 $D = 0.889 \text{ m}$
 $W_{eng} = kg = lb$
 $= 35 \text{ in}$

Static Sea Level:

 $T_{ssl} = 55603 \text{ N}$
 $T_{ssl}^{AB} = 97860 \text{ N}$
 $= 12500 \text{ lbf}$
 $= 22000 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 76.7 \text{ kg/s} = 169.1 \text{ lb/s}$
 $BPR = 0.4$
 $OPR = 30$
 $FPR =$
 $TET = ^\circ K$

Nb of shafts = 2

 $L = 3.912 \text{ m}$
 $= 154 \text{ in}$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

F415-WR-400**Manufacturer:** Williams/Rolls-Royce**Application:** RGM-109E, UGM-109E**Composition:** 2 / - / 5 / 1 / - / 1 $D_{fan} = m = in$ $D = 0.241 m$ $W_{eng} = kg = lb$ $= 9.5 in$ **Static Sea Level:** $T_{ssl} = 3114 N$ $= 700 lbf$ $SFC_{ssl} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

 $T_{ssl}^{AB} = N$ $= lbf$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

 $L = 0.889 m$ $= 35 in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$ **F415-WR-402****Manufacturer:** Williams/Rolls-Royce**Application:** RGM-109E, UGM-109E**Composition:** 2 / - / 5 / 1 / - / 1 $D_{fan} = m = in$ $D = 0.241 m$ $W_{eng} = kg = lb$ $= 9.5 in$ **Static Sea Level:** $T_{ssl} = 3114 N$ $= 700 lbf$ $SFC_{ssl} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

 $T_{ssl}^{AB} = N$ $= lbf$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

 $L = 0.889 m$ $= 35 in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$ **FJ33-1****Manufacturer:** Williams**Application:** Aerostar, Century Jet, FJ-100, Leopard Six**Composition:** ?? / - / ?? / ?? / - / ?? $D_{fan} = m = in$ $D = 0.483 m$ $W_{eng} = 136 kg = 300 lb$ $= 19 in$ **Static Sea Level:** $T_{ssl} = 5338 N$ $= 1200 lbf$ $SFC_{ssl} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

 $T_{ssl}^{AB} = N$ $= lbf$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

 $L = 1.217 m$ $= 47.9 in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$

FJ33-4
Manufacturer: Williams

Application: S-26 Safire, Javelin Mk.10, D-Jet, Javelin AJT Mk.20, Mk.30

Composition: ?? / - / ?? / ?? / - / ??

Nb of shafts = 2

 $D_{fan} = m = in$
 $D = 0.483\ m$
 $L = 1.217\ m$
 $W_{eng} = 136\ kg = 300\ lb$
 $= 19\ in$
 $= 47.9\ in$
Static Sea Level:
 $T_{ssl} = 5338\ N$
 $T_{ssl}^{AB} = N$
 $= 1200\ lbf$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR = 3.4$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$
Cruise:
 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
FJ44
Manufacturer: Williams/Rolls-Royce

Year: 1992

Application: CitationJet, SJ30

Composition: / / / /

 $D_{fan} = 0.483\ m = 19\ in$
 $D = m$
 $L = 1.021\ m$
 $W_{eng} = 202\ kg = 445\ lb$
 $= in$
 $= 40.2\ in$
Static Sea Level:
 $T_{ssl} = 8452\ N$
 $T_{ssl}^{AB} = N$
 $= 1900\ lbf$
 $= lbf$
 $SFC_{ssl} = 1.3 \cdot 10^{-5}\ (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.46\ (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 28.7\ kg/s = 63.3\ lb/s$
 $BPR = 3.28$
 $OPR = 12.8$
 $FPR = 1.6$
 $TET = 1291\ ^\circ K$
Cruise:
 $T_{cr} = 2669\ N$
 $= 600\ lbf$
 $SFC_{cr} = 2.12 \cdot 10^{-5}\ (kg/s)/N$
 $= 0.75\ (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = 0.7 , h_{cr} = 9144\ m$
FJ44-1A
Manufacturer: Williams/Rolls-Royce

Application: Citation CJ1, SigmaJet, MagnaJet

Composition: 1 / 1B / 1C / 1 / - / 2

 $D_{fan} = 0.531\ m = 20.9\ in$
 $D = m$
 $L = 1.064\ m$
 $W_{eng} = 203\ kg = 448\ lb$
 $= in$
 $= 41.9\ in$
Static Sea Level:
 $T_{ssl} = 8452\ N$
 $T_{ssl}^{AB} = N$
 $= 1900\ lbf$
 $= lbf$
 $SFC_{ssl} = 1.29 \cdot 10^{-5}\ (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.46\ (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 28.6\ kg/s = 63.1\ lb/s$
 $BPR = 3.28$
 $OPR = 12.8$
 $FPR =$
 $TET = ^\circ K$
Cruise:
 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

FJ44-1AP
Manufacturer: Williams/Rolls-Royce

Application: Citation CJ1+

Composition: 1 / 1B / 1C / 1 / - / 2

 $D_{fan} = 0.526 \text{ m} = 20.7 \text{ in}$ $D = \text{m}$
 $W_{eng} = 209 \text{ kg} = 461 \text{ lb}$ $= \text{in}$
Static Sea Level:
 $T_{ssl} = 8740 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 1965 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $\text{BPR} = 2.58$ $\text{OPR} =$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

 $L = 1.052 \text{ m}$
 $= 41.4 \text{ in}$
Cruise:
 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$
FJ44-1C
Manufacturer: Williams/Rolls-Royce

Application: SK60

Composition: 1 / 1B / 1C / 1 / - / 2

 $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$
 $W_{eng} = 203 \text{ kg} = 448 \text{ lb}$ $= \text{in}$
Static Sea Level:
 $T_{ssl} = 6672 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 1500 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 1.3 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.46 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 26.3 \text{ kg/s} = 58 \text{ lb/s}$
 $\text{BPR} = 3.4$ $\text{OPR} = 10.3$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

 $L = 1.064 \text{ m}$
 $= 41.9 \text{ in}$
Cruise:
 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$
FJ44-2A
Manufacturer: Williams/Rolls-Royce

Application: Premier 1, SJ30-2, Citation Eagle II, NauticAir 450

Composition: 1 / 1B / 2 + 1C / 1 / - / 2

 $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$
 $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$
Static Sea Level:
 $T_{ssl} = 10231 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2300 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $\text{BPR} =$ $\text{OPR} =$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

 $L = 1.199 \text{ m}$
 $= 47.2 \text{ in}$
Cruise:
 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

FJ44-2C

Manufacturer: Williams/Rolls-Royce

Application: Citation CJ2, Spirit Wing Learjet 25D

Composition: 1 / 1B / 2 + 1C / 1 / - / 2

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = 1.199 m$

$W_{eng} = kg = lb$

$= in$

$= 47.2 in$

Static Sea Level:

$T_{ssl} = 10676 N$

$T_{ssl}^{AB} = N$

$= 2400 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

FJ44-3A

Manufacturer: Williams/Rolls-Royce

Application: Citation CJ2+, CJ3

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 12540 N$

$T_{ssl}^{AB} = N$

$= 2819 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 2.2

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

FJ44-4A

Manufacturer: Williams/Rolls-Royce

Application: Citation CJ4

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 15120 N$

$T_{ssl}^{AB} = N$

$= 3399 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

FJX-1

Manufacturer: Williams

Application: V-Jet II

Composition: ?? / - / ?? / ?? / - / ??

 $D_{fan} = m = in$
 $D = m$

Nb of shafts = 2

 $L = m$
 $W_{eng} = kg = lb$
 $= in$
 $= in$

Static Sea Level:

 $T_{ssl} = 2402 N$
 $T_{ssl}^{AB} = N$

Cruise:

 $T_{cr} = N$
 $= 540 lbf$
 $= lbf$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

 OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$
FJX-2

Manufacturer: Williams

Application: V-Jet II, Eclipse 500 (candidate engine)

Composition: ?? / - / ?? / ?? / - / ??

Nb of shafts = 2

 $D_{fan} = m = in$
 $D = 0.368 m$
 $L = 1.041 m$
 $W_{eng} = 39 kg = 86 lb$
 $= 14.5 in$
 $= 41 in$

Static Sea Level:

 $T_{ssl} = 3114 N$
 $T_{ssl}^{AB} = N$

Cruise:

 $T_{cr} = N$
 $= 700 lbf$
 $= lbf$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

 OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$
Gabizo

Manufacturer: Turboméca

Application: Mirage II, Etendard II, CM-171, CM-191 (not produced)

Composition: - / - / 1 / 1 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$
 $D = m$
 $L = m$
 $W_{eng} = 364 kg = 802 lb$
 $= in$
 $= in$

Static Sea Level:

 $T_{ssl} = 10765 N$
 $T_{ssl}^{AB} = 14679 N$

Cruise:

 $T_{cr} = N$
 $= 2420 lbf$
 $= 3300 lbf$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 20.4 kg/s = 45 lb/s$
 $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

 OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$

GE1

Manufacturer: GE : General Electric

Application: Technology demonstrator

Composition: - / - / 14 / 2 / - / -

$D_{fan} = m = in$ $D = 0.61 m$

$W_{eng} = kg = lb$ $= 24 in$

Static Sea Level:

$T_{ssl} = 22241 N$ $T_{ssl}^{AB} = N$

$= 5000 lbf$ $= lbf$

$SFC_{ssl} = 1.98 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.7 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 34.9 kg/s = 76.9 lb/s$

BPR = OPR = 11

FPR = TET = °K

Nb of shafts = 1

$L = 1.778 m$

$= 70 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

GE1/10

Manufacturer: GE : General Electric

Application: Technology demonstrator

Composition: 1 / - / 14 / 1 / - / 2

$D_{fan} = m = in$ $D = 0.965 m$

$W_{eng} = kg = lb$ $= 38 in$

Static Sea Level:

$T_{ssl} = 44482 N$ $T_{ssl}^{AB} = 75619 N$

$= 10000 lbf$ $= 17000 lbf$

$SFC_{ssl} = 2.27 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.1 \cdot 10^{-5} (kg/s)/N$
 $= 0.8 (lb/h)/lbf$ $= 1.8 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = 1365+ °K

Nb of shafts = 2

$L = 3.632 m$

$= 143 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

GE1/6

Manufacturer: GE : General Electric

Application: Technology demonstrator

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 70415 N$ $T_{ssl}^{AB} = N$

$= 15830 lbf$ $= lbf$

$SFC_{ssl} = 0.95 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.34 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 8 OPR = 25

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

GE1/J1A1

Manufacturer: GE : General Electric

Application:

Composition: - / - / 14 / 2 / - / -

 $D_{fan} = m = in$
 $D = 0.61 \text{ m}$
 $W_{eng} = kg = lb$
 $= 24 \text{ in}$

Nb of shafts = 1

 $L = 3.556 \text{ m}$
 $= 140 \text{ in}$

Static Sea Level:

 $T_{ssl} = 24465 \text{ N}$
 $T_{ssl}^{AB} = 33362 \text{ N}$
 $= 5500 \text{ lbf}$
 $= 7500 \text{ lbf}$
 $SFC_{ssl} = 1.98 \cdot 10^{-5} \text{ (kg/s)/N}$
 $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.7 \text{ (lb/h)/lbf}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 34.9 \text{ kg/s} = 76.9 \text{ lb/s}$
 $BPR =$
 $OPR = 11$
 $FPR =$
 $TET = ^\circ K$

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
GE4/J5P

Manufacturer: GE : General Electric

Application: B-2707-200/-300 (not produced)

Composition: - / - / 9 / 2 / - / -

 $D_{fan} = m = in$
 $D = 2.273 \text{ m}$
 $W_{eng} = 5126 \text{ kg} = 11301 \text{ lb}$
 $= 89.5 \text{ in}$

Nb of shafts = 1

 $L = 7.823 \text{ m}$
 $= 308 \text{ in}$

Static Sea Level:

 $T_{ssl} = 229082 \text{ N}$
 $T_{ssl}^{AB} = 305147 \text{ N}$
 $= 51500 \text{ lbf}$
 $= 68600 \text{ lbf}$
 $SFC_{ssl} = 2.95 \cdot 10^{-5} \text{ (kg/s)/N}$
 $SFC_{ssl}^{AB} = 5.27 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 1.04 \text{ (lb/h)/lbf}$
 $= 1.86 \text{ (lb/h)/lbf}$
 $\dot{w}_{ssl} = 293 \text{ kg/s} = 646 \text{ lb/s}$
 $BPR =$
 $OPR = 12.5$
 $FPR =$
 $TET = ^\circ K$

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
GE90-110B1

Manufacturer: GE : General Electric

Application: B777-200LR, B777-300ER (option), B777-200F (proposed)

Composition: 1 / 3B / 9 / 2 / - / 6

 $D_{fan} = 3.124 \text{ m} = 123 \text{ in}$
 $D = 3.404 \text{ m}$
 $W_{eng} = 8550 \text{ kg} = 18850 \text{ lb}$
 $= 134 \text{ in}$

Nb of shafts = 2

 $L = 4.897 \text{ m}$
 $= 192.8 \text{ in}$

Static Sea Level:

 $T_{ssl} = 489302 \text{ N}$
 $T_{ssl}^{AB} = N$
 $= 109999 \text{ lbf}$
 $= \text{lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$
 $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR = 7.2$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

GE90-115B**Manufacturer:** GE : General Electric**Application:** B777-300ER, B777-200LR (option)**Composition:** 1 / 3B / 9 / 2 / - / 6 $D_{fan} = 3.124 \text{ m} = 123 \text{ in}$ $D = 3.404 \text{ m}$ $W_{eng} = 8283 \text{ kg} = 18261 \text{ lb}$ $= 134 \text{ in}$ **Static Sea Level:**

$T_{ssl} = 511543 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 114999 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $\text{BPR} = 7.2$ $\text{OPR} = 42$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

 $L = 4.897 \text{ m}$ $= 192.8 \text{ in}$ **Cruise:**

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

GE90-76B**Manufacturer:** GE : General Electric**Application:** B777-200**Composition:** 1 / 3B / 10 / 2 / - / 6 $D_{fan} = 3.124 \text{ m} = 123 \text{ in}$ $D = 3.404 \text{ m}$ $W_{eng} = 7074 \text{ kg} = 15596 \text{ lb}$ $= 134 \text{ in}$ **Static Sea Level:**

$T_{ssl} = 339842 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 76400 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 1377.6 \text{ kg/s} = 3037.1 \text{ lb/s}$
 $\text{BPR} = 8.4$ $\text{OPR} = 39.3$
 $\text{FPR} = 1.65$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

 $L = 4.897 \text{ m}$ $= 192.8 \text{ in}$ **Cruise:**

$T_{cr} = 77844 \text{ N}$
 $= 17500 \text{ lbf}$
 $\text{SFC}_{cr} = 1.54 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.55 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = 0.83, h_{cr} = 10668 \text{ m}$

GE90-85B**Manufacturer:** GE : General Electric**Application:** B777-200/-200ER/-300**Composition:** 1 / 3B / 10 / 2 / - / 6 $D_{fan} = 3.124 \text{ m} = 123 \text{ in}$ $D = 3.404 \text{ m}$ $W_{eng} = 7074 \text{ kg} = 15596 \text{ lb}$ $= 134 \text{ in}$ **Static Sea Level:**

$T_{ssl} = 376763 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 84700 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 0.92 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.32 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 1377.6 \text{ kg/s} = 3037.1 \text{ lb/s}$
 $\text{BPR} = 8.4$ $\text{OPR} = 39.3$
 $\text{FPR} = 1.65$ $\text{TET} = ^\circ\text{K}$

Year: 1995

Nb of shafts = 2

 $L = 4.897 \text{ m}$ $= 192.8 \text{ in}$ **Cruise:**

$T_{cr} = 77844 \text{ N}$
 $= 17500 \text{ lbf}$
 $\text{SFC}_{cr} = 1.47 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.52 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = 0.83, h_{cr} = 10668 \text{ m}$

GE90-90B

Manufacturer: GE : General Electric

Application: B777-200ER, B777-200 (option)

Composition: 1 / 3B / 14 / 2 / - / 6

$D_{fan} = 3.124 \text{ m} = 123 \text{ in}$ $D = 3.404 \text{ m}$

$W_{eng} = 7074 \text{ kg} = 15596 \text{ lb}$ $= 134 \text{ in}$

Static Sea Level:

$T_{ssl} = 400338 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 90000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1449.2 \text{ kg/s} = 3194.9 \text{ lb/s}$

$\text{BPR} = 8.4$ $\text{OPR} = 40$

$\text{FPR} = 1.65$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.897 \text{ m}$

$= 192.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

GE90-92B

Manufacturer: GE : General Electric

Application: B777-200ER, B777-200 (option)

Composition: 1 / 3B / 14 / 2 / - / 6

$D_{fan} = 3.124 \text{ m} = 123 \text{ in}$ $D = 3.404 \text{ m}$

$W_{eng} = 7074 \text{ kg} = 15596 \text{ lb}$ $= 134 \text{ in}$

Static Sea Level:

$T_{ssl} = 409234 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 91999 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1461 \text{ kg/s} = 3221 \text{ lb/s}$

$\text{BPR} = 8.3$ $\text{OPR} = 40$

$\text{FPR} = 1.65$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.897 \text{ m}$

$= 192.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

GE90-94B

Manufacturer: GE : General Electric

Application: B777-200/-200ER/-300

Composition: 1 / 3B / 10 / 2 / - / 6

$D_{fan} = 3.124 \text{ m} = 123 \text{ in}$ $D = 3.404 \text{ m}$

$W_{eng} = 7550 \text{ kg} = 16645 \text{ lb}$ $= 134 \text{ in}$

Static Sea Level:

$T_{ssl} = 416796 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 93699 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 8.7$ $\text{OPR} = 40$

$\text{FPR} = 1.65$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.897 \text{ m}$

$= 192.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

GENx-1A72

Manufacturer: GE : General Electric

Year: 2007

Application: A350-800/-900

Composition: 1 / 4B / 10 / 2 / - / 7

 $D_{fan} = 2.82 \text{ m} = 111 \text{ in}$ $D = 2.85 \text{ m}$ $W_{eng} = \text{kg} = \text{lb}$ $= 112.2 \text{ in}$

Static Sea Level:

 $T_{ssl} = 320000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 71939 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 8.9

OPR = 43

FPR =

TET = °K

Nb of shafts =

 $L = \text{m}$ $= \text{in}$

Cruise:

 $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$ **GENx-1B70**

Manufacturer: GE : General Electric

Year: 2008

Application: B787

Composition: 1 / 4B / 10 / 2 / - / 7

 $D_{fan} = 2.82 \text{ m} = 111 \text{ in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

 $T_{ssl} = 311000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 69916 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 9.6

OPR = 43

FPR =

TET = °K

Nb of shafts =

 $L = \text{m}$ $= \text{in}$

Cruise:

 $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$ **GENx-2B67**

Manufacturer: GE : General Electric

Year: 2009

Application: B747 Advanced

Composition: 1 / 3B / 10 / 2 / - / 6

 $D_{fan} = 2.64 \text{ m} = 103.9 \text{ in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

 $T_{ssl} = 298000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 66993 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 8

OPR = 45

FPR =

TET = °K

Nb of shafts =

 $L = \text{m}$ $= \text{in}$

Cruise:

 $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$

Ghost 101

Manufacturer: De Havilland

Application: Vampire FB.1/NF.2/NF.3/FB.4

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 22508 \text{ N}$ $T_{ssl}^{AB} = N$

$= 5060 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 2.89 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 1.02 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 39.5 \text{ kg/s} = 87.1 \text{ lb/s}$

$BPR =$ $OPR = 4.5$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Ghost 103

Manufacturer: De Havilland

Application: Venom FB.1, Venom NF.2/NF.2A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 21574 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4850 \text{ lbf}$ $= lbf$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Ghost 104

Manufacturer: De Havilland

Application: Venom NF.3, Sea Venom F(AW).20/F(AW).21

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 22019 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4950 \text{ lbf}$ $= lbf$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Ghost 105

Manufacturer: De Havilland

Application: Sea Venom F(AW).22/F(AW).53

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 23575 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 5300 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Ghost 48

Manufacturer: De Havilland

Application: Aquilon

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = 912 \text{ kg} = 2011 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 21574 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 4850 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 2.89 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.02 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 38 \text{ kg/s} = 83.8 \text{ lb/s}$
 $BPR =$ $OPR = 4.3$
 $FPR =$ $TET = 1073 ^\circ K$

Nb of shafts = 1

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Ghost 50

Manufacturer: De Havilland

Application: XJ 29

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 19572 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 4400 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Ghost 50 Mk.1

Manufacturer: De Havilland

Application: Comet 1

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 22241 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 5000 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Ghost 50 Mk.2

Manufacturer: De Havilland

Application: Comet 1A

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 22330 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 5020 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Goblin DGu.1

Manufacturer: De Havilland

Application: Meteor prototype, Meteor F.2, F.9/40

Composition: - / - / / / - / -

$D_{fan} = m = in$

$D = m$

Nb of shafts = 1

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 12010 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 2700 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Goblin DGu.2

Manufacturer: De Havilland

Application: Vampire F.1/F.3/FB.5/FB.9/NF.10/FB.20

Composition: - / - / / - / -

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 13789 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 3100 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Goblin DGu.3

Manufacturer: De Havilland

Application: D.H. 108, Meteor F.2, Vampire FB.5/FB.6/FB.50/FB.52/FB.53, G.80-1B/-2B/-3B

Composition: - / - / / - / -

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 14901 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 3350 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

GP7168

Manufacturer: Engine Alliance : GE + P&W + 0...

Application: B747-500X/-600X (not produced)

Composition: 1 / 3B / 9 / 2 / - / 4

$D_{fan} = m = in$ $D = 2.515 \text{ m}$ $L = 4.293 \text{ m}$
 $W_{eng} = 5216 \text{ kg} = 11499 \text{ lb}$ $= 99 \text{ in}$ $= 169 \text{ in}$

Static Sea Level:

$T_{ssl} = 302478 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 68000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 907.2 \text{ kg/s} = 2000 \text{ lb/s}$
 $BPR = 7$ $OPR = 42.3$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

GP7172

Manufacturer: Engine Alliance : GE + P&W + 0...

Application: B767-400ERX, (not produced)

Composition: 1 / 3B / 9 / 2 / - / 4

$D_{fan} = 2.946 \text{ m} = 116 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 315822 \text{ N}$

$= 71000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 8.7

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 43.9

TET = °K

Nb of shafts = 2

$L = 4.75 \text{ m}$

$= 187 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

GP7176

Manufacturer: Engine Alliance : GE + P&W + 0...

Application:

Composition: / / / /

$D_{fan} = 2.946 \text{ m} = 116 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 338000 \text{ N}$

$= 75985 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 8.7

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 43.9

TET = °K

Nb of shafts =

$L = 4.75 \text{ m}$

$= 187 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

GP7268

Manufacturer: Engine Alliance : GE + P&W + 0...

Year: 2005

Application: A380-800

Composition: 1 / 5B / 9 / 2 / - / 6

$D_{fan} = 2.946 \text{ m} = 116 \text{ in}$ $D = \text{m}$

$W_{eng} = 5216 \text{ kg} = 11499 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 302478 \text{ N}$

$= 68000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 907 \text{ kg/s} = 1999.6 \text{ lb/s}$

BPR = 8

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 46

TET = °K

Nb of shafts = 2

$L = 4.29 \text{ m}$

$= 168.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

GP7270

Manufacturer: Engine Alliance : GE + P&W + 0...

Year: 2005

Application: A380-861

Composition: 1 / 5B / 9 / 2 / - / 6

$D_{fan} = 2.946 \text{ m} = 116 \text{ in}$ $D = 3.15 \text{ m}$

$W_{eng} = \text{kg} = \text{lb}$ $= 124 \text{ in}$

Static Sea Level:

$T_{ssl} = 311374 \text{ N}$

$= 70000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 8.7

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 45.6

TET = °K

Nb of shafts = 2

$L = 4.752 \text{ m}$

$= 187.1 \text{ in}$

Cruise:

$T_{cr} = 56194 \text{ N}$

$= 12633 \text{ lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

GP7277

Manufacturer: Engine Alliance : GE + P&W + 0...

Year: 2005

Application: A380-863F

Composition: 1 / 5B / 9 / 2 / - / 6

$D_{fan} = 2.946 \text{ m} = 116 \text{ in}$ $D = 3.15 \text{ m}$

$W_{eng} = 6033 \text{ kg} = 13300 \text{ lb}$ $= 124 \text{ in}$

Static Sea Level:

$T_{ssl} = 342511 \text{ N}$

$= 77000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1179.3 \text{ kg/s} = 2599.9 \text{ lb/s}$

BPR = 8.7

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 45.6

TET = °K

Nb of shafts = 2

$L = 4.752 \text{ m}$

$= 187.1 \text{ in}$

Cruise:

$T_{cr} = 60940 \text{ N}$

$= 13700 \text{ lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

Gyron 1

Manufacturer: Bristol Siddeley

Application: Prototype

Composition: - / - / 7 / ?? / - / -

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 88964 \text{ N}$

$= 20000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 145.1 \text{ kg/s} = 319.9 \text{ lb/s}$

BPR =

FPR =

$T_{ssl}^{AB} = 120101 \text{ N}$

$= 27000 \text{ lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 1

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Gyron Junior DGJ.10

Manufacturer: Bristol Siddeley

Application: Buccaneer S.1, Bristol Type 188

Composition: - / - / 7 / ?? / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 48930 N$ $T_{ssl}^{AB} = 62364 N$

$= 11000 lbf$ $= 14020 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

HO-10

Manufacturer: PZL Rzeszów

Application: TS-11A

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7651 N$ $T_{ssl}^{AB} = N$

$= 1720 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

HTF7000

Manufacturer: Honeywell

Application: Challenger 300

Composition: / / / / /

$D_{fan} = 0.84 m = 33.1 in$ $D = m$

$W_{eng} = 619 kg = 1364 lb$ $= in$

Static Sea Level:

$T_{ssl} = 30400 N$ $T_{ssl}^{AB} = N$

$= 6834 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 4.4 OPR = 28.2

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Year: 2005

Iroquois PS-13

Manufacturer: Orenda

Application: CF-105 (not produced)

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 86295 \text{ N}$ $T_{ssl}^{AB} = 116098 \text{ N}$

$= 19400 \text{ lbf}$ $= 26100 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J100-CA-100

Manufacturer: Teledyne CAE

Application: AQM-34P/Q/R

Composition: - / - / 2 + 1C / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = 191 \text{ kg} = 421 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 12010 \text{ N}$ $T_{ssl}^{AB} = N$

$= 2700 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20.4 \text{ kg/s} = 45 \text{ lb/s}$

BPR = OPR = 6.3

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J101-GE-100

Manufacturer: GE : General Electric

Application: YF-17

Composition: 3/5?? / - / 7/2?? / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 41146 \text{ N}$ $T_{ssl}^{AB} = 63609 \text{ N}$

$= 9250 \text{ lbf}$ $= 14300 \text{ lbf}$

$SFC_{ssl} = 2.22 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.33 \cdot 10^{-5} (kg/s)/N$

$= 0.79 (lb/h)/lbf$ $= 1.88 (lb/h)/lbf$

$\dot{w}_{ssl} = 58.1 \text{ kg/s} = 128.1 \text{ lb/s}$

BPR = 0.25 OPR = 21

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J104-AD-100

Manufacturer: Allison

Application:

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = 0.295 m$

$W_{eng} = 19 kg = 42 lb$ $= 11.6 in$

Static Sea Level:

$T_{ssl} = 2157 N$ $T_{ssl}^{AB} = N$

$= 485 lbf$ $= lbf$

$SFC_{ssl} = 3.51 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.24 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = 0.495 m$

$= 19.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J3-IHI-3

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application: T-1B

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 11788 N$ $T_{ssl}^{AB} = N$

$= 2650 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J3-IHI-7C

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application: T-1C, P-2J (boosters)

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 13700 N$ $T_{ssl}^{AB} = N$

$= 3080 lbf$ $= lbf$

$SFC_{ssl} = 2.83 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 25.4 kg/s = 56 lb/s$

BPR =

OPR = 4.5

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J3-IHI-8

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application:

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 15191 N$ $T_{ssl}^{AB} = N$

$= 3415 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J30-WE-19

Manufacturer: Westinghouse

Application:

Composition: - / - / 10 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = kg = lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 6072 N$ $T_{ssl}^{AB} = N$

$= 1365 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 2.388 m$

$= 94 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J30-WE-19A

Manufacturer: Westinghouse

Application:

Composition: - / - / 10 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = kg = lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 6072 N$ $T_{ssl}^{AB} = N$

$= 1365 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 2.388 m$

$= 94 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J30-WE-20

Manufacturer: Westinghouse

Application: FH-1

Composition: - / - / 10 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = kg = lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 7117 N$ $T_{ssl}^{AB} = N$

$= 1600 lbf$ $= lbf$

$SFC_{ssl} = 3.26 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.15 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 13.6 kg/s = 30 lb/s$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

$L = 2.388 m$

$= 94 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J31-GE-1

Manufacturer: GE : General Electric

Application: YP-59A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.054 m$

$W_{eng} = 392 kg = 864 lb$ $= 41.5 in$

Static Sea Level:

$T_{ssl} = 7162 N$ $T_{ssl}^{AB} = N$

$= 1610 lbf$ $= lbf$

$SFC_{ssl} = 3.48 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.23 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 15 kg/s = 33.1 lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Nb of shafts = 1

$L = 1.829 m$

$= 72 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J31-GE-3

Manufacturer: GE : General Electric

Application: P-59A, FR-1, XA-26F, XF2R-1

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.054 m$

$W_{eng} = 392 kg = 864 lb$ $= 41.5 in$

Static Sea Level:

$T_{ssl} = 7162 N$ $T_{ssl}^{AB} = N$

$= 1610 lbf$ $= lbf$

$SFC_{ssl} = 3.48 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.23 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 15 kg/s = 33.1 lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Nb of shafts = 1

$L = 1.829 m$

$= 72 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J31-GE-5

Manufacturer: GE : General Electric

Application: XP-59A, P-59A/B

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.054 m$

$W_{eng} = 392 kg = 864 lb$ $= 41.5 in$

Static Sea Level:

$T_{ssl} = 6895 N$ $T_{ssl}^{AB} = N$

$= 1550 lbf$ $= lbf$

$SFC_{ssl} = 3.54 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.25 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Nb of shafts = 1

$L = 1.829 m$

$= 72 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J31-GE-7

Manufacturer: GE : General Electric

Application:

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.054 m$

$W_{eng} = 392 kg = 864 lb$ $= 41.5 in$

Static Sea Level:

$T_{ssl} = 6895 N$ $T_{ssl}^{AB} = N$

$= 1550 lbf$ $= lbf$

$SFC_{ssl} = 3.54 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.25 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Nb of shafts = 1

$L = 1.829 m$

$= 72 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J32-WE-5

Manufacturer: Westinghouse

Application:

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 1223 N$ $T_{ssl}^{AB} = N$

$= 275 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-10

Manufacturer: Allison

Application: AJ-1/-1P/-2/-2P

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = kg = lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = N$

$= 4600 lbf$ $= lbf$

$SFC_{ssl} = 3.18 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 40 kg/s = 88.2 lb/s$

BPR = OPR = 4.4

FPR = TET = 953 °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-13

Manufacturer: Allison

Application:

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 850 kg = 1874 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 17014 N$ $T_{ssl}^{AB} = N$

$= 3825 lbf$ $= lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-16

Manufacturer: Allison

Application: F9F-4, XF-92A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = kg = lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 27801 N$ $T_{ssl}^{AB} = 30915 N$

$= 6250 lbf$ $= 6950 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-16A

Manufacturer: Allison

Application: F9F-7

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = kg = lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 28246 N$ $T_{ssl}^{AB} = 30915 N$

$= 6350 lbf$ $= 6950 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

J33-A-17

Manufacturer: Allison

Application: P-80A/B, XP-80R

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 850 kg = 1874 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 17014 N$ $T_{ssl}^{AB} = N$

$= 3825 lbf$ $= lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.1

FPR =

TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

J33-A-17A

Manufacturer: Allison

Application: P-80A/B

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 850 kg = 1874 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 17014 N$ $T_{ssl}^{AB} = 20017 N$

$= 3825 lbf$ $= 4500 lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.1

FPR =

TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

J33-A-18A

Manufacturer: Allison

Application: BQM-6C, RGM-6A/B

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = kg = lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = N$

$= 4600 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-19

Manufacturer: Allison

Application: XAJ-2

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 810 kg = 1786 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = 24020 N$

$= 4600 lbf$ $= 5400 lbf$

$SFC_{ssl} = 3.26 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.15 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-21

Manufacturer: Allison

Application: P-80B, XF-92A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 839 kg = 1850 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 17014 N$ $T_{ssl}^{AB} = 20017 N$

$= 3825 lbf$ $= 4500 lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-23

Manufacturer: Allison

Application: P-80C, QF-80C, RF-80C, XF-92A, TF-80C, TV-1/-2, T2V, CT-133

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 1.283 m$

$L = 2.718 m$

$W_{eng} = 814 kg = 1795 lb$ $= 50.5 in$

$= 107 in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = 24020 N$

$= 4600 lbf$ $= 5400 lbf$

$SFC_{ssl} = 3.23 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.14 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-25

Manufacturer: Allison

Application: RF-80A

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 1.283 m$

$L = 2.614 m$

$W_{eng} = 814 kg = 1795 lb$ $= 50.5 in$

$= 102.9 in$

Static Sea Level:

$T_{ssl} = 23353 N$ $T_{ssl}^{AB} = 27579 N$

$= 5250 lbf$ $= 6200 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-27

Manufacturer: Allison

Application: F-80E (not produced)

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 1.283 m$

$L = 2.235 m$

$W_{eng} = 810 kg = 1786 lb$ $= 50.5 in$

$= 88 in$

Static Sea Level:

$T_{ssl} = 26022 N$ $T_{ssl}^{AB} = 28913 N$

$= 5850 lbf$ $= 6500 lbf$

$SFC_{ssl} = 3 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.06 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-29

Manufacturer: Allison

Application: XF-92A, XF-90, F-80D (not produced)

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 998 kg = 2200 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 24910 N$ $T_{ssl}^{AB} = 33362 N$

$= 5600 lbf$ $= 7500 lbf$

$SFC_{ssl} = 3.26 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$

$= 1.15 (lb/h)/lbf$ $= 2.5 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Nb of shafts = 1

$L = 5.182 m$

$= 204 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-31

Manufacturer: Allison

Application: XSSM-A-3

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 797 kg = 1757 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = N$

$= 4600 lbf$ $= lbf$

$SFC_{ssl} = 3.2 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.13 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Nb of shafts = 1

$L = 2.235 m$

$= 88 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-33

Manufacturer: Allison

Application: F-94A/B

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.252 m$

$W_{eng} = 1084 kg = 2390 lb$ $= 49.3 in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = 26689 N$

$= 4600 lbf$ $= 6000 lbf$

$SFC_{ssl} = 3.26 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$

$= 1.15 (lb/h)/lbf$ $= 2.5 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 5.461 m$

$= 215 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-33A

Manufacturer: Allison

Application: F-94A/B, YF-94D

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.252 m$

$W_{eng} = 1084 kg = 2390 lb$ $= 49.3 in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = 26689 N$

$= 4600 lbf$ $= 6000 lbf$

$SFC_{ssl} = 3.26 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$

$= 1.15 (lb/h)/lbf$ $= 2.5 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 5.461 m$

$= 215 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-35

Manufacturer: Allison

Application: P-80C, RF-80C, T2V

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 814 kg = 1795 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = 24020 N$

$= 4600 lbf$ $= 5400 lbf$

$SFC_{ssl} = 3.23 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.14 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 2.718 m$

$= 107 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-37

Manufacturer: Allison

Application: MGM-1/-1A/-1B/-1C

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = N$

$= 4600 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-41

Manufacturer: Allison

Application: CGM-13A/B, MGM-13A/B/C

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 23353 N$ $T_{ssl}^{AB} = N$

$= 5250 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-6

Manufacturer: Allison

Application: XF9F-1

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 17793 N$ $T_{ssl}^{AB} = N$

$= 4000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-8

Manufacturer: Allison

Application: F9F-3

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = N$

$= 4600 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-A-9

Manufacturer: Allison

Application: YP-80A, P-80A, XFP-80A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 \text{ m}$
 $W_{eng} = 805 \text{ kg} = 1775 \text{ lb}$ $= 50.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 17014 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3825 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 3.46 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 1.22 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR = 4.1$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 2.614 \text{ m}$
 $= 102.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

J33-A-9A

Manufacturer: Allison

Application: RF-80A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 \text{ m}$
 $W_{eng} = 805 \text{ kg} = 1775 \text{ lb}$ $= 50.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 17014 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3825 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 3.46 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 1.22 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR = 4.1$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 2.614 \text{ m}$
 $= 102.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

J33-A-9B

Manufacturer: Allison

Application: RF-80A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 \text{ m}$
 $W_{eng} = 853 \text{ kg} = 1881 \text{ lb}$ $= 50.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 17014 \text{ N}$ $T_{ssl}^{AB} = 20017 \text{ N}$
 $= 3825 \text{ lbf}$ $= 4500 \text{ lbf}$
 $SFC_{ssl} = 3.46 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 1.22 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR = 4.1$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 2.614 \text{ m}$
 $= 102.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

J33-GE-11

Manufacturer: GE : General Electric

Application: P-80A, RF-80A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 805 kg = 1775 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 17014 N$ $T_{ssl}^{AB} = N$

$= 3825 lbf$ $= lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-GE-11A

Manufacturer: GE : General Electric

Application: RF-80A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 805 kg = 1775 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 17014 N$ $T_{ssl}^{AB} = N$

$= 3825 lbf$ $= lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-GE-11B

Manufacturer: GE : General Electric

Application: RF-80A

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 807 kg = 1779 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 17014 N$ $T_{ssl}^{AB} = 20017 N$

$= 3825 lbf$ $= 4500 lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J33-GE-15

Manufacturer: GE : General Electric

Application:

Composition: - / - / 1C / 1 / - / -

 $D_{fan} = m = in$ $D = 1.283 m$ $W_{eng} = 805 kg = 1775 lb$ $= 50.5 in$

Static Sea Level:

 $T_{ssl} = 17014 N$ $T_{ssl}^{AB} = N$ $= 3825 lbf$ $= lbf$ $SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

 $L = 2.614 m$ $= 102.9 in$

Cruise:

 $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$ **J34-IHI-34**

Manufacturer: Westinghouse

Application: P-7J (boost engines)

Composition: - / - / 11 / 2 / - / -

 $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$

Static Sea Level:

 $T_{ssl} = 14457 N$ $T_{ssl}^{AB} = N$ $= 3250 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

 $L = m$ $= in$

Cruise:

 $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$ **J34-WE-22**

Manufacturer: Westinghouse

Application: F2H-1, XF3D-1, XF6U-1, XF-85

Composition: - / - / 11 / 2 / - / -

 $D_{fan} = m = in$ $D = 0.65 m$ $W_{eng} = 537 kg = 1184 lb$ $= 25.6 in$

Static Sea Level:

 $T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$ $= 3000 lbf$ $= lbf$ $SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

 $L = 3.028 m$ $= 119.2 in$

Cruise:

 $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ OPR_{cr} = $M_{cr} = , h_{cr} = m$

J34-WE-30

Manufacturer: Westinghouse

Application: F2H-1, F6U-1/-1P

Composition: - / - / 11 / 2 / - / -

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Nb of shafts = 1

 $L = m$
 $= in$

Static Sea Level:

 $T_{ssl} = 14012\ N$
 $T_{ssl}^{AB} = 18682\ N$
 $= 3150\ lbf$
 $= 4200\ lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
J34-WE-30A

Manufacturer: Westinghouse

Application: F6U-1/-1P

Composition: - / - / 11 / 2 / - / -

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Nb of shafts = 1

 $L = m$
 $= in$

Static Sea Level:

 $T_{ssl} = 14012\ N$
 $T_{ssl}^{AB} = 18682\ N$
 $= 3150\ lbf$
 $= 4200\ lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
J34-WE-32

Manufacturer: Westinghouse

Application: F3D-1/-1M, F7U-1, XF2Y-1, F7U-2 (not produced)

Composition: - / - / 11 / 2 / - / -

 $D_{fan} = m = in$
 $D = 0.65\ m$
 $W_{eng} = 770\ kg = 1698\ lb$
 $= 25.6\ in$

Nb of shafts = 1

 $L = 4.674\ m$
 $= 184\ in$

Static Sea Level:

 $T_{ssl} = 14990\ N$
 $T_{ssl}^{AB} = 21796\ N$
 $= 3370\ lbf$
 $= 4900\ lbf$
 $SFC_{ssl} = 3.06 \cdot 10^{-5}\ (kg/s)/N$
 $SFC_{ssl}^{AB} = 7.37 \cdot 10^{-5}\ (kg/s)/N$
 $= 1.08\ (lb/h)/lbf$
 $= 2.6\ (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR = 4.1$
 $FPR =$
 $TET = ^\circ K$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J34-WE-34

Manufacturer: Westinghouse

Application: F2H-2/-2B/-2N/-2P/-3, F3D-1, P2V-5F/-6F/-7/-7LP/-7S/-7U (boost engines)

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$

$D = m$

Nb of shafts = 1

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 14457 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 3250 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J34-WE-36

Manufacturer: Westinghouse

Application: F3D-2/-2M/-2Q/-2T/-2T2

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$

$D = m$

Nb of shafts = 1

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 15124 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 3400 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J34-WE-36A

Manufacturer: Westinghouse

Application: F3D-2, RB-69A, F3D-3 (not produced)

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$

$D = m$

Nb of shafts = 1

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 15124 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 3400 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J34-WE-38

Manufacturer: Westinghouse

Application: F2H-4

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16903 N$ $T_{ssl}^{AB} = N$

$= 3800 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J34-WE-42

Manufacturer: Westinghouse

Application: F2Y-1 (not produced)

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 15124 N$ $T_{ssl}^{AB} = 18682 N$

$= 3400 lbf$ $= 4200 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J34-WE-46

Manufacturer: Westinghouse

Application:

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 15124 N$ $T_{ssl}^{AB} = N$

$= 3400 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J34-WE-48

Manufacturer: Westinghouse

Application:

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 15124 N$ $T_{ssl}^{AB} = N$

$= 3400 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-11

Manufacturer: Allison

Application: B-45A

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1114 kg = 2456 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 3.683 m$

$= 145 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-13

Manufacturer: Allison

Application:

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1114 kg = 2456 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 3.683 m$

$= 145 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-13A

Manufacturer: Allison

Application:

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 0.953 m$

$W_{eng} = 1114 kg = 2456 lb$ $= 37.5 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$
 $= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 3.683 m$

$= 145 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-13B

Manufacturer: Allison

Application:

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 0.953 m$

$W_{eng} = 1114 kg = 2456 lb$ $= 37.5 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$
 $= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 3.683 m$

$= 145 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-13C

Manufacturer: Allison

Application: P-84C

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 0.953 m$

$W_{eng} = 1114 kg = 2456 lb$ $= 37.5 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$
 $= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 3.683 m$

$= 145 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-15

Manufacturer: Allison

Application: YP-84, XP-89

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1089 kg = 2401 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$
 $= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4

FPR =

TET = °K

Nb of shafts = 1

$L = 4.267 m$

$= 168 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-15C

Manufacturer: Allison

Application: P-84B/C, F-84KX

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1089 kg = 2401 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$
 $= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4

FPR =

TET = °K

Nb of shafts = 1

$L = 4.267 m$

$= 168 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-17

Manufacturer: Allison

Application: X-5, XF4D-1

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1025 kg = 2260 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 21796 N$ $T_{ssl}^{AB} = N$
 $= 4900 lbf$ $= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.7

FPR =

TET = °K

Nb of shafts = 1

$L = 3.734 m$

$= 147 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-17A

Manufacturer: Allison

Application:

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1025 kg = 2260 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 21796 N$ $T_{ssl}^{AB} = N$

$= 4900 lbf$ $= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.7

FPR = TET = °K

Nb of shafts = 1

$L = 3.734 m$

$= 147 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-17B

Manufacturer: Allison

Application:

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1025 kg = 2260 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 21796 N$ $T_{ssl}^{AB} = N$

$= 4900 lbf$ $= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.7

FPR = TET = °K

Nb of shafts = 1

$L = 3.734 m$

$= 147 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-17C

Manufacturer: Allison

Application:

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1025 kg = 2260 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 21796 N$ $T_{ssl}^{AB} = N$

$= 4900 lbf$ $= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.7

FPR = TET = °K

Nb of shafts = 1

$L = 3.734 m$

$= 147 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-17D

Manufacturer: Allison

Application: F-84D/E

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1025 kg = 2260 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 21796 N$ $T_{ssl}^{AB} = N$

$= 4900 lbf$ $= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.7

FPR = TET = °K

Nb of shafts = 1

$L = 3.734 m$

$= 147 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-19

Manufacturer: Allison

Application: YRB-49, RB-35B (not produced)

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1002 kg = 2209 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 21796 N$ $T_{ssl}^{AB} = N$

$= 4900 lbf$ $= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.7

FPR = TET = °K

Nb of shafts = 1

$L = 3.734 m$

$= 147 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-2

Manufacturer: Allison

Application: FJ-1

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-21

Manufacturer: Allison

Application: YF-89A, F-89A/B/C

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016\ m$

$W_{eng} = 1195\ kg = 2635\ lb$ $= 40\ in$

Static Sea Level:

$T_{ssl} = 22908\ N$ $T_{ssl}^{AB} = 30248\ N$

$= 5150\ lbf$ $= 6800\ lbf$

$SFC_{ssl} = 3.14\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08\ 10^{-5}\ (kg/s)/N$

$= 1.11\ (lb/h)/lbf$ $= 2.5\ (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.7

FPR =

TET = °K

Nb of shafts = 1

$L = 6.299\ m$

$= 248\ in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-21A

Manufacturer: Allison

Application: F-89A/B/C

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016\ m$

$W_{eng} = 1195\ kg = 2635\ lb$ $= 40\ in$

Static Sea Level:

$T_{ssl} = 22686\ N$ $T_{ssl}^{AB} = 30248\ N$

$= 5100\ lbf$ $= 6800\ lbf$

$SFC_{ssl} = 3.14\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08\ 10^{-5}\ (kg/s)/N$

$= 1.11\ (lb/h)/lbf$ $= 2.5\ (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.7

FPR =

TET = °K

Nb of shafts = 1

$L = 6.299\ m$

$= 248\ in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-25

Manufacturer: Allison

Application: XF-84E (XF-96A)

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 0.953\ m$

$W_{eng} = 1025\ kg = 2260\ lb$ $= 37.5\ in$

Static Sea Level:

$T_{ssl} = 23575\ N$ $T_{ssl}^{AB} = N$

$= 5300\ lbf$ $= lbf$

$SFC_{ssl} = 3.13\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.11\ (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.7

FPR =

TET = °K

Nb of shafts = 1

$L = 3.683\ m$

$= 145\ in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-29

Manufacturer: Allison

Application: F-84G

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24910 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 5600 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-3

Manufacturer: Allison

Application: XB-43

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16681 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 3750 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-33

Manufacturer: Allison

Application: F-89C

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24020 \text{ N}$ $T_{ssl}^{AB} = 32027 \text{ N}$
 $= 5400 \text{ lbf}$ $= 7200 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-33A

Manufacturer: Allison

Application: F-89C/D

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24020 N$ $T_{ssl}^{AB} = 32027 N$

$= 5400 lbf$ $= 7200 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-35

Manufacturer: Allison

Application: F-89D/H/J, F-89G (not produced)

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24198 N$ $T_{ssl}^{AB} = 32027 N$

$= 5440 lbf$ $= 7200 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-35A

Manufacturer: Allison

Application: F-89D/J

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24198 N$ $T_{ssl}^{AB} = 32027 N$

$= 5440 lbf$ $= 7200 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-A-4**Manufacturer:** Allison**Application:** XB-45A**Composition:** - / - / 11 / 1 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 17793 \text{ N}$ $T_{ssl}^{AB} = N$ $= 4000 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **J35-A-41****Manufacturer:** Allison**Application:** F-89D/J**Composition:** - / - / 11 / 1 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 24910 \text{ N}$ $T_{ssl}^{AB} = 32917 \text{ N}$ $= 5600 \text{ lbf}$ $= 7400 \text{ lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **J35-A-5****Manufacturer:** Allison**Application:** YB-49, XP-86**Composition:** - / - / 11 / 1 / - / - $D_{fan} = m = in$ $D = 1.016 \text{ m}$ $W_{eng} = 1089 \text{ kg} = 2401 \text{ lb}$ $= 40 \text{ in}$ **Static Sea Level:** $T_{ssl} = 16681 \text{ N}$ $T_{ssl}^{AB} = N$ $= 3750 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= 1.12 (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR = 4$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = 4.267 \text{ m}$ $= 168 \text{ in}$ **Cruise:** $T_{cr} = N$ $= \text{lbf}$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/\text{lbf}$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

J35-A-9

Manufacturer: Allison

Application: XP-89

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016\ m$

$W_{eng} = 1114\ kg = 2456\ lb$ $= 40\ in$

Static Sea Level:

$T_{ssl} = 16681\ N$ $T_{ssl}^{AB} = N$

$= 3750\ lbf$ $= lbf$

$SFC_{ssl} = 3.17\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12\ (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 3.683\ m$

$= 145\ in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-C-3

Manufacturer: Chevrolet

Application: XP-86

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016\ m$

$W_{eng} = 1089\ kg = 2401\ lb$ $= 40\ in$

Static Sea Level:

$T_{ssl} = 16681\ N$ $T_{ssl}^{AB} = N$

$= 3750\ lbf$ $= lbf$

$SFC_{ssl} = 3.17\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12\ (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 4.267\ m$

$= 168\ in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-GE-2

Manufacturer: GE : General Electric

Application: XFJ-1

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16681\ N$ $T_{ssl}^{AB} = N$

$= 3750\ lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-GE-7

Manufacturer: GE : General Electric

Application: XP-84, XB-48

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1089 kg = 2401 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 4.267 m$

$= 168 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J35-GE-9

Manufacturer: GE : General Electric

Application: XB-48

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1114 kg = 2456 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 3.683 m$

$= 145 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J36-AC-1

Manufacturer: Allison

Application: XP-80A

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$

$= 3000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J40-WE-12

Manufacturer: Westinghouse

Application: XA3D-1

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 31137 N$ $T_{ssl}^{AB} = N$

$= 7000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J40-WE-22

Manufacturer: Westinghouse

Application: F3H-1N, F3H-1P (not produced)

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32027 N$ $T_{ssl}^{AB} = 48485 N$

$= 7200 lbf$ $= 10900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J40-WE-22A

Manufacturer: Westinghouse

Application: F3H-1N, F3H-1P (not produced)

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32027 N$ $T_{ssl}^{AB} = 48485 N$

$= 7200 lbf$ $= 10900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J40-WE-6

Manufacturer: Westinghouse

Application: XF3H-1, XF4D-1, XF10F-1

Composition: / / / /

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 30248 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 6800 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J40-WE-8

Manufacturer: Westinghouse

Application: XF3H-1/-1N, XF4D-1, F10F-1 (not produced)

Composition: / / / /

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 32917 \text{ N}$ $T_{ssl}^{AB} = 48485 \text{ N}$
 $= 7400 \text{ lbf}$ $= 10900 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J400-WR-104

Manufacturer: Williams/Rolls-Royce

Application: AGM-154D/E, Griffon-36 (CASOM candidate)

Composition: - / - / 1 + 1C / 1 / - / -

$D_{fan} = m = in$ $D = 0.274 \text{ m}$ $L = 0.495 \text{ m}$
 $W_{eng} = 23 \text{ kg} = 51 \text{ lb}$ $= 10.8 \text{ in}$ $= 19.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 1068 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 240 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 3.4 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.2 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J400-WR-404

Manufacturer: Williams/Rolls-Royce

Application: X-48A, BQM-74C/D/E, MQM-74A/B/C

Composition: - / - / 1 + 1C / 1 / - / -

$D_{fan} = m = in$ $D = 0.274 m$ $L = 0.495 m$
 $W_{eng} = 23 kg = 51 lb$ $= 10.8 in$ $= 19.5 in$

Static Sea Level:

$T_{ssl} = 1068 N$ $T_{ssl}^{AB} = N$
 $= 240 lbf$ $= lbf$
 $SFC_{ssl} = 3.4 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.2 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J402-CA-100-2

Manufacturer: Teledyne CAE

Application: AGM-158A

Composition: / / / / /

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 3025 N$ $T_{ssl}^{AB} = N$
 $= 680 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J402-CA-100-9B

Manufacturer: Teledyne CAE

Application: AGM-158A

Composition: / / / / /

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 3025 N$ $T_{ssl}^{AB} = N$
 $= 680 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J402-CA-400**Manufacturer:** Teledyne CAE**Application:** AGM-84A/B/C/D/E/F/G/H, RGM-84A/B/C/D/E/F, UGM-84A/B/C/D**Composition:** / / / / $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 3025 N$ $T_{ssl}^{AB} = N$ $= 680 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR = 5.6$ $FPR =$ $TET = ^\circ K$

Nb of shafts =

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **J402-CA-401****Manufacturer:** Teledyne CAE**Application:** RGM-109H/E (candidate engine), UGM-84A/B/C/D/E/F/H, UGM-109H/E (candidate engine), AGM-109C/H/I/J/K/L (not produced)**Composition:** / / / / $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 3025 N$ $T_{ssl}^{AB} = N$ $= 680 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR = 5.6$ $FPR =$ $TET = ^\circ K$

Nb of shafts =

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **J402-CA-700****Manufacturer:** Teledyne CAE**Application:** MQM-107A/C, XAGM-130TJ**Composition:** / / / / $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 2847 N$ $T_{ssl}^{AB} = N$ $= 640 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR = 5.5$ $FPR =$ $TET = ^\circ K$

Nb of shafts =

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

J403-MT-400

Manufacturer: Microturbo

Application: C-22L, BQM-126A (not produced)

Composition: - / - / 3 / 1 / - / -

$D_{fan} = m = in$ $D = 0.33 m$

$W_{eng} = 53 kg = 117 lb$ $= 13 in$

Static Sea Level:

$T_{ssl} = 4003 N$ $T_{ssl}^{AB} = N$

$= 900 lbf$ $= lbf$

$SFC_{ssl} = 3.65 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.29 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.9

FPR = TET = °K

Nb of shafts = 1

$L = 0.749 m$

$= 29.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J42-P-6

Manufacturer: Pratt & Whitney

Application: F9F-2

Composition: / / C / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = 778 kg = 1715 lb$ $= in$

Static Sea Level:

$T_{ssl} = 22241 N$ $T_{ssl}^{AB} = 25577 N$

$= 5000 lbf$ $= 5750 lbf$

$SFC_{ssl} = 3.09 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.09 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 40 kg/s = 88.2 lb/s$

BPR = OPR = 4.3

FPR = TET = 1014 °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J42-P-8

Manufacturer: Pratt & Whitney

Application: F9F-2/-2D/-2P

Composition: / / C / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = 778 kg = 1715 lb$ $= in$

Static Sea Level:

$T_{ssl} = 22241 N$ $T_{ssl}^{AB} = 25577 N$

$= 5000 lbf$ $= 5750 lbf$

$SFC_{ssl} = 3.09 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.09 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 40 kg/s = 88.2 lb/s$

BPR = OPR = 4.3

FPR = TET = 1014 °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J44-R-1

Manufacturer: Fairchild

Application:

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

= in

= in

Static Sea Level:

$T_{ssl} = 4448 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

= 1000 lbf

= lbf

= lbf

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

= (lb/h)/lbf

= (lb/h)/lbf

= (lb/h)/lbf

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J46-WE-3

Manufacturer: Westinghouse

Application: F3D-2 (candidate engine), F3D-3 (not produced)

Composition: - / - / 12 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

= in

= in

Static Sea Level:

$T_{ssl} = 18149 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

= 4080 lbf

= lbf

= lbf

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

= (lb/h)/lbf

= (lb/h)/lbf

= (lb/h)/lbf

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J46-WE-4

Manufacturer: Westinghouse

Application:

Composition: - / - / 12 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

= in

= in

Static Sea Level:

$T_{ssl} = 20017 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

= 4500 lbf

= lbf

= lbf

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

= (lb/h)/lbf

= (lb/h)/lbf

= (lb/h)/lbf

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J46-WE-8

Manufacturer: Westinghouse

Application: F7U-3/-3M/-3P

Composition: - / - / 12 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = 27134 N$

$= 4600 lbf$ $= 6100 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J46-WE-8A

Manufacturer: Westinghouse

Application: F7U-3/-3M/-3P

Composition: - / - / 12 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 20462 N$ $T_{ssl}^{AB} = 27134 N$

$= 4600 lbf$ $= 6100 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-1

Manufacturer: GE : General Electric

Application: F-86A

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = 1123 kg = 2476 lb$ $= 39 in$

Static Sea Level:

$T_{ssl} = 21574 N$ $T_{ssl}^{AB} = 25889 N$

$= 4850 lbf$ $= 5820 lbf$

$SFC_{ssl} = 3.12 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 3.26 \cdot 10^{-5} (kg/s)/N$

$= 1.1 (lb/h)/lbf$ $= 1.15 (lb/h)/lbf$

$\dot{w}_{ssl} = 40.8 kg/s = 89.9 lb/s$

BPR = OPR = 4.3

FPR = TET = °K

Nb of shafts = 1

$L = 3.658 m$

$= 144 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-11

Manufacturer: GE : General Electric

Application: B-47A/B

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = 1123 kg = 2476 lb$ $= 39 in$

Nb of shafts = 1

$L = 3.658 m$

$= 144 in$

Static Sea Level:

$T_{ssl} = 23131 N$ $T_{ssl}^{AB} = N$

$= 5200 lbf$ $= lbf$

$SFC_{ssl} = 3.2 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.13 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-13

Manufacturer: GE : General Electric

Application: F-86A, F-86E-1/-5/-6-CAN/-10/-15, B-45A/C, RB-45C, CL-13 Sabre Mk.1/Mk.2/Mk.3/Mk.4, Sabre F.4, XB-51, XfJ-2/-2B

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = 1145 kg = 2524 lb$ $= 39 in$

Nb of shafts = 1

$L = 3.658 m$

$= 144 in$

Static Sea Level:

$T_{ssl} = 23131 N$ $T_{ssl}^{AB} = 26689 N$

$= 5200 lbf$ $= 6000 lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 3.26 \cdot 10^{-5} (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= 1.15 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-15

Manufacturer: GE : General Electric

Application: B-45A/C, RB-45C

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = 0.991 m$

$W_{eng} = 1141 kg = 2515 lb$ $= 39 in$

Nb of shafts = 1

$L = 3.658 m$

$= 144 in$

Static Sea Level:

$T_{ssl} = 23131 N$ $T_{ssl}^{AB} = 26689 N$

$= 5200 lbf$ $= 6000 lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 3.26 \cdot 10^{-5} (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= 1.15 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-17

Manufacturer: GE : General Electric

Application: F-86D-5/-10/-15/-20/-30

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24510 \text{ N}$ $T_{ssl}^{AB} = 32694 \text{ N}$

$= 5510 \text{ lbf}$ $= 7350 \text{ lbf}$

$SFC_{ssl} = 2.86 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5.67 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 1.01 \text{ (lb/h)/lbf}$ $= 2 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 44.9 \text{ kg/s} = 99 \text{ lb/s}$

BPR = OPR = 5.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-17B

Manufacturer: GE : General Electric

Application: F-86D-40/-45

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24510 \text{ N}$ $T_{ssl}^{AB} = 32694 \text{ N}$

$= 5510 \text{ lbf}$ $= 7350 \text{ lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-19

Manufacturer: GE : General Electric

Application: B-36D/J (boosters)

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 23131 \text{ N}$ $T_{ssl}^{AB} = N$

$= 5200 \text{ lbf}$ $= lbf$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-2

Manufacturer: GE : General Electric

Application: FJ-2

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26289 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 5910 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

OPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-21

Manufacturer: GE : General Electric

Application: F-89E/F, XF-90 (not produced)

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 25221 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 5670 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

OPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-23

Manufacturer: GE : General Electric

Application: B-47B, DB-47B, KB-47B, QB-47B, RB-47B, TB-47B, YB-47F

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 25221 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 5670 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

OPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-25

Manufacturer: GE : General Electric

Application: B-47E-I

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 25221 N$

$= 5670 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-25A

Manufacturer: GE : General Electric

Application: B-47E-I/-II/-III, EB-47E, EB-47L, JB-47E, NB-47E, RB-47E/H/K, ERB-47H, ETB-47E

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 25221 N$

$= 5670 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = 32027 N$

$= 7200 lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-27

Manufacturer: GE : General Electric

Application: F-86E-10, F-86F-1/-2/-3/-5/-10/-15/-20/-25/-30/-35/-40, RF-86F, TF-86F

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26289 N$

$= 5910 lbf$

$SFC_{ssl} = 2.56 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.9 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 45.4 kg/s = 100.1 lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR = 5.5

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J47-GE-3

Manufacturer: GE : General Electric

Application: XB-47, XF-91

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = 0.991 \text{ m}$ $L = 3.658 \text{ m}$
 $W_{eng} = 1120 \text{ kg} = 2469 \text{ lb}$ $= 39 \text{ in}$ $= 144 \text{ in}$

Static Sea Level:

$T_{ssl} = 21574 \text{ N}$ $T_{ssl}^{AB} = 25889 \text{ N}$
 $= 4850 \text{ lbf}$ $= 5820 \text{ lbf}$
 $SFC_{ssl} = 3.12 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 3.26 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 1.1 \text{ (lb/h)/lbf}$ $= 1.15 \text{ (lb/h)/lbf}$
 $\dot{w}_{ssl} = 40.8 \text{ kg/s} = 89.9 \text{ lb/s}$
 $BPR =$ $OPR = 4.3$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J47-GE-33

Manufacturer: GE : General Electric

Application: F-86D-45/-50/-55/-60, F-86K, F-86L-50/-55/-60

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 24910 \text{ N}$ $T_{ssl}^{AB} = 34696 \text{ N}$
 $= 5600 \text{ lbf}$ $= 7800 \text{ lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 45.8 \text{ kg/s} = 101 \text{ lb/s}$
 $BPR =$ $OPR = 5.5$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J47-GE-7

Manufacturer: GE : General Electric

Application: F-86A, RF-86A, B-45A, B-45B, F-87A (not produced)

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = 0.94 \text{ m}$ $L = 3.658 \text{ m}$
 $W_{eng} = 1145 \text{ kg} = 2524 \text{ lb}$ $= 37 \text{ in}$ $= 144 \text{ in}$

Static Sea Level:

$T_{ssl} = 22241 \text{ N}$ $T_{ssl}^{AB} = 25889 \text{ N}$
 $= 5000 \text{ lbf}$ $= 5820 \text{ lbf}$
 $SFC_{ssl} = 3.2 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 1.13 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR = 4.3$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J47-GE-9

Manufacturer: GE : General Electric

Application: B-45A, B-45B (not produced)

Composition: - / - / 12 / 1 / - / -

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 22241 N$
 $T_{ssl}^{AB} = 25889 N$
 $= 5000 lbf$
 $= 5820 lbf$
 $SFC_{ssl} = 3.2 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.13 (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.3

FPR =

TET = °K

Nb of shafts = 1

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$
J48-P-2

Manufacturer: Pratt & Whitney

Application: XF9F-5

Composition: - / - / 1C / 1 / - / -

 $D_{fan} = m = in$
 $D = 1.27 m$
 $W_{eng} = 932 kg = 2055 lb$
 $= 50 in$

Nb of shafts = 1

 $L = 5.131 m$
 $= 202 in$

Static Sea Level:

 $T_{ssl} = 27801 N$
 $T_{ssl}^{AB} = 35586 N$
 $= 6250 lbf$
 $= 8000 lbf$
 $SFC_{ssl} = 3.29 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$
 $= 1.16 (lb/h)/lbf$
 $= 2.5 (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.4

FPR =

TET = °K

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$
J48-P-3

Manufacturer: Pratt & Whitney

Application: YF-94C

Composition: - / - / 1C / 1 / - / -

 $D_{fan} = m = in$
 $D = 1.27 m$
 $W_{eng} = 939 kg = 2070 lb$
 $= 50 in$

Nb of shafts = 1

 $L = 5.131 m$
 $= 202 in$

Static Sea Level:

 $T_{ssl} = 27801 N$
 $T_{ssl}^{AB} = 35586 N$
 $= 6250 lbf$
 $= 8000 lbf$
 $SFC_{ssl} = 3.29 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$
 $= 1.16 (lb/h)/lbf$
 $= 2.5 (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 4.4

FPR =

TET = °K

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$

J48-P-4

Manufacturer: Pratt & Whitney

Application:

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 22241 N$ $T_{ssl}^{AB} = N$

$= 5000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J48-P-5

Manufacturer: Pratt & Whitney

Application: F-94C

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28246 N$ $T_{ssl}^{AB} = 36920 N$

$= 6350 lbf$ $= 8300 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J48-P-6

Manufacturer: Pratt & Whitney

Application: F9F-5/-5K/-5KD/-5P, XF9F-6, X/YF-93A (X/YF-86C)

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 27801 N$ $T_{ssl}^{AB} = 31137 N$

$= 6250 lbf$ $= 7000 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J48-P-6A

Manufacturer: Pratt & Whitney

Application: F9F-4(RE), F9F-5/-5K/-5KD/-5P, F9F-6

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 27801\ N$

$= 6250\ lbf$

$T_{ssl}^{AB} = 31137\ N$

$= 7000\ lbf$

Cruise:
 $T_{cr} = N$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J48-P-8

Manufacturer: Pratt & Whitney

Application: F9F-6/-6D/-6K/-6K2/-6P, F9F-7(RE)

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 32249\ N$

$= 7250\ lbf$

$T_{ssl}^{AB} = 37810\ N$

$= 8500\ lbf$

Cruise:
 $T_{cr} = N$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J48-P-8A

Manufacturer: Pratt & Whitney

Application: F9F-6/-6P, F9F-8/-8P/-8T

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 32249\ N$

$= 7250\ lbf$

$T_{ssl}^{AB} = 37810\ N$

$= 8500\ lbf$

Cruise:
 $T_{cr} = N$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J48-P-8B

Manufacturer: Pratt & Whitney

Application: F9F-6/-6P

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32249 \text{ N}$ $T_{ssl}^{AB} = 37810 \text{ N}$

$= 7250 \text{ lbf}$ $= 8500 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J48-P-8C

Manufacturer: Pratt & Whitney

Application: F9F-6/-6P, F9F-8/-8P/-8T

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32249 \text{ N}$ $T_{ssl}^{AB} = 37810 \text{ N}$

$= 7250 \text{ lbf}$ $= 8500 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-P-16

Manufacturer: Pratt & Whitney

Application: F-8C

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 75175 \text{ N}$ $T_{ssl}^{AB} = N$

$= 16900 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-P-3

Manufacturer: Pratt & Whitney

Application: AGM-28A/B

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33362 N$ $T_{ssl}^{AB} = N$

$= 7500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-P-6

Manufacturer: Pratt & Whitney

Application: A4D-5 (A-4E), A-4J, TA-4J, A2F-1 (A-6A)

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.766 m$

$W_{eng} = 933 kg = 2057 lb$ $= 30.2 in$

Static Sea Level:

$T_{ssl} = 37810 N$ $T_{ssl}^{AB} = N$

$= 8500 lbf$ $= lbf$

$SFC_{ssl} = 2.32 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.82 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-P-6A

Manufacturer: Pratt & Whitney

Application: A4D-5 (A-4E), A2F-1 (A-6A), A2F-1Q (EA-6A), A-6B

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.766 m$

$W_{eng} = 933 kg = 2057 lb$ $= 30.2 in$

Static Sea Level:

$T_{ssl} = 37810 N$ $T_{ssl}^{AB} = N$

$= 8500 lbf$ $= lbf$

$SFC_{ssl} = 2.32 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.82 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-P-6B

Manufacturer: Pratt & Whitney

Application: A4D-5 (A-4E)

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 37810 N$ $T_{ssl}^{AB} = N$

$= 8500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-P-8

Manufacturer: Pratt & Whitney

Application: A-6C, KA-6D

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.766 m$

$W_{eng} = 961 kg = 2119 lb$ $= 30.2 in$

Static Sea Level:

$T_{ssl} = 41368 N$ $T_{ssl}^{AB} = N$

$= 9300 lbf$ $= lbf$

$SFC_{ssl} = 2.44 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.86 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 13

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-P-8A

Manufacturer: Pratt & Whitney

Application: A-4F/G/H/K, EA-4F, TA-4F/G/H/K, A-6B, EA-6B prototypes, Super Mystère B2

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.766 m$

$W_{eng} = 961 kg = 2119 lb$ $= 30.2 in$

Static Sea Level:

$T_{ssl} = 41368 N$ $T_{ssl}^{AB} = N$

$= 9300 lbf$ $= lbf$

$SFC_{ssl} = 2.44 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.86 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 13

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-P-8B

Manufacturer: Pratt & Whitney

Application: A-6E

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 41368 N$ $T_{ssl}^{AB} = N$

$= 9300 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 13

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-PW-408

Manufacturer: Pratt & Whitney

Application: A-4E, EA-6B, AGM-28

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.814 m$

$W_{eng} = 1051 kg = 2317 lb$ $= 32 in$

Static Sea Level:

$T_{ssl} = 49820 N$ $T_{ssl}^{AB} = N$

$= 11200 lbf$ $= lbf$

$SFC_{ssl} = 2.24 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.79 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 64.9 kg/s = 143.1 lb/s$

BPR = OPR = 14.6

FPR = TET = °K

Nb of shafts = 2

$L = 3.02 m$

$= 118.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-PW-408A

Manufacturer: Pratt & Whitney

Application: A-4KU/M/N, OA-4M, TA-4KU, EA-6B, AGM-28

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 49820 N$ $T_{ssl}^{AB} = N$

$= 11200 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 64.9 kg/s = 143.1 lb/s$

BPR = OPR = 14.6

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J52-PW-409

Manufacturer: Pratt & Whitney

Application: A-6E, EA-6B

Composition: - / 5 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 53378 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 12000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J57-P-10

Manufacturer: Pratt & Whitney

Application: A3D-2 (A-3B), A3D-2P (RA-3B), A3D-2Q (EA-3B), A3D-2T (TA-3B), KA-3B

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 46706 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 10500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J57-P-11

Manufacturer: Pratt & Whitney

Application: YF-102

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$ $T_{ssl}^{AB} = 71171 \text{ N}$
 $= 10000 \text{ lbf}$ $= 16000 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J57-P-12

Manufacturer: Pratt & Whitney

Application: F-8A, TF-8A

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$ $T_{ssl}^{AB} = 71171 \text{ N}$
 $= 10000 \text{ lbf}$ $= 16000 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-12A

Manufacturer: Pratt & Whitney

Application: F-8A, TF-8A

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$ $T_{ssl}^{AB} = 71171 \text{ N}$
 $= 10000 \text{ lbf}$ $= 16000 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-13

Manufacturer: Pratt & Whitney

Application: F-101A/C, RF-101A/C/H, U-2B

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 45372 \text{ N}$ $T_{ssl}^{AB} = 70282 \text{ N}$
 $= 10200 \text{ lbf}$ $= 15800 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-13B

Manufacturer: Pratt & Whitney

Application: U-2B

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 75619 N$
 $= lbf$ $= 17000 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-16

Manufacturer: Pratt & Whitney

Application: F-8C/K

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 47596 N$ $T_{ssl}^{AB} = 75175 N$
 $= 10700 lbf$ $= 16900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-17

Manufacturer: Pratt & Whitney

Application: F-106A/B, SM-62A

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 51154 N$ $T_{ssl}^{AB} = 108981 N$
 $= 11500 lbf$ $= 24500 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-19W

Manufacturer: Pratt & Whitney

Application: B-52B/C/D/E, NB-52B, RB-52B

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 46706 \text{ N}$ $T_{ssl}^{AB} = 53823 \text{ N}$

$= 10500 \text{ lbf}$ $= 12100 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 12.5

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-2

Manufacturer: Pratt & Whitney

Application: F4D-1

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 43148 \text{ N}$ $T_{ssl}^{AB} = 60051 \text{ N}$

$= 9700 \text{ lbf}$ $= 13500 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-20

Manufacturer: Pratt & Whitney

Application: F-8D, RF-8G, TF-8A

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = 0.988 \text{ m}$

$W_{eng} = 2155 \text{ kg} = 4751 \text{ lb}$ $= 38.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 47596 \text{ N}$ $T_{ssl}^{AB} = 80068 \text{ N}$

$= 10700 \text{ lbf}$ $= 18000 \text{ lbf}$

$SFC_{ssl} = 2.18 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.93 \cdot 10^{-5} (kg/s)/N$

$= 0.77 (lb/h)/lbf$ $= 2.8 (lb/h)/lbf$

$\dot{w}_{ssl} = 81.6 \text{ kg/s} = 179.9 \text{ lb/s}$

BPR = OPR = 13

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-20A

Manufacturer: Pratt & Whitney

Application: F-8E/H/J

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = 0.988 m$

$W_{eng} = 2155 kg = 4751 lb$ $= 38.9 in$

Static Sea Level:

$T_{ssl} = 47596 N$ $T_{ssl}^{AB} = 83181 N$

$= 10700 lbf$ $= 18700 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 81.6 kg/s = 179.9 lb/s$

BPR = OPR = 13

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-21

Manufacturer: Pratt & Whitney

Application: F-100C/D/F, QF-100

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 45372 N$ $T_{ssl}^{AB} = 75397 N$

$= 10200 lbf$ $= 16950 lbf$

$SFC_{ssl} = 2.18 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.95 \cdot 10^{-5} (kg/s)/N$

$= 0.77 (lb/h)/lbf$ $= 2.1 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-21A

Manufacturer: Pratt & Whitney

Application: F-100C/D/F

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 45372 N$ $T_{ssl}^{AB} = 75397 N$

$= 10200 lbf$ $= 16950 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-22

Manufacturer: Pratt & Whitney

Application: RF-8G

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 47596 N$

$= 10700 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = 80068 N$

$= 18000 lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-23

Manufacturer: Pratt & Whitney

Application: AB, F-100D, YF-102A, F-102A, TF-102A

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 2345 kg = 5170 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 45372 N$

$= 10200 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 74.8 kg/s = 164.9 lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = 71171 N$

$= 16000 lbf$

$SFC_{ssl}^{AB} = 5.95 \cdot 10^{-5} (kg/s)/N$

$= 2.1 (lb/h)/lbf$

OPR = 11.5

TET = 1144 °K

Nb of shafts = 2

$L = 6.25 m$

$= 246.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-25

Manufacturer: Pratt & Whitney

Application: F-102A, PQM-102A, QF-102A, YF-105A

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 45372 N$

$= 10200 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

FPR =

$T_{ssl}^{AB} = 76509 N$

$= 17200 lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-29W

Manufacturer: Pratt & Whitney

Application: B-52B/C/D/E, RB-52B

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 46706 \text{ N}$ $T_{ssl}^{AB} = 53823 \text{ N}$
 $= 10500 \text{ lbf}$ $= 12100 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 12.5$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J57-P-29WA

Manufacturer: Pratt & Whitney

Application: B-52B/C/D/E, RB-52B

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 46706 \text{ N}$ $T_{ssl}^{AB} = 53823 \text{ N}$
 $= 10500 \text{ lbf}$ $= 12100 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 12.5$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J57-P-37A

Manufacturer: Pratt & Whitney

Application: RB-57D

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 48930 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 11000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J57-P-39

Manufacturer: Pratt & Whitney

Application: F-100A/C

Composition: - / 9 / 7 / 1 / - / 2

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 43148 N$
 $T_{ssl}^{AB} = 70282 N$
 $= 9700 lbf$
 $= 15800 lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 2

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
J57-P-43WA

Manufacturer: Pratt & Whitney

Application: B-52E/F

Composition: - / 9 / 7 / 1 / - / 2

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 49820 N$
 $T_{ssl}^{AB} = 61163 N$
 $= 11200 lbf$
 $= 13750 lbf$
 $SFC_{ssl} = 2.18 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = 2.69 \cdot 10^{-5} (kg/s)/N$
 $= 0.77 (lb/h)/lbf$
 $= 0.95 (lb/h)/lbf$
 $\dot{w}_{ssl} = 82.1 kg/s = 181 lb/s$

BPR =

OPR = 12.5

FPR =

TET = °K

Nb of shafts = 2

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
J57-P-43WB

Manufacturer: Pratt & Whitney

Application: B-52G

Composition: - / 9 / 7 / 1 / - / 2

 $D_{fan} = m = in$
 $D = 0.988 m$
 $W_{eng} = 1755 kg = 3869 lb$
 $= 38.9 in$

Static Sea Level:

 $T_{ssl} = 49820 N$
 $T_{ssl}^{AB} = 61163 N$
 $= 11200 lbf$
 $= 13750 lbf$
 $SFC_{ssl} = 2.18 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = 2.69 \cdot 10^{-5} (kg/s)/N$
 $= 0.77 (lb/h)/lbf$
 $= 0.95 (lb/h)/lbf$
 $\dot{w}_{ssl} = 82.1 kg/s = 181 lb/s$

BPR =

OPR = 12.5

FPR =

TET = 1144 °K

Nb of shafts = 2

 $L = 4.249 m$
 $= 167.3 in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} = 16$
 $M_{cr} = , h_{cr} = m$

J57-P-47

Manufacturer: Pratt & Whitney

Application: YF-102C

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 48930 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 11000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-4A

Manufacturer: Pratt & Whitney

Application: F-8B/L, QF-8A, RF-8A

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$ $T_{ssl}^{AB} = 72061 \text{ N}$
 $= 10000 \text{ lbf}$ $= 16200 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-55

Manufacturer: Pratt & Whitney

Application: NF-100A/B, F-101B/F, CF-101B/F, RF-101B/G, TF-101B

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 53334 \text{ N}$ $T_{ssl}^{AB} = 65833 \text{ N}$
 $= 11990 \text{ lbf}$ $= 14800 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-59W

Manufacturer: Pratt & Whitney

Application: C-135A/B/C, EC-135A, KC-135A, RC-135A

Composition: - / 9 / 7 / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 0.988 m$

$L = m$

$W_{eng} = 1960 kg = 4321 lb$ $= 38.9 in$

$= in$

Static Sea Level:

$T_{ssl} = 61163 N$ $T_{ssl}^{AB} = N$

$= 13750 lbf$ $= lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-6

Manufacturer: Pratt & Whitney

Application: A3D-1 (A-3A), YA3D-1P/-1Q

Composition: - / 9 / 7 / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 43148 N$ $T_{ssl}^{AB} = N$

$= 9700 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 12.4

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-6A

Manufacturer: Pratt & Whitney

Application: A3D-1 (A-3A), A3D-1Q (EA-3A)

Composition: - / 9 / 7 / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 43148 N$ $T_{ssl}^{AB} = N$

$= 9700 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 12.4

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-7

Manufacturer: Pratt & Whitney

Application: YF-100A, F-100A/C, RF-100A, U-2A, B-58A (candidate engine)

Composition: - / 9 / 7 / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$ $L = m$

$W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 43148 \text{ N}$ $T_{ssl}^{AB} = 65833 \text{ N}$

$= 9700 \text{ lbf}$ $= 14800 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-7A

Manufacturer: Pratt & Whitney

Application: U-2A

Composition: - / 9 / 7 / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$ $L = m$

$W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 49820 \text{ N}$ $T_{ssl}^{AB} = N$

$= 11200 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-8

Manufacturer: Pratt & Whitney

Application: F4D-1, XF5D-1

Composition: - / 9 / 7 / 1 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$ $L = m$

$W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 45372 \text{ N}$ $T_{ssl}^{AB} = 64499 \text{ N}$

$= 10200 \text{ lbf}$ $= 14500 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J57-P-8A

Manufacturer: Pratt & Whitney

Application: F4D-1

Composition: - / 9 / 7 / 1 / - / 2

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 45372 \text{ N}$
 $T_{ssl}^{AB} = 64499 \text{ N}$
 $= 10200 \text{ lbf}$
 $= 14500 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 13.6

FPR =

TET = °K

Nb of shafts = 2

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$
J57-P-8B

Manufacturer: Pratt & Whitney

Application: F4D-1

Composition: - / 9 / 7 / 1 / - / 2

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 45372 \text{ N}$
 $T_{ssl}^{AB} = 64499 \text{ N}$
 $= 10200 \text{ lbf}$
 $= 14500 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 13.6

FPR =

TET = °K

Nb of shafts = 2

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$
J57-P-9

Manufacturer: Pratt & Whitney

Application: RB-57D, X-16A

Composition: - / 9 / 7 / 1 / - / 2

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 44482 \text{ N}$
 $T_{ssl}^{AB} = N$
 $= 10000 \text{ lbf}$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 2

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$

J57-P-9W

Manufacturer: Pratt & Whitney

Application: B-52A, NB-52A

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Nb of shafts = 2
 $L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$ $T_{ssl}^{AB} = 53823 \text{ N}$
 $= 10000 \text{ lbf}$ $= 12100 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J58-P-4

Manufacturer: Pratt & Whitney

Application: SR-71A/B, YF-12A

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Nb of shafts = 1
 $L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 111205 \text{ N}$ $T_{ssl}^{AB} = 151239 \text{ N}$
 $= 25000 \text{ lbf}$ $= 34000 \text{ lbf}$
 $SFC_{ssl} = 2.27 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.38 \cdot 10^{-5} (kg/s)/N$
 $= 0.8 (lb/h)/lbf$ $= 1.9 (lb/h)/lbf$
 $\dot{w}_{ssl} = 204.1 \text{ kg/s} = 450 \text{ lb/s}$
 $BPR =$ $OPR = 8.8$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J60-P-3

Manufacturer: Pratt & Whitney

Application: T-39A/D/F

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 \text{ m}$
 $W_{eng} = 203 \text{ kg} = 448 \text{ lb}$ $= 21.9 \text{ in}$

Nb of shafts = 1
 $L = 2.019 \text{ m}$
 $= 79.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 13345 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 3000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.96 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 22.7 \text{ kg/s} = 50 \text{ lb/s}$
 $BPR =$ $OPR = 6.5$
 $FPR =$ $TET = 1144 ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J60-P-4

Manufacturer: Pratt & Whitney

Application:

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 m$

$W_{eng} = 212 kg = 467 lb$ $= 21.9 in$

Static Sea Level:

$T_{ssl} = 14679 N$ $T_{ssl}^{AB} = N$

$= 3300 lbf$ $= lbf$

$SFC_{ssl} = 2.82 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.99 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J60-P-5

Manufacturer: Pratt & Whitney

Application: C-140A/B/C

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 m$

$W_{eng} = 203 kg = 448 lb$ $= 21.9 in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$

$= 3000 lbf$ $= lbf$

$SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.96 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 6.5

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J60-P-6

Manufacturer: Pratt & Whitney

Application: T-2B, T-39D

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 m$

$W_{eng} = 225 kg = 496 lb$ $= 21.9 in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$

$= 3000 lbf$ $= lbf$

$SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.96 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 6.5

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J60-P-9

Manufacturer: Pratt & Whitney

Application: RB-57F (boosters)

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 m$

$W_{eng} = kg = lb$ $= 21.9 in$

Static Sea Level:

$T_{ssl} = 14679 N$ $T_{ssl}^{AB} = N$

$= 3300 lbf$ $= lbf$

$SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.96 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 6.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J65-B-3

Manufacturer: Buick

Application: F-84F

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32605 N$ $T_{ssl}^{AB} = N$

$= 7330 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J65-B-7

Manufacturer: Buick

Application: F-84F

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33362 N$ $T_{ssl}^{AB} = N$

$= 7500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J65-W-1

Manufacturer: Wright

Application: F-84F, B-57A

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32027 N$ $T_{ssl}^{AB} = N$
 $= 7200 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J65-W-16

Manufacturer: Wright

Application: A4D-2 (A-4B), A4D-2N (A-4C), TA-4B

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 34251 N$ $T_{ssl}^{AB} = N$
 $= 7700 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J65-W-16A

Manufacturer: Wright

Application: FJ-4/-4B/-4D, A4D-2 (A-4B), A4D-2N (A-4C), A-4P/Q, EA-4P, TA-4B

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 34251 N$ $T_{ssl}^{AB} = N$
 $= 7700 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J65-W-18

Manufacturer: Wright

Application: F11F-1, F11F-1P

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 34251 \text{ N}$ $T_{ssl}^{AB} = 46706 \text{ N}$

$= 7700 \text{ lbf}$ $= 10500 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J65-W-1A

Manufacturer: Wright

Application: F-84F, B-57A

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32027 \text{ N}$ $T_{ssl}^{AB} = N$

$= 7200 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J65-W-2

Manufacturer: Wright

Application: XFJ-3, XA4D-1

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32027 \text{ N}$ $T_{ssl}^{AB} = N$

$= 7200 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J65-W-3

Manufacturer: Wright

Application: F-84F, RF-84F

Composition: / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32605 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 7330 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J65-W-4

Manufacturer: Wright

Application: FJ-3/-3D/-3D2/-3M, A4D-1 (A-4A)

Composition: / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 34696 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 7800 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J65-W-4B

Manufacturer: Wright

Application: FJ-3/-3D/-3D2/-3M, A4D-1 (A-4A)

Composition: / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 34696 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 7800 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J65-W-5

Manufacturer: Wright

Application: B-57B/C, RB-57A

Composition: / / / / /

 $D_{fan} = m = in$
 $D = m$

Nb of shafts =

 $L = m$
 $W_{eng} = kg = lb$
 $= in$
 $= in$

Static Sea Level:

 $T_{ssl} = 32116 \text{ N}$
 $T_{ssl}^{AB} = N$

Cruise:

 $T_{cr} = N$
 $= 7220 \text{ lbf}$
 $= lbf$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

 $OPR_{cr} =$

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$
J65-W-6

Manufacturer: Wright

Application: XRG-15A

Composition: / / / / /

 $D_{fan} = m = in$
 $D = m$

Nb of shafts =

 $L = m$
 $W_{eng} = kg = lb$
 $= in$
 $= in$

Static Sea Level:

 $T_{ssl} = 34696 \text{ N}$
 $T_{ssl}^{AB} = 46706 \text{ N}$
 $T_{cr} = N$
 $= 7800 \text{ lbf}$
 $= 10500 \text{ lbf}$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

 $OPR_{cr} =$

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$
J65-W-7

Manufacturer: Wright

Application: F-84F, RF-84F, XF11F-1 (XF9F-9)

Composition: / / / / /

 $D_{fan} = m = in$
 $D = m$

Nb of shafts =

 $L = m$
 $W_{eng} = kg = lb$
 $= in$
 $= in$

Static Sea Level:

 $T_{ssl} = 33362 \text{ N}$
 $T_{ssl}^{AB} = N$

Cruise:

 $T_{cr} = N$
 $= 7500 \text{ lbf}$
 $= lbf$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

 $OPR_{cr} =$

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$

J69-T-17

Manufacturer: Continental

Application: XGAM-67

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4448 N$ $T_{ssl}^{AB} = N$

$= 1000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-25

Manufacturer: Continental

Application: T-37A/B/C, C-117D

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = 0.566 m$

$W_{eng} = 165 kg = 364 lb$ $= 22.3 in$

Static Sea Level:

$T_{ssl} = 4559 N$ $T_{ssl}^{AB} = N$

$= 1025 lbf$ $= lbf$

$SFC_{ssl} = 3.14 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.11 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 9.1 kg/s = 20.1 lb/s$

BPR =

OPR = 3.8

FPR =

TET = 1103 °K

Nb of shafts = 1

$L = 1.27 m$

$= 50 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-27

Manufacturer: Continental

Application:

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 5115 N$ $T_{ssl}^{AB} = N$

$= 1150 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-29

Manufacturer: Continental

Application: AQM-34G/H/J/K/V/U, BGM-34C, BQM-34A/S, MQM-34D

Composition: - / - / 1 + 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 0.568 \text{ m}$ $L = 1.175 \text{ m}$

$W_{eng} = 154 \text{ kg} = 340 \text{ lb}$ $= 22.4 \text{ in}$ $= 46.3 \text{ in}$

Static Sea Level:

$T_{ssl} = 7562 \text{ N}$ $T_{ssl}^{AB} = N$

$= 1700 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.06 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 1.08 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 13.2 \text{ kg/s} = 29.1 \text{ lb/s}$

BPR = OPR = 5.5

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-3

Manufacturer: Continental

Application:

Composition: - / - / 1 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$ $L = m$

$W_{eng} = \text{kg} = \text{lb}$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 3928 \text{ N}$ $T_{ssl}^{AB} = N$

$= 883 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-39

Manufacturer: Continental

Application:

Composition: - / - / 2 + 1C / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$ $L = m$

$W_{eng} = \text{kg} = \text{lb}$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 11209 \text{ N}$ $T_{ssl}^{AB} = N$

$= 2520 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.72 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.96 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 19.5 \text{ kg/s} = 43 \text{ lb/s}$

BPR = OPR = 6.5

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-406

Manufacturer: Continental

Application: BQM-34E/F/T

Composition: - / - / 1+ 1C / 1 / - / -

$D_{fan} = m = in$ $D = 0.568 m$

$W_{eng} = 163 kg = 359 lb$ $= 22.4 in$

Static Sea Level:

$T_{ssl} = 8185 N$ $T_{ssl}^{AB} = N$

$= 1840 lbf$ $= lbf$

$SFC_{ssl} = 3.14 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.11 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 14.1 kg/s = 31.1 lb/s$

BPR = OPR = 5.5

FPR = TET = °K

Nb of shafts = 1

$L = 1.175 m$

$= 46.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-41

Manufacturer: Continental

Application:

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8185 N$ $T_{ssl}^{AB} = N$

$= 1840 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 5.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-41A

Manufacturer: Continental

Application: AQM-34L/M/N, BQM-34B/S, XAQM-103A

Composition: - / - / 1+ 1C / 1 / - / -

$D_{fan} = m = in$ $D = 0.568 m$

$W_{eng} = 159 kg = 351 lb$ $= 22.4 in$

Static Sea Level:

$T_{ssl} = 8541 N$ $T_{ssl}^{AB} = N$

$= 1920 lbf$ $= lbf$

$SFC_{ssl} = 3.09 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.09 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 13.6 kg/s = 30 lb/s$

BPR = OPR = 6

FPR = TET = °K

Nb of shafts = 1

$L = 1.175 m$

$= 46.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-7

Manufacturer: Continental

Application:

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4092 \text{ N}$ $T_{ssl}^{AB} = N$

$= 920 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J69-T-9

Manufacturer: Continental

Application: T-37A, TT-1

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4092 \text{ N}$ $T_{ssl}^{AB} = N$

$= 920 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J71-A-11

Manufacturer: Allison

Application: B-66B, RB-66A/B/C

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 45372 \text{ N}$ $T_{ssl}^{AB} = N$

$= 10200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J71-A-13

Manufacturer: Allison

Application: B-66B, EB-66C/E, RB-66B/C, WB-66D

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 45372 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 10200 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J71-A-2

Manufacturer: Allison

Application: F3H-1(RE)/-2/-2M/-2N/-2P

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 42258 N$

$T_{ssl}^{AB} = 64054 N$

Cruise:

$T_{cr} = N$

$= 9500 lbf$

$= 14400 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J71-A-2A

Manufacturer: Allison

Application: F3H-1(RE)/-2/-2M/-2N/-2P

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 42258 N$

$T_{ssl}^{AB} = 64054 N$

Cruise:

$T_{cr} = N$

$= 9500 lbf$

$= 14400 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

J71-A-2B

Manufacturer: Allison

Application: F3H-1(RE)/-2/-2M/-2N/-2P

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 42258 \text{ N}$ $T_{ssl}^{AB} = 64054 \text{ N}$
 $= 9500 \text{ lbf}$ $= 14400 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J71-A-9

Manufacturer: Allison

Application: YRB-66A, RB-66A

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 62275 \text{ N}$
 $= lbf$ $= 14000 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J73-GE-3

Manufacturer: GE : General Electric

Application: F-86H-1, F3H-3 (not produced)

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 40923 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 9200 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J73-GE-3A

Manufacturer: GE : General Electric

Application: F-86H-5

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$
Static Sea Level:
 $T_{ssl} = 40923 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 9200 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J73-GE-3D

Manufacturer: GE : General Electric

Application: F-86H-5

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$
Static Sea Level:
 $T_{ssl} = 40923 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 9200 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J73-GE-3E

Manufacturer: GE : General Electric

Application: F-86H-10

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$
Static Sea Level:
 $T_{ssl} = 40923 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 9200 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J73-GE-5**Manufacturer:** GE : General Electric**Application:** YF-84J**Composition:** / / / / / $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 38922 N$ $T_{ssl}^{AB} = N$ $= 8750 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$ **Nb of shafts =** $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **J73-GE-7****Manufacturer:** GE : General Electric**Application:** YF-84J**Composition:** / / / / / $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 39678 N$ $T_{ssl}^{AB} = N$ $= 8920 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$ **Nb of shafts =** $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **J75-P-13B****Manufacturer:** Pratt & Whitney**Application:** U-2C, TR-1A**Composition:** - / 8 / 7 / 1 / - / 2 $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 75619 N$ $T_{ssl}^{AB} = N$ $= 17000 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$ **Nb of shafts = 2** $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

J75-P-17

Manufacturer: Pratt & Whitney

Application: AB, F-106A/B, QF-106A

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.092 \text{ m}$ Nb of shafts = 2
 $W_{eng} = 2665 \text{ kg} = 5875 \text{ lb}$ $= 43 \text{ in}$ $L = 6.035 \text{ m}$
 $= 237.6 \text{ in}$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 108981 \text{ N}$
 $= lbf$ $= 24500 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = 6.09 \cdot 10^{-5} (kg/s)/N$
 $= (lb/h)/lbf$ $= 2.15 (lb/h)/lbf$
 $\dot{w}_{ssl} = 114.3 \text{ kg/s} = 252 \text{ lb/s}$
 $BPR =$ $OPR = 12$
 $FPR =$ $TET = 1150 \text{ }^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J75-P-19

Manufacturer: Pratt & Whitney

Application: F-105B, F-105C (not produced)

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$ Nb of shafts = 2
 $W_{eng} = \text{kg} = \text{lb}$ $= in$ $L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 72061 \text{ N}$ $T_{ssl}^{AB} = 111205 \text{ N}$
 $= 16200 \text{ lbf}$ $= 25000 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR = 12$
 $FPR =$ $TET = \text{ }^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J75-P-19W

Manufacturer: Pratt & Whitney

Application: F-105D/F/G, F-105E, RF-105D (not produced)

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.092 \text{ m}$ Nb of shafts = 2
 $W_{eng} = 2703 \text{ kg} = 5959 \text{ lb}$ $= 43 \text{ in}$ $L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 76509 \text{ N}$ $T_{ssl}^{AB} = 117877 \text{ N}$
 $= 17200 \text{ lbf}$ $= 26500 \text{ lbf}$
 $SFC_{ssl} = 2.24 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.23 \cdot 10^{-5} (kg/s)/N$
 $= 0.79 (lb/h)/lbf$ $= 2.2 (lb/h)/lbf$
 $\dot{w}_{ssl} = 120.2 \text{ kg/s} = 265 \text{ lb/s}$
 $BPR =$ $OPR = 12$
 $FPR =$ $TET = \text{ }^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J75-P-3

Manufacturer: Pratt & Whitney

Application: YF-105B, CF-105

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 73395 N$ $T_{ssl}^{AB} = 104533 N$

$= 16500 lbf$ $= 23500 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J75-P-5

Manufacturer: Pratt & Whitney

Application:

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 73395 N$ $T_{ssl}^{AB} = 104533 N$

$= 16500 lbf$ $= 23500 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-10

Manufacturer: GE : General Electric

Application: F-4J, A3J-3, RA-5C

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.992 m$

$W_{eng} = 1749 kg = 3856 lb$ $= 39.1 in$

Static Sea Level:

$T_{ssl} = 52800 N$ $T_{ssl}^{AB} = 79445 N$

$= 11870 lbf$ $= 17860 lbf$

$SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.58 \cdot 10^{-5} (kg/s)/N$

$= 0.84 (lb/h)/lbf$ $= 1.97 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 13.4

FPR = TET = °K

Nb of shafts = 1

$L = 5.301 m$

$= 208.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-10B

Manufacturer: GE : General Electric

Application: F-4J/S, QF-4S

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.992 m$ $L = 5.301 m$
 $W_{eng} = kg = lb$ $= 39.1 in$ $= 208.7 in$

Static Sea Level:

$T_{ssl} = 52800 N$ $T_{ssl}^{AB} = 79445 N$
 $= 11870 lbf$ $= 17860 lbf$
 $SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.58 \cdot 10^{-5} (kg/s)/N$
 $= 0.84 (lb/h)/lbf$ $= 1.97 (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 13.4$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 5.301 m$
 $= 208.7 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J79-GE-11

Manufacturer: GE : General Electric

Application: F-104G, NF-104G, RF-104G, TF-104G

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.973 m$ $L = 5.282 m$
 $W_{eng} = kg = lb$ $= 38.3 in$ $= 208 in$

Static Sea Level:

$T_{ssl} = 44482 N$ $T_{ssl}^{AB} = 70282 N$
 $= 10000 lbf$ $= 15800 lbf$
 $SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.58 \cdot 10^{-5} (kg/s)/N$
 $= 0.84 (lb/h)/lbf$ $= 1.97 (lb/h)/lbf$
 $\dot{w}_{ssl} = 76.7 kg/s = 169.1 lb/s$
 $BPR =$ $OPR = 12.9$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 5.282 m$
 $= 208 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J79-GE-119

Manufacturer: GE : General Electric

Application: MDD F-4 Phantom, Lockheed F-104

Composition: - / - / 17 / 3 / - / -

$D_{fan} = 0.992 m = 39.1 in$ $D = m$ $L = 5.3 m$
 $W_{eng} = 1715 kg = 3781 lb$ $= in$ $= 208.7 in$

Static Sea Level:

$T_{ssl} = 53601 N$ $T_{ssl}^{AB} = 83293 N$
 $= 12050 lbf$ $= 18725 lbf$
 $SFC_{ssl} = 2.36 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.75 \cdot 10^{-5} (kg/s)/N$
 $= 0.83 (lb/h)/lbf$ $= 2.03 (lb/h)/lbf$
 $\dot{w}_{ssl} = 77 kg/s = 169.8 lb/s$
 $BPR = 0$ $OPR = 13.4$
 $FPR =$ $TET = 1273 ^\circ K$

Nb of shafts = 1

$L = 5.3 m$
 $= 208.7 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Year: 1955

J79-GE-11A

Manufacturer: GE : General Electric

Application: F-104G, NF-104G, RF-104G, TF-104G

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.973 \text{ m}$ $L = 5.282 \text{ m}$
 $W_{eng} = 1615 \text{ kg} = 3560 \text{ lb}$ $= 38.3 \text{ in}$ $= 208 \text{ in}$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$ $T_{ssl}^{AB} = 70282 \text{ N}$
 $= 10000 \text{ lbf}$ $= 15800 \text{ lbf}$
 $SFC_{ssl} = (\text{kg/s})/N$ $SFC_{ssl}^{AB} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 76.7 \text{ kg/s} = 169.1 \text{ lb/s}$
 $BPR =$ $OPR = 12.9$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J79-GE-15

Manufacturer: GE : General Electric

Application: F-4C/D, EF-4C/D, RF-4C

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.973 \text{ m}$ $L = 5.301 \text{ m}$
 $W_{eng} = 1678 \text{ kg} = 3699 \text{ lb}$ $= 38.3 \text{ in}$ $= 208.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 48485 \text{ N}$ $T_{ssl}^{AB} = 75619 \text{ N}$
 $= 10900 \text{ lbf}$ $= 17000 \text{ lbf}$
 $SFC_{ssl} = 2.44 \cdot 10^{-5} (\text{kg/s})/N$ $SFC_{ssl}^{AB} = 5.52 \cdot 10^{-5} (\text{kg/s})/N$
 $= 0.86 (\text{lb/h})/\text{lbf}$ $= 1.95 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR = 12.9$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J79-GE-17

Manufacturer: GE : General Electric

Application: F-4E/G

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.992 \text{ m}$ $L = 5.301 \text{ m}$
 $W_{eng} = 1740 \text{ kg} = 3836 \text{ lb}$ $= 39.1 \text{ in}$ $= 208.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 52800 \text{ N}$ $T_{ssl}^{AB} = 79623 \text{ N}$
 $= 11870 \text{ lbf}$ $= 17900 \text{ lbf}$
 $SFC_{ssl} = 2.39 \cdot 10^{-5} (\text{kg/s})/N$ $SFC_{ssl}^{AB} = 5.58 \cdot 10^{-5} (\text{kg/s})/N$
 $= 0.84 (\text{lb/h})/\text{lbf}$ $= 1.97 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 77.1 \text{ kg/s} = 170 \text{ lb/s}$
 $BPR =$ $OPR = 13.5$
 $FPR =$ $TET = 928 ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/N$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J79-GE-17C

Manufacturer: GE : General Electric

Application: F-4E/G

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.992 m$

$W_{eng} = kg = lb$ $= 39.1 in$

Static Sea Level:

$T_{ssl} = 52800 N$ $T_{ssl}^{AB} = 79623 N$

$= 11870 lbf$ $= 17900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 77.1 kg/s = 170 lb/s$

BPR = OPR = 13.5

FPR = TET = °K

Nb of shafts = 1

$L = 5.301 m$

$= 208.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-17E

Manufacturer: GE : General Electric

Application: F-4E/G

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.992 m$

$W_{eng} = kg = lb$ $= 39.1 in$

Static Sea Level:

$T_{ssl} = 52800 N$ $T_{ssl}^{AB} = 79623 N$

$= 11870 lbf$ $= 17900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 77.1 kg/s = 170 lb/s$

BPR = OPR = 13.5

FPR = TET = °K

Nb of shafts = 1

$L = 5.301 m$

$= 208.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-19

Manufacturer: Fiat

Application: F-104S

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.992 m$

$W_{eng} = 1740 kg = 3836 lb$ $= 39.1 in$

Static Sea Level:

$T_{ssl} = 52800 N$ $T_{ssl}^{AB} = 79623 N$

$= 11870 lbf$ $= 17900 lbf$

$SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.58 \cdot 10^{-5} (kg/s)/N$

$= 0.84 (lb/h)/lbf$ $= 1.97 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 5.301 m$

$= 208.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-2

Manufacturer: GE : General Electric

Application: F4H-1F (F-4A), A-5A

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.973 m$

$W_{eng} = 1642 kg = 3620 lb$ $= 38.3 in$

Static Sea Level:

$T_{ssl} = 46039 N$ $T_{ssl}^{AB} = 71838 N$

$= 10350 lbf$ $= 16150 lbf$

$SFC_{ssl} = 2.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.67 \cdot 10^{-5} (kg/s)/N$

$= 0.87 (lb/h)/lbf$ $= 2 (lb/h)/lbf$

$\dot{w}_{ssl} = 75.3 kg/s = 166 lb/s$

BPR = OPR = 12.5

FPR = TET = °K

Nb of shafts = 1

$L = 5.282 m$

$= 208 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-2A

Manufacturer: GE : General Electric

Application: F4H-1F (F-4A), A-5A

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.973 m$

$W_{eng} = kg = lb$ $= 38.3 in$

Static Sea Level:

$T_{ssl} = 46039 N$ $T_{ssl}^{AB} = 71838 N$

$= 10350 lbf$ $= 16150 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 75.3 kg/s = 166 lb/s$

BPR = OPR = 12.5

FPR = TET = °K

Nb of shafts = 1

$L = 5.282 m$

$= 208 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-3

Manufacturer: GE : General Electric

Application: GQM-13A, MQM-13A, RGM-13A, XF11F-1F

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.973 m$

$W_{eng} = kg = lb$ $= 38.3 in$

Static Sea Level:

$T_{ssl} = 43592 N$ $T_{ssl}^{AB} = 66723 N$

$= 9800 lbf$ $= 15000 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 5.269 m$

$= 207.4 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-3A

Manufacturer: GE : General Electric

Application: F-104A/B

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.973 m$
 $W_{eng} = kg = lb$ $= 38.3 in$

Nb of shafts = 1
 $L = 5.269 m$
 $= 207.4 in$

Static Sea Level:

$T_{ssl} = 43592 N$ $T_{ssl}^{AB} = 66723 N$
 $= 9800 lbf$ $= 15000 lbf$
 $SFC_{ssl} = 2.4 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.78 \cdot 10^{-5} (kg/s)/N$
 $= 0.85 (lb/h)/lbf$ $= 2.04 (lb/h)/lbf$
 $\dot{w}_{ssl} = 72.6 kg/s = 160.1 lb/s$
BPR = OPR = 12
FPR = TET = °K

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
OPR_{cr} =
 $M_{cr} = , h_{cr} = m$

J79-GE-3B

Manufacturer: GE : General Electric

Application: F-104A/B

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.973 m$
 $W_{eng} = 1508 kg = 3325 lb$ $= 38.3 in$

Nb of shafts = 1
 $L = 5.269 m$
 $= 207.4 in$

Static Sea Level:

$T_{ssl} = 43592 N$ $T_{ssl}^{AB} = 66723 N$
 $= 9800 lbf$ $= 15000 lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 72.6 kg/s = 160.1 lb/s$
BPR = OPR = 12
FPR = TET = °K

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
OPR_{cr} =
 $M_{cr} = , h_{cr} = m$

J79-GE-4

Manufacturer: GE : General Electric

Application: A3J-1 (A-5A)

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Nb of shafts = 1
 $L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 45816 N$ $T_{ssl}^{AB} = N$
 $= 10300 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
BPR = OPR =
FPR = TET = °K

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
OPR_{cr} =
 $M_{cr} = , h_{cr} = m$

J79-GE-5

Manufacturer: GE : General Electric

Application: B-58A

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.965 m$

$W_{eng} = kg = lb$ $= 38 in$

Static Sea Level:

$T_{ssl} = 45816 N$ $T_{ssl}^{AB} = 69392 N$

$= 10300 lbf$ $= 15600 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 5.135 m$

$= 202.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-5A

Manufacturer: GE : General Electric

Application: B-58A

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.965 m$

$W_{eng} = kg = lb$ $= 38 in$

Static Sea Level:

$T_{ssl} = 45816 N$ $T_{ssl}^{AB} = 69392 N$

$= 10300 lbf$ $= 15600 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 5.135 m$

$= 202.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-5B

Manufacturer: GE : General Electric

Application: B-58A

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.965 m$

$W_{eng} = kg = lb$ $= 38 in$

Static Sea Level:

$T_{ssl} = 45816 N$ $T_{ssl}^{AB} = 69392 N$

$= 10300 lbf$ $= 15600 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 5.135 m$

$= 202.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-GE-5C

Manufacturer: GE : General Electric

Application: B-58A

Composition: - / - / 17 / 3 / - / -

 $D_{fan} = m = in$
 $D = 0.965 m$
 $W_{eng} = 1671 kg = 3684 lb$
 $= 38 in$

Static Sea Level:

 $T_{ssl} = 45816 N$
 $T_{ssl}^{AB} = 69392 N$
 $= 10300 lbf$
 $= 15600 lbf$
 $SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = 6.23 \cdot 10^{-5} (kg/s)/N$
 $= 0.84 (lb/h)/lbf$
 $= 2.2 (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

 $L = 5.135 m$
 $= 202.2 in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
J79-GE-7

Manufacturer: GE : General Electric

Application: F-104C/D

Composition: - / - / 17 / 3 / - / -

 $D_{fan} = m = in$
 $D = 0.973 m$
 $W_{eng} = kg = lb$
 $= 38.3 in$

Static Sea Level:

 $T_{ssl} = 44482 N$
 $T_{ssl}^{AB} = 70282 N$
 $= 10000 lbf$
 $= 15800 lbf$
 $SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = 5.58 \cdot 10^{-5} (kg/s)/N$
 $= 0.84 (lb/h)/lbf$
 $= 1.97 (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

 $L = 5.282 m$
 $= 208 in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
J79-GE-7A

Manufacturer: GE : General Electric

Application: F-104C/D

Composition: - / - / 17 / 3 / - / -

 $D_{fan} = m = in$
 $D = 0.973 m$
 $W_{eng} = kg = lb$
 $= 38.3 in$

Static Sea Level:

 $T_{ssl} = 44482 N$
 $T_{ssl}^{AB} = 70282 N$
 $= 10000 lbf$
 $= 15800 lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

 $L = 5.282 m$
 $= 208 in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J79-GE-8

Manufacturer: GE : General Electric

Application: F4H-1 (F-4B), F-4N, RF-4B, A3J-1, A3J-2 (A-4B), A3J-3 (RA-3C)

Composition: - / - / 17 / 3 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$
 $D = 0.973 \text{ m}$
 $L = 5.295 \text{ m}$
 $W_{eng} = 1666 \text{ kg} = 3673 \text{ lb}$
 $= 38.3 \text{ in}$
 $= 208.5 \text{ in}$

Static Sea Level:

 $T_{ssl} = 48485 \text{ N}$
 $T_{ssl}^{AB} = 75619 \text{ N}$
 $= 10900 \text{ lbf}$
 $= 17000 \text{ lbf}$
 $SFC_{ssl} = 2.44 \cdot 10^{-5} \text{ (kg/s)/N}$
 $SFC_{ssl}^{AB} = 5.47 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.86 \text{ (lb/h)/lbf}$
 $= 1.93 \text{ (lb/h)/lbf}$
 $\dot{w}_{ssl} = 76.7 \text{ kg/s} = 169.1 \text{ lb/s}$

BPR =

OPR = 12.9

FPR =

TET = °K

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$
J79-GE-8A

Manufacturer: GE : General Electric

Application: F4H-1 (F-4B), F-4N, RF-4B, A3J-1, A3J-2 (A-4B), A3J-3 (RA-3C)

Composition: - / - / 17 / 3 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$
 $D = 0.973 \text{ m}$
 $L = 5.295 \text{ m}$
 $W_{eng} = \text{kg} = \text{lb}$
 $= 38.3 \text{ in}$
 $= 208.5 \text{ in}$

Static Sea Level:

 $T_{ssl} = 48485 \text{ N}$
 $T_{ssl}^{AB} = 75619 \text{ N}$
 $= 10900 \text{ lbf}$
 $= 17000 \text{ lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$
 $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 76.7 \text{ kg/s} = 169.1 \text{ lb/s}$

BPR =

OPR = 12.9

FPR =

TET = °K

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$
J79-GE-J1E

Manufacturer: GE : General Electric

Application: Kfir-C1

Composition: - / - / 17 / 3 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$
 $D = m$
 $L = m$
 $W_{eng} = \text{kg} = \text{lb}$
 $= in$
 $= in$

Static Sea Level:

 $T_{ssl} = N$
 $T_{ssl}^{AB} = 79623 \text{ N}$
 $= \text{lbf}$
 $= 17900 \text{ lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$
 $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = m$

J79-MTU-17A

Manufacturer: MTU

Application: F-4F

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = 0.992 m$

$W_{eng} = 1749 kg = 3856 lb$ $= 39.1 in$

Static Sea Level:

$T_{ssl} = 52800 N$ $T_{ssl}^{AB} = 79623 N$

$= 11870 lbf$ $= 17900 lbf$

$SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.58 \cdot 10^{-5} (kg/s)/N$

$= 0.84 (lb/h)/lbf$ $= 1.97 (lb/h)/lbf$

$\dot{w}_{ssl} = 77.1 kg/s = 170 lb/s$

BPR = OPR = 13.5

FPR = TET = °K

Nb of shafts = 1

$L = 5.301 m$

$= 208.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-MTU-J1K

Manufacturer: MTU

Application: F-104G

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 46706 N$ $T_{ssl}^{AB} = 71171 N$

$= 10500 lbf$ $= 16000 lbf$

$SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.83 \cdot 10^{-5} (kg/s)/N$

$= 0.84 (lb/h)/lbf$ $= 2.06 (lb/h)/lbf$

$\dot{w}_{ssl} = 74.4 kg/s = 164 lb/s$

BPR = OPR = 12.4

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J79-OEL-7

Manufacturer: Orenda

Application: CF-104A/D

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = 1622 kg = 3576 lb$ $= in$

Static Sea Level:

$T_{ssl} = 44482 N$ $T_{ssl}^{AB} = 70282 N$

$= 10000 lbf$ $= 15800 lbf$

$SFC_{ssl} = 2.39 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.58 \cdot 10^{-5} (kg/s)/N$

$= 0.84 (lb/h)/lbf$ $= 1.97 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-CAN-15

Manufacturer: Orenda

Application: CF-5A/D

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 13011 \text{ N}$ $T_{ssl}^{AB} = 19127 \text{ N}$

$= 2925 \text{ lbf}$ $= 4300 \text{ lbf}$

$SFC_{ssl} = 2.61 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 6.18 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.92 \text{ (lb/h)/lbf}$ $= 2.18 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$

$BPR =$ $OPR = 7$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

J85-CAN-40

Manufacturer: Orenda

Application: CT-114 (CL-41A/R) Tutor

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 12677 \text{ N}$ $T_{ssl}^{AB} = 12677 \text{ N}$

$= 2850 \text{ lbf}$ $= 2850 \text{ lbf}$

$SFC_{ssl} = 2.75 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.97 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$

$BPR =$ $OPR = 6.8$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

J85-GE-1

Manufacturer: GE : General Electric

Application: T-38A

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 9341 \text{ N}$ $T_{ssl}^{AB} = N$

$= 2100 \text{ lbf}$ $= lbf$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

J85-GE-12

Manufacturer: GE : General Electric

Application: AT-3D

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 10676 N$ $T_{ssl}^{AB} = N$
 $= 2400 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-13

Manufacturer: GE : General Electric

Application: F-5A/B, RF-5A

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.559 m$

$W_{eng} = 271 kg = 597 lb$ $= 22 in$

Static Sea Level:

$T_{ssl} = 12099 N$ $T_{ssl}^{AB} = 18149 N$
 $= 2720 lbf$ $= 4080 lbf$

$SFC_{ssl} = 3.57 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.29 \cdot 10^{-5} (kg/s)/N$
 $= 1.26 (lb/h)/lbf$ $= 2.22 (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR = 6.5

FPR = TET = °K

Nb of shafts = 1

$L = 2.766 m$

$= 108.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-13A

Manufacturer: GE : General Electric

Application: F-5A/B, RF-5A, G91Y, Y/T, Y/S

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.559 m$

$W_{eng} = kg = lb$ $= 22 in$

Static Sea Level:

$T_{ssl} = 12099 N$ $T_{ssl}^{AB} = 18149 N$
 $= 2720 lbf$ $= 4080 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR = 6.5

FPR = TET = °K

Nb of shafts = 1

$L = 2.766 m$

$= 108.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-17

Manufacturer: GE : General Electric

Application: AC-119G/K, C-123K

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.45 m$

$W_{eng} = 181 kg = 399 lb$ $= 17.7 in$

Static Sea Level:

$T_{ssl} = 12677 N$ $T_{ssl}^{AB} = N$

$= 2850 lbf$ $= lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR = 6.5

FPR = TET = 1167 °K

Nb of shafts = 1

$L = 1.029 m$

$= 40.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-17A

Manufacturer: GE : General Electric

Application: A-37B, OA-37B

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 12677 N$ $T_{ssl}^{AB} = N$

$= 2850 lbf$ $= lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR = 6.9

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-17B

Manufacturer: GE : General Electric

Application: Saab 105XT

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 12677 N$ $T_{ssl}^{AB} = N$

$= 2850 lbf$ $= lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR = 6.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-17C

Manufacturer: GE : General Electric

Application:

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 12677 N$ $T_{ssl}^{AB} = N$

$= 2850 lbf$ $= lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = OPR = 6.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-2

Manufacturer: GE : General Electric

Application: SP-5B Marlin (boosters)

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 12677 N$ $T_{ssl}^{AB} = N$

$= 2850 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-21

Manufacturer: GE : General Electric

Application: F-5E/F

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.663 m$

$W_{eng} = 290 kg = 639 lb$ $= 26.1 in$

Static Sea Level:

$T_{ssl} = 16014 N$ $T_{ssl}^{AB} = 22241 N$

$= 3600 lbf$ $= 5000 lbf$

$SFC_{ssl} = 3.51 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.03 \cdot 10^{-5} (kg/s)/N$

$= 1.24 (lb/h)/lbf$ $= 2.13 (lb/h)/lbf$

$\dot{w}_{ssl} = 24 kg/s = 52.9 lb/s$

BPR = OPR = 8.3

FPR = TET = 1250 °K

Nb of shafts = 1

$L = 2.858 m$

$= 112.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-21A

Manufacturer: GE : General Electric

Application: F-5E/F

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.663 \text{ m}$
 $W_{eng} = kg = lb$ $= 26.1 \text{ in}$

Nb of shafts = 1

$L = 2.858 \text{ m}$
 $= 112.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 16014 \text{ N}$ $T_{ssl}^{AB} = 22241 \text{ N}$
 $= 3600 \text{ lbf}$ $= 5000 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 24 \text{ kg/s} = 52.9 \text{ lb/s}$
 $BPR =$ $OPR = 8.1$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J85-GE-3

Manufacturer: GE : General Electric

Application: ADM-20A

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Nb of shafts = 1

$L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 10898 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2450 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J85-GE-4

Manufacturer: GE : General Electric

Application: T-2C, XMQM-34D Mod II

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.434 \text{ m}$
 $W_{eng} = 183 \text{ kg} = 403 \text{ lb}$ $= 17.1 \text{ in}$

Nb of shafts = 1

$L = 1.152 \text{ m}$
 $= 45.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 13122 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2950 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = 2.78 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.98 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$
 $BPR =$ $OPR = 6.5$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J85-GE-5

Manufacturer: GE : General Electric

Application: A-37A, T-38A, AT-38B, X-14A/B, AQM-35B, F-109 (D-118A) (not produced)

Composition: - / - / 9 / 2 / - / -

 $D_{fan} = m = in$
 $D = 0.559 \text{ m}$
 $W_{eng} = 265 \text{ kg} = 584 \text{ lb}$
 $= 22 \text{ in}$

Nb of shafts = 1

 $L = 2.746 \text{ m}$
 $= 108.1 \text{ in}$

Static Sea Level:

 $T_{ssl} = 11921 \text{ N}$
 $T_{ssl}^{AB} = 17126 \text{ N}$
 $= 2680 \text{ lbf}$
 $= 3850 \text{ lbf}$
 $SFC_{ssl} = 2.92 \cdot 10^{-5} \text{ (kg/s)/N}$
 $SFC_{ssl}^{AB} = 6.23 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 1.03 \text{ (lb/h)/lbf}$
 $= 2.2 \text{ (lb/h)/lbf}$
 $\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$

BPR =

OPR = 6.7

FPR =

TET = 1167 °K

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
J85-GE-5A

Manufacturer: GE : General Electric

Application: T-38A, AT-38B

Composition: - / - / 9 / 2 / - / -

 $D_{fan} = m = in$
 $D = 0.559 \text{ m}$
 $W_{eng} = \text{kg} = \text{lb}$
 $= 22 \text{ in}$

Nb of shafts = 1

 $L = 2.746 \text{ m}$
 $= 108.1 \text{ in}$

Static Sea Level:

 $T_{ssl} = 11921 \text{ N}$
 $T_{ssl}^{AB} = 17126 \text{ N}$
 $= 2680 \text{ lbf}$
 $= 3850 \text{ lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$
 $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$

BPR =

OPR = 6.5

FPR =

TET = °K

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
J85-GE-7

Manufacturer: GE : General Electric

Application: ADM-20B/C, BQM-34A(RE), MQM-34D Mod II

Composition: - / - / 8 / 2 / - / -

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = \text{kg} = \text{lb}$
 $= in$

Nb of shafts = 1

 $L = m$
 $= in$

Static Sea Level:

 $T_{ssl} = 10898 \text{ N}$
 $T_{ssl}^{AB} = N$
 $= 2450 \text{ lbf}$
 $= \text{lbf}$
 $SFC_{ssl} = 2.75 \cdot 10^{-5} \text{ (kg/s)/N}$
 $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.97 \text{ (lb/h)/lbf}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 19.1 \text{ kg/s} = 42.1 \text{ lb/s}$

BPR =

OPR = 6.5

FPR =

TET = °K

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

J85-GE-J4

Manufacturer: GE : General Electric

Application: CL-41G

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 13122 N$ $T_{ssl}^{AB} = N$

$= 2950 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-GE-LF1

Manufacturer: GE : General Electric

Application: XV-5B

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 13122 N$ $T_{ssl}^{AB} = N$

$= 2950 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J85-J1

Manufacturer: GE : General Electric

Application:

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16014 N$ $T_{ssl}^{AB} = 22241 N$

$= 3600 lbf$ $= 5000 lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 24 kg/s = 52.9 lb/s$

BPR = OPR = 8.3

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

J97-GE-100

Manufacturer: GE : General Electric

Application: AQM-91A, YQM-94A

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 23442 N$ $T_{ssl}^{AB} = N$
 $= 5270 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

JT12A

Manufacturer: Pratt & Whitney

Application:

Composition: / / / / /

$D_{fan} = 0.457 m = 18 in$ $D = m$
 $W_{eng} = 203 kg = 448 lb$ $= in$

Static Sea Level:

$T_{ssl} = 13342 N$ $T_{ssl}^{AB} = N$
 $= 2999 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 22 kg/s = 48.5 lb/s$
 $BPR = 0$ $OPR = 6.5$
 $FPR =$ $TET = ^\circ K$

Year: 1958

Nb of shafts =
 $L = 1.6 m$
 $= 63 in$

Cruise:

$T_{cr} = 3561 N$
 $= 801 lbf$
 $SFC_{cr} = 3 \cdot 10^{-5} (kg/s)/N$
 $= 1.06 (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = 0.8 , h_{cr} = 11000 m$

JT12A-3

Manufacturer: Pratt & Whitney

Application: XV-4, SD-4, Model 533

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 m$
 $W_{eng} = 205 kg = 452 lb$ $= 21.9 in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$
 $= 3000 lbf$ $= lbf$
 $SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.96 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

JT12A-5

Manufacturer: Pratt & Whitney

Application: CT-114 prototype

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 \text{ m}$
 $W_{eng} = 205 \text{ kg} = 452 \text{ lb}$ $= 21.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 13345 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

$L = m$
 $= in$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

JT12A-6

Manufacturer: Pratt & Whitney

Application: Sabreliner 40/50

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 \text{ m}$
 $W_{eng} = 205 \text{ kg} = 452 \text{ lb}$ $= 21.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 13345 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 2.72 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.96 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

$L = m$
 $= in$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

JT12A-6A

Manufacturer: Pratt & Whitney

Application: Sabreliner 40/50, JetStar I, C-140A/B JetStar

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 \text{ m}$
 $W_{eng} = 205 \text{ kg} = 452 \text{ lb}$ $= 21.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 13345 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 2.72 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.96 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

$L = m$
 $= in$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

JT12A-8

Manufacturer: Pratt & Whitney

Application: Sabreliner 60, JetStar I, CT-39E/G

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 m$

$W_{eng} = 212 kg = 467 lb$ $= 21.9 in$

Static Sea Level:

$T_{ssl} = 14679 N$ $T_{ssl}^{AB} = N$

$= 3300 lbf$ $= lbf$

$SFC_{ssl} = 2.82 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.99 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 23.1 kg/s = 50.9 lb/s$

BPR = OPR = 6.7

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

JT12A-8A

Manufacturer: Pratt & Whitney

Application: Sabreliner 60, JetStar I

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.556 m$

$W_{eng} = 212 kg = 467 lb$ $= 21.9 in$

Static Sea Level:

$T_{ssl} = 14679 N$ $T_{ssl}^{AB} = N$

$= 3300 lbf$ $= lbf$

$SFC_{ssl} = 2.82 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.99 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 23.1 kg/s = 50.9 lb/s$

BPR = OPR = 6.7

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

JT15D-1

Manufacturer: Pratt & Whitney

Application: Citation, SN.600 prototype

Composition: 1 / - / 1C / 1 / - / 2

$D_{fan} = 0.693 m = 27.3 in$ $D = 0.691 m$

$W_{eng} = 233 kg = 514 lb$ $= 27.2 in$

Static Sea Level:

$T_{ssl} = 9786 N$ $T_{ssl}^{AB} = N$

$= 2200 lbf$ $= lbf$

$SFC_{ssl} = 1.53 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.54 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 34 kg/s = 75 lb/s$

BPR = 3.3 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 1.506 m$

$= 59.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

JT15D-1A

Manufacturer: Pratt & Whitney

Application: Citation I/ISP

Composition: 1 / - / 1C / 1 / - / 2

$D_{fan} = 0.693 \text{ m} = 27.3 \text{ in}$ $D = 0.691 \text{ m}$

$W_{eng} = 235 \text{ kg} = 518 \text{ lb}$ $= 27.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 9786 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.53 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.54 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 34 \text{ kg/s} = 75 \text{ lb/s}$

BPR = 3.3 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 1.506 \text{ m}$

$= 59.3 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT15D-1B

Manufacturer: Pratt & Whitney

Application: Citation I/ISP

Composition: 1 / - / 1C / 1 / - / 2

$D_{fan} = 0.693 \text{ m} = 27.3 \text{ in}$ $D = 0.691 \text{ m}$

$W_{eng} = 235 \text{ kg} = 518 \text{ lb}$ $= 27.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 9786 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.53 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.54 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 34 \text{ kg/s} = 75 \text{ lb/s}$

BPR = 3.3 OPR = 10

FPR = 1.5 TET = °K

Nb of shafts = 2

$L = 1.506 \text{ m}$

$= 59.3 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT15D-4

Manufacturer: Pratt & Whitney

Application: Citation II/IISP, SN.601 Corvette, Diamond I, Fan Ranger

Composition: 1 / 1B / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = 0.528 \text{ m} = 20.8 \text{ in}$ $D = 0.686 \text{ m}$

$L = 1.6 \text{ m}$

$W_{eng} = 253 \text{ kg} = 558 \text{ lb}$ $= 27 \text{ in}$

$= 63 \text{ in}$

Static Sea Level:

$T_{ssl} = 11121 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.59 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.56 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.6 OPR =

FPR = TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT15D-4B

Manufacturer: Pratt & Whitney

Application: Citation S/II

Composition: 1 / 1B / 1C / 1 / - / 2

$D_{fan} = 0.528 \text{ m} = 20.8 \text{ in}$ $D = 0.686 \text{ m}$

$W_{eng} = 258 \text{ kg} = 569 \text{ lb}$ $= 27 \text{ in}$

Static Sea Level:

$T_{ssl} = 11121 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 2500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.59 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.56 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.6

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 1.6 \text{ m}$

$= 63 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT15D-4C

Manufacturer: Pratt & Whitney

Application: S211

Composition: 1 / 1B / 1C / 1 / - / 2

$D_{fan} = 0.528 \text{ m} = 20.8 \text{ in}$ $D = 0.686 \text{ m}$

$W_{eng} = 261 \text{ kg} = 575 \text{ lb}$ $= 27 \text{ in}$

Static Sea Level:

$T_{ssl} = 11121 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 2500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.59 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.56 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.6

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 1.6 \text{ m}$

$= 63 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT15D-4D

Manufacturer: Pratt & Whitney

Application: Diamond IA

Composition: 1 / 1B / 1C / 1 / - / 2

$D_{fan} = 0.528 \text{ m} = 20.8 \text{ in}$ $D = 0.686 \text{ m}$

$W_{eng} = 254 \text{ kg} = 560 \text{ lb}$ $= 27 \text{ in}$

Static Sea Level:

$T_{ssl} = 11121 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 2500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.59 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.56 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.6

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 1.6 \text{ m}$

$= 63 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT15D-5

Manufacturer: Pratt & Whitney

Year: 1983

Application: Beechjet 400 (Diamond II), Beechjet 400A/400T, T-1A, T-47A, ARES, Citation Beech

Composition: 1 / 1B / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = 0.521 \text{ m} = 20.5 \text{ in}$ $D = 0.686 \text{ m}$

$L = 1.6 \text{ m}$

$W_{eng} = 287 \text{ kg} = 633 \text{ lb}$ $= 27 \text{ in}$

$= 63 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 13545 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3045 \text{ lbf}$ $= \text{lbf}$

$T_{cr} = 10738 \text{ N}$
 $= 2414 \text{ lbf}$

$SFC_{ssl} = 1.59 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.56 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$SFC_{cr} = 1.53 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.54 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 42.2 \text{ kg/s} = 93 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 3.3 OPR = 12.6

OPR_{cr} =

FPR = TET = 1288 °K

$M_{cr} = 0.8$, $h_{cr} = 12192 \text{ m}$

JT15D-5A

Manufacturer: Pratt & Whitney

Application: Citation V

Composition: 1 / 1B / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = 0.521 \text{ m} = 20.5 \text{ in}$ $D = 0.686 \text{ m}$

$L = 1.6 \text{ m}$

$W_{eng} = 287 \text{ kg} = 633 \text{ lb}$ $= 27 \text{ in}$

$= 63 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 12900 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2900 \text{ lbf}$ $= \text{lbf}$

$T_{cr} = \text{N}$
 $= \text{lbf}$

$SFC_{ssl} = 1.56 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.55 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 2 OPR = 12.6

OPR_{cr} =

FPR = TET = °K

$M_{cr} =$, $h_{cr} = \text{m}$

JT15D-5B

Manufacturer: Pratt & Whitney

Application: T-1A

Composition: 1 / 1B / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = 12900 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2900 \text{ lbf}$ $= \text{lbf}$

$T_{cr} = \text{N}$
 $= \text{lbf}$

$SFC_{ssl} = 1.56 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.55 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

OPR_{cr} =

FPR = TET = °K

$M_{cr} =$, $h_{cr} = \text{m}$

JT15D-5C

Manufacturer: Pratt & Whitney

Application: S211A, S.211A, X-47A/B, Bird of Prey, X-45A (candidate engine)

Composition: 1 / 1B / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = 0.521 \text{ m} = 20.5 \text{ in}$ $D = 0.686 \text{ m}$

$L = 1.6 \text{ m}$

$W_{eng} = 302 \text{ kg} = 666 \text{ lb}$ $= 27 \text{ in}$

$= 63 \text{ in}$

Static Sea Level:

$T_{ssl} = 14190 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3190 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.56 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.55 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 2$ $\text{OPR} = 13.5$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

JT15D-5D

Manufacturer: Pratt & Whitney

Application: Citation V Ultra, VisionAire Vantage, UC-35C

Composition: 1 / 1B / 1C / 1 / - / 2

Nb of shafts = 2

$D_{fan} = 0.521 \text{ m} = 20.5 \text{ in}$ $D = 0.686 \text{ m}$

$L = 1.6 \text{ m}$

$W_{eng} = 284 \text{ kg} = 626 \text{ lb}$ $= 27 \text{ in}$

$= 63 \text{ in}$

Static Sea Level:

$T_{ssl} = 13545 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3045 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.56 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.55 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 2$ $\text{OPR} = 13.1$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

JT3C-12

Manufacturer: Pratt & Whitney

Application: B720, B720F, B707-120 (option)

Composition: - / 9 / 7 / 1 / - / 2

Nb of shafts = 2

$D_{fan} = 0.986 \text{ m} = 38.8 \text{ in}$ $D = \text{m}$

$L = 3.52 \text{ m}$

$W_{eng} = 1610 \text{ kg} = 3549 \text{ lb}$ $= \text{in}$

$= 138.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 53378 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 12000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 2.2 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.77 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 84.8 \text{ kg/s} = 187 \text{ lb/s}$

$\text{BPR} =$ $\text{OPR} = 13.8$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

JT3C-2

Manufacturer: Pratt & Whitney

Application: DC-8-11/-12

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = 0.986 \text{ m} = 38.8 \text{ in}$ $D = 0.988 \text{ m}$

$W_{eng} = 1755 \text{ kg} = 3869 \text{ lb}$ $= 38.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 49820 \text{ N}$ $T_{ssl}^{AB} = 61163 \text{ N}$
 $= 11200 \text{ lbf}$ $= 13750 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = 2.69 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= 0.95 (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.52 \text{ m}$

$= 138.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT3C-4

Manufacturer: Pratt & Whitney

Application: B707-120, B720

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = 0.986 \text{ m} = 38.8 \text{ in}$ $D = 0.988 \text{ m}$

$W_{eng} = \text{kg} = \text{lb}$ $= 38.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 49820 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 11200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.52 \text{ m}$

$= 138.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT3C-6

Manufacturer: Pratt & Whitney

Application: B707-120, DC-8-11/-12

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = 0.986 \text{ m} = 38.8 \text{ in}$ $D = 0.988 \text{ m}$

$W_{eng} = 1921 \text{ kg} = 4235 \text{ lb}$ $= 38.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 49820 \text{ N}$ $T_{ssl}^{AB} = 60051 \text{ N}$
 $= 11200 \text{ lbf}$ $= 13500 \text{ lbf}$

$SFC_{ssl} = 2.2 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.77 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.52 \text{ m}$

$= 138.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT3C-7

Manufacturer: Pratt & Whitney

Year: 1957

Application: B720, B720F

Composition: - / 9 / 7 / 1 / - / 2

 $D_{fan} = 0.986 \text{ m} = 38.8 \text{ in}$ $D = 0.988 \text{ m}$
 $W_{eng} = 1585 \text{ kg} = 3494 \text{ lb}$ $= 38.9 \text{ in}$

Static Sea Level:

 $T_{ssl} = 53378 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 12000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 2.22 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.79 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 84.8 \text{ kg/s} = 187 \text{ lb/s}$
 $BPR = 0$ $OPR = 13$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 3.52 \text{ m}$
 $= 138.6 \text{ in}$

Cruise:

 $T_{cr} = 15107 \text{ N}$
 $= 3396 \text{ lbf}$
 $SFC_{cr} = 2.55 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.9 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8, h_{cr} = 11000 \text{ m}$
JT3D-1

Manufacturer: Pratt & Whitney

Application: B707-120B/-120BF, B720B, B720BF, DC-8-51/52

Composition: 2 / 6B / 7 / 1 / - / 3

 $D_{fan} = 1.349 \text{ m} = 53.1 \text{ in}$ $D = 1.346 \text{ m}$
 $W_{eng} = 1880 \text{ kg} = 4145 \text{ lb}$ $= 53 \text{ in}$

Static Sea Level:

 $T_{ssl} = 75619 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 17000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.47 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.52 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 204.1 \text{ kg/s} = 450 \text{ lb/s}$
 $BPR = 1.4$ $OPR = 12.5$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 3.462 \text{ m}$
 $= 136.3 \text{ in}$

Cruise:

 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} =, h_{cr} = \text{m}$
JT3D-3

Manufacturer: Pratt & Whitney

Year: 1958

Application: B707-120B/-320B/-320C, B720B, DC-8-51/-51F/-52/-52F/-53/-53F/-54/-54F/-55/-55F/-61/-61F/-62/-62F

Composition: 2 / 6B / 7 / 1 / - / 3

 $D_{fan} = 1.285 \text{ m} = 50.6 \text{ in}$ $D = 1.346 \text{ m}$
 $W_{eng} = 2170 \text{ kg} = 4784 \text{ lb}$ $= 53 \text{ in}$

Static Sea Level:

 $T_{ssl} = 80148 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 18018 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.77 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 236 \text{ kg/s} = 520.3 \text{ lb/s}$
 $BPR = 1.25$ $OPR = 16$
 $FPR = 1.75$ $TET = 1233 ^\circ\text{K}$

Nb of shafts = 2

 $L = 3.6 \text{ m}$
 $= 141.7 \text{ in}$

Cruise:

 $T_{cr} = 22300 \text{ N}$
 $= 5013 \text{ lbf}$
 $SFC_{cr} = 2.16 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.76 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8, h_{cr} = 10600 \text{ m}$

JT3D-3B

Manufacturer: Pratt & Whitney

Application: B707-120B, B707-320B/BH/C/CH, B720B/BF, DC-8-53F/-55/-62/-62F, EC/RC-135, EC-24A

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.349 \text{ m} = 53.1 \text{ in}$ $D = 1.346 \text{ m}$

$W_{eng} = 1950 \text{ kg} = 4299 \text{ lb}$ $= 53 \text{ in}$

Static Sea Level:

$T_{ssl} = 80068 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 18000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.52 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.53 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 207.7 \text{ kg/s} = 457.9 \text{ lb/s}$

BPR = 1.37 OPR = 13.6

FPR = 1.74 TET = 1144 °K

Nb of shafts = 2

$L = 3.465 \text{ m}$

$= 136.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT3D-3C

Manufacturer: Pratt & Whitney

Application: DC8-50/61/61F/62/63, B707-120B/320B/C, B720B, VC-137C

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.349 \text{ m} = 53.1 \text{ in}$ $D = 1.346 \text{ m}$

$W_{eng} = 1969 \text{ kg} = 4341 \text{ lb}$ $= 53 \text{ in}$

Static Sea Level:

$T_{ssl} = 80068 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 18000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.45 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.51 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 204.1 \text{ kg/s} = 450 \text{ lb/s}$

BPR = 1.4 OPR = 13

FPR = 1.66 TET = °K

Nb of shafts = 2

$L = 3.696 \text{ m}$

$= 145.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT3D-7

Manufacturer: Pratt & Whitney

Application: B707-320B/-320C, DC-8-62/-62F/-63/-63F

Composition: 2 / 7B / 7 / 1 / - / 3

$D_{fan} = 1.349 \text{ m} = 53.1 \text{ in}$ $D = 1.346 \text{ m}$

$W_{eng} = 1969 \text{ kg} = 4341 \text{ lb}$ $= 53 \text{ in}$

Static Sea Level:

$T_{ssl} = 84516 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 19000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.47 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.52 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 214.1 \text{ kg/s} = 472 \text{ lb/s}$

BPR = 1.43 OPR = 13.5

FPR = 1.82 TET = °K

Nb of shafts = 2

$L = 3.696 \text{ m}$

$= 145.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT3D-7A

Manufacturer: Pratt & Whitney

Application: B707-320B/C/F, DC8-63/63F

Composition: 2 / 7B / 7 / 1 / - / 3

$D_{fan} = 1.349 \text{ m} = 53.1 \text{ in}$ $D = 1.346 \text{ m}$

$W_{eng} = 1969 \text{ kg} = 4341 \text{ lb}$ $= 53 \text{ in}$

Static Sea Level:

$T_{ssl} = 84516 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 19000 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 1.47 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.52 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 214.1 \text{ kg/s} = 472 \text{ lb/s}$
 $\text{BPR} = 1.43$ $\text{OPR} = 13.5$
 $\text{FPR} = 1.82$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.696 \text{ m}$

$= 145.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

JT3D-7B

Manufacturer: Pratt & Whitney

Application: C-22, C-9, T-43A

Composition: 2 / 7B / 7 / 1 / - / 3

$D_{fan} = 1.349 \text{ m} = 53.1 \text{ in}$ $D = 1.143 \text{ m}$

$W_{eng} = 1475 \text{ kg} = 3252 \text{ lb}$ $= 45 \text{ in}$

Static Sea Level:

$T_{ssl} = 64499 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 14500 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 1.66 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.58 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 144.2 \text{ kg/s} = 317.9 \text{ lb/s}$
 $\text{BPR} = 1.03$ $\text{OPR} = 16.9$
 $\text{FPR} =$ $\text{TET} = 853 ^\circ\text{K}$

Nb of shafts = 2

$L = 3.142 \text{ m}$

$= 123.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

JT4A-10

Manufacturer: Pratt & Whitney

Application: B707-320

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.092 \text{ m}$

$W_{eng} = 2313 \text{ kg} = 5099 \text{ lb}$ $= 43 \text{ in}$

Static Sea Level:

$T_{ssl} = 74730 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 16800 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 2.29 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.81 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $\text{BPR} =$ $\text{OPR} =$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.66 \text{ m}$

$= 144.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

JT4A-11

Manufacturer: Pratt & Whitney

Year: 1956

Application: DC-8-33F/-33F(AF), B707-320 (option)

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = \text{m}$

$W_{eng} = 2313 \text{ kg} = 5099 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 77844 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 17500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.38 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.84 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 116.1 \text{ kg/s} = 256 \text{ lb/s}$

BPR = OPR = 12.5

FPR = TET = °K

Nb of shafts = 2

$L = 3.66 \text{ m}$

$= 144.1 \text{ in}$

Cruise:

$T_{cr} = 20895 \text{ N}$

$= 4697 \text{ lbf}$

$SFC_{cr} = 2.61 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.92 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8$, $h_{cr} = 11000 \text{ m}$

JT4A-12

Manufacturer: Pratt & Whitney

Application: B707-320/-320F

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = \text{m}$

$W_{eng} = 2220 \text{ kg} = 4894 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 77844 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 17500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.38 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.84 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 116.1 \text{ kg/s} = 256 \text{ lb/s}$

BPR = OPR = 12.5

FPR = TET = °K

Nb of shafts = 2

$L = 3.66 \text{ m}$

$= 144.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

JT4A-3

Manufacturer: Pratt & Whitney

Application: B707-220, DC-8-21/-21F

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = \text{m}$

$W_{eng} = 2277 \text{ kg} = 5020 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 70282 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 15800 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.77 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.66 \text{ m}$

$= 144.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

JT4A-5

Manufacturer: Pratt & Whitney

Application: B707-220

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = \text{m}$

$W_{eng} = 2184 \text{ kg} = 4815 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 70282 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 15800 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.77 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.66 \text{ m}$

$= 144.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT4A-7

Manufacturer: Pratt & Whitney

Application: B707-320

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 70282 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 15800 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.77 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT4A-9

Manufacturer: Pratt & Whitney

Application: DC-8-21/-21F/-33F/-33F(AF)

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.092 \text{ m}$

$W_{eng} = 2291 \text{ kg} = 5051 \text{ lb}$ $= 43 \text{ in}$

Static Sea Level:

$T_{ssl} = 74730 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 16800 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.29 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.81 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.66 \text{ m}$

$= 144.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT4B-21

Manufacturer: Pratt & Whitney

Application: XB-68A (not produced)

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 72728 \text{ N}$ $T_{ssl}^{AB} = 122326 \text{ N}$
 $= 16350 \text{ lbf}$ $= 27500 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

JT8D-1

Manufacturer: Pratt & Whitney

Application: Caravelle 10B1R/10B3, DC-9-15

Composition: 2 / 4B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$
 $W_{eng} = 1404 \text{ kg} = 3095 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 62275 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 14000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = 1.66 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.58 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 142.9 \text{ kg/s} = 315 \text{ lb/s}$
 $BPR = 1.06$ $OPR = 15.4$
 $FPR = 1.9$ $TET = ^\circ K$

Nb of shafts = 2

$L = 3.137 \text{ m}$
 $= 123.5 \text{ in}$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

JT8D-11

Manufacturer: Pratt & Whitney

Application: DC-9-21/-32/-41

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$
 $W_{eng} = 1501 \text{ kg} = 3309 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 66723 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 15000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = 1.76 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.62 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 148.3 \text{ kg/s} = 326.9 \text{ lb/s}$
 $BPR = 1.05$ $OPR = 16.2$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = 3.137 \text{ m}$
 $= 123.5 \text{ in}$

Cruise:

$T_{cr} = 21129 \text{ N}$
 $= 4750 \text{ lbf}$
 $SFC_{cr} = 2.28 \cdot 10^{-5} (kg/s)/N$
 $= 0.81 (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-15

Manufacturer: Pratt & Whitney

Application: B727-200/-200A/-200F/-200AF, B737-200A/-200CA, DC-9-33/-34/-41, Mercure-100, C-22C

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1549 \text{ kg} = 3415 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 68947 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 15500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.63 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 146.1 \text{ kg/s} = 322.1 \text{ lb/s}$

$\text{BPR} = 1.03$ $\text{OPR} = 16.5$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 21885 \text{ N}$

$= 4920 \text{ lbf}$

$\text{SFC}_{cr} = 2.29 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.81 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-15A

Manufacturer: Pratt & Whitney

Application: B727-200A, B737-200A/-200CA, DC-9-30/-40/-50

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1576 \text{ kg} = 3474 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 68947 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 15500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.67 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.59 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 148.3 \text{ kg/s} = 326.9 \text{ lb/s}$

$\text{BPR} = 1.04$ $\text{OPR} = 16.6$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 21885 \text{ N}$

$= 4920 \text{ lbf}$

$\text{SFC}_{cr} = 2.29 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.81 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-17

Manufacturer: Pratt & Whitney

Application: B727-200A/-200AF, B737-200/-200A/-200CA/-200F/-200AF, DC-9-31/-32/-34/-34F(CF)/-51, YC-15

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1556 \text{ kg} = 3430 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 71171 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 16000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 147 \text{ kg/s} = 324.1 \text{ lb/s}$

$\text{BPR} = 1.01$ $\text{OPR} = 16.9$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 22864 \text{ N}$

$= 5140 \text{ lbf}$

$\text{SFC}_{cr} = 2.31 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.81 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-17A

Manufacturer: Pratt & Whitney

Application: B727-200A, B737-200A/-200CA/-200AF, DC-9-41/-51

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1576 \text{ kg} = 3474 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 71171 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 16000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 148.8 \text{ kg/s} = 328 \text{ lb/s}$

$BPR = 1.02$ $OPR = 17.1$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 22864 \text{ N}$

$= 5140 \text{ lbf}$

$SFC_{cr} = 2.19 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.77 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-17AR

Manufacturer: Pratt & Whitney

Application: B727-200A, B737-200

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1585 \text{ kg} = 3494 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 72950 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 16400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.73 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.61 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 147.9 \text{ kg/s} = 326.1 \text{ lb/s}$

$BPR = 1$ $OPR = 17.3$

$FPR = 2.16$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 22864 \text{ N}$

$= 5140 \text{ lbf}$

$SFC_{cr} = 2.21 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.78 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-17R

Manufacturer: Pratt & Whitney

Application: B727-200/-200A/-200AF

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1585 \text{ kg} = 3494 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 77399 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 17400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 150.1 \text{ kg/s} = 330.9 \text{ lb/s}$

$BPR = 1$ $OPR = 17.5$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 22864 \text{ N}$

$= 5140 \text{ lbf}$

$SFC_{cr} = 2.32 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.82 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-1A

Manufacturer: Pratt & Whitney

Application: B727-100/100C, DC9-10/20/30, Caravelle 10B/10R

Composition: 2 / 4B / 7 / 1 / - / 3

Nb of shafts = 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$L = 3.137 \text{ m}$

$W_{eng} = 1404 \text{ kg} = 3095 \text{ lb}$ $= 42.5 \text{ in}$

$= 123.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 62275 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 14000 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 1.66 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.58 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 142.9 \text{ kg/s} = 315 \text{ lb/s}$
 $\text{BPR} = 1.06$ $\text{OPR} = 15.4$
 $\text{FPR} = 1.9$ $\text{TET} = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

JT8D-1B

Manufacturer: Pratt & Whitney

Application:

Composition: 2 / 4B / 7 / 1 / - / 3

Nb of shafts = 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$L = 3.137 \text{ m}$

$W_{eng} = 1404 \text{ kg} = 3095 \text{ lb}$ $= 42.5 \text{ in}$

$= 123.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 62275 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 14000 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 1.66 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.58 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 142.9 \text{ kg/s} = 315 \text{ lb/s}$
 $\text{BPR} = 1.06$ $\text{OPR} = 15.4$
 $\text{FPR} = 1.9$ $\text{TET} = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $\text{SFC}_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

JT8D-209

Manufacturer: Pratt & Whitney

Application: MD-81

Composition: 1 / 6B / 7 / 1 / - / 3

Nb of shafts = 2

$D_{fan} = 1.25 \text{ m} = 49.2 \text{ in}$ $D = \text{m}$

$L = 3.917 \text{ m}$

$W_{eng} = 2000 \text{ kg} = 4409 \text{ lb}$ $= \text{in}$

$= 154.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 82292 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 18500 \text{ lbf}$ $= \text{lbf}$
 $\text{SFC}_{ssl} = 1.45 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.51 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 213.6 \text{ kg/s} = 470.9 \text{ lb/s}$
 $\text{BPR} = 1.82$ $\text{OPR} = 17.4$
 $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Cruise:

$T_{cr} = 21996 \text{ N}$
 $= 4945 \text{ lbf}$
 $\text{SFC}_{cr} = 2.05 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.72 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $\text{OPR}_{cr} =$
 $M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

JT8D-217

Manufacturer: Pratt & Whitney

Application: MD-81/-82

Composition: 1 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.25 \text{ m} = 49.2 \text{ in}$ $D = \text{m}$

$W_{eng} = 2009 \text{ kg} = 4429 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 88964 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 20000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.5 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.53 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 220.4 \text{ kg/s} = 485.9 \text{ lb/s}$

$BPR = 1.77$ $OPR = 18.6$

$FPR = 1.75$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 23309 \text{ N}$

$= 5240 \text{ lbf}$

$SFC_{cr} = 2.13 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.75 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} = 19.4$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

JT8D-217A

Manufacturer: Pratt & Whitney

Application: MD-81/-82/-82(SA)

Composition: 1 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.25 \text{ m} = 49.2 \text{ in}$ $D = \text{m}$

$W_{eng} = 2009 \text{ kg} = 4429 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 88964 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 20000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.5 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.53 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 220.4 \text{ kg/s} = 485.9 \text{ lb/s}$

$BPR = 1.77$ $OPR = 18.6$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 23309 \text{ N}$

$= 5240 \text{ lbf}$

$SFC_{cr} = 2.13 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.75 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

JT8D-217C

Manufacturer: Pratt & Whitney

Application: B727-100(RE)/-200A(RE)/-200AF(RE), MD-81/-82/-87/-88

Composition: 1 / 6B / 7 / 1 / - / 3

$D_{fan} = 1.25 \text{ m} = 49.2 \text{ in}$ $D = \text{m}$

$W_{eng} = 2041 \text{ kg} = 4500 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 88964 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 20000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.42 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.5 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 225.4 \text{ kg/s} = 496.9 \text{ lb/s}$

$BPR = 1.72$ $OPR = 20.1$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 23309 \text{ N}$

$= 5240 \text{ lbf}$

$SFC_{cr} = 2.09 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.74 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

JT8D-219

Manufacturer: Pratt & Whitney

Year: 1986

Application: MD-82/-83/-87/-88, B707-330C(RE), B727-200AF(RE)

Composition: 1 / 6B / 7 / 1 / - / 3

Nb of shafts = 2

$D_{fan} = 1.25 \text{ m} = 49.2 \text{ in}$ $D = 1.43 \text{ m}$

$L = 3.917 \text{ m}$

$W_{eng} = 2048 \text{ kg} = 4515 \text{ lb}$ $= 56.3 \text{ in}$

$= 154.2 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 96526 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = 23309 \text{ N}$

$= 21700 \text{ lbf}$ $= \text{lbf}$

$= 5240 \text{ lbf}$

$\text{SFC}_{ssl} = 1.47 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = 2.09 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.52 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= 0.74 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 221.4 \text{ kg/s} = 488.1 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 1.77 OPR = 19.2

OPR_{cr} =

FPR = 1.91 TET = 1411 °K

$M_{cr} = 0.76$, $h_{cr} = 10668 \text{ m}$

JT8D-5

Manufacturer: Pratt & Whitney

Application: DC-9-11

Composition: 2 / 4B / 7 / 1 / - / 3

Nb of shafts = 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$L = 3.137 \text{ m}$

$W_{eng} = 1404 \text{ kg} = 3095 \text{ lb}$ $= 42.5 \text{ in}$

$= 123.5 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 54490 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 12250 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$\text{SFC}_{ssl} = 1.6 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= 0.56 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

OPR_{cr} =

FPR = TET = °K

$M_{cr} =$, $h_{cr} = \text{m}$

JT8D-7

Manufacturer: Pratt & Whitney

Year: 1961

Application: B727-100/-100C/-100QC/-100F/-200/-200F, B737-100/-200A/-200CA, DC-9-15/-15F(RC)/-31, Caravelle 10B1R/10B3/11R, C-22B

Composition: 2 / 4B / 7 / 1 / - / 3

Nb of shafts = 2

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$L = 3.137 \text{ m}$

$W_{eng} = 1431 \text{ kg} = 3155 \text{ lb}$ $= 42.5 \text{ in}$

$= 123.5 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 62275 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = 18994 \text{ N}$

$= 14000 \text{ lbf}$ $= \text{lbf}$

$= 4270 \text{ lbf}$

$\text{SFC}_{ssl} = 1.66 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$\text{SFC}_{cr} = 2.26 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= 0.8 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 142.9 \text{ kg/s} = 315 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 1.07 OPR = 15.8

OPR_{cr} =

FPR = 1.93 TET = °K

$M_{cr} = 0.8$, $h_{cr} = 9144 \text{ m}$

JT8D-7A

Manufacturer: Pratt & Whitney

Application: B727-100/-100C/-100QC/-100F/-200, B737-100/-200, DC-9-14/-15/-15F(MC)/-31/-31

Composition: 2 / 4B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1404 \text{ kg} = 3095 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 62275 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 14000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.66 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 142.9 \text{ kg/s} = 315 \text{ lb/s}$

$\text{BPR} = 1.07$ $\text{OPR} = 15.8$

$\text{FPR} = 1.93$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 18994 \text{ N}$

$= 4270 \text{ lbf}$

$\text{SFC}_{cr} = 2.26 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.8 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-7B

Manufacturer: Pratt & Whitney

Application: B727-100/-100C/-100F/-200/-200A/-200F, B737-100/-200, DC-9-14/-15/-15F(MC)/-15F(RC)/-31/-31F/-32

Composition: 2 / 4B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1404 \text{ kg} = 3095 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 62275 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 14000 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.66 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 142.9 \text{ kg/s} = 315 \text{ lb/s}$

$\text{BPR} = 1.07$ $\text{OPR} = 15.8$

$\text{FPR} = 1.93$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 18994 \text{ N}$

$= 4270 \text{ lbf}$

$\text{SFC}_{cr} = 2.26 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.8 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-9

Manufacturer: Pratt & Whitney

Application: B727-100/-100C/-200/-200A, B737-200/-200A/-200C/-200CA, DC-9-32/-32F/-33F/-33F(RC), Caravelle 10B3/12

Composition: 2 / 4B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1450 \text{ kg} = 3197 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 64499 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 14500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.6 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.56 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 144.7 \text{ kg/s} = 319 \text{ lb/s}$

$\text{BPR} = 1.03$ $\text{OPR} = 15.9$

$\text{FPR} = 1.91$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 20195 \text{ N}$

$= 4540 \text{ lbf}$

$\text{SFC}_{cr} = 2.27 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.8 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-9A

Manufacturer: Pratt & Whitney

Application: B727-100/-100C/-100F/-200/-200A/-200AF/-200F, B737-100/-200/-200A/-200C/-200CA/-200AF, DC-9-31/-32/-32F/-33F(RC), C-9A/B/C, VC-9C, T-43A, CT-43A, NT-43A

Composition: 2 / 4B / 7 / 1 / - / 3

$D_{fan} = 1.08 \text{ m} = 42.5 \text{ in}$ $D = 1.08 \text{ m}$

$W_{eng} = 1450 \text{ kg} = 3197 \text{ lb}$ $= 42.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 64499 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 14500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.6 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.56 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 144.7 \text{ kg/s} = 319 \text{ lb/s}$

BPR = 1.03 OPR = 15.9

FPR = 1.91 TET = °K

Nb of shafts = 2

$L = 3.137 \text{ m}$

$= 123.5 \text{ in}$

Cruise:

$T_{cr} = 20195 \text{ N}$

$= 4540 \text{ lbf}$

$SFC_{cr} = 2.27 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.8 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

JT8D-M-9

Manufacturer: Mitsubishi

Application: C-1

Composition: 2 / 4B / 7 / 1 / - / 3

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 64499 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 14500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 1.03 OPR = 15.9

FPR = 1.91 TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT9D-1

Manufacturer: Pratt & Whitney

Application: B747-100 (option)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 186824 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 42000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 673.1 \text{ kg/s} = 1483.9 \text{ lb/s}$

BPR = 5 OPR = 21.5

FPR = 1.6 TET = °K

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT9D-15

Manufacturer: Pratt & Whitney

Application: DC-10-20/-40 (option), MD-11 (proposed)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 202393 \text{ N}$ $T_{ssl}^{AB} = 209065 \text{ N}$

$= 45500 \text{ lbf}$ $= 47000 \text{ lbf}$

$SFC_{ssl} = 1.01 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT9D-20

Manufacturer: Pratt & Whitney

Application: DC-10-40, MD-11 (proposed)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 3833 \text{ kg} = 8450 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 205952 \text{ N}$ $T_{ssl}^{AB} = 219741 \text{ N}$

$= 46300 \text{ lbf}$ $= 49400 \text{ lbf}$

$SFC_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 689.9 \text{ kg/s} = 1521 \text{ lb/s}$

BPR = 5.2

OPR = 21.1

FPR =

TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 47507 \text{ N}$

$= 10680 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-20J

Manufacturer: Pratt & Whitney

Application: DC-10-40, MD-11 (proposed)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 3833 \text{ kg} = 8450 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 205952 \text{ N}$ $T_{ssl}^{AB} = 219741 \text{ N}$

$= 46300 \text{ lbf}$ $= 49400 \text{ lbf}$

$SFC_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 689.9 \text{ kg/s} = 1521 \text{ lb/s}$

BPR = 5.2

OPR = 23.5

FPR =

TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 47507 \text{ N}$

$= 10680 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-25

Manufacturer: Pratt & Whitney

Application: DC-10-20 (option), MD-11 (proposed)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 209065 \text{ N}$ $T_{ssl}^{AB} = 222410 \text{ N}$

$= 47000 \text{ lbf}$ $= 50000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.2 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT9D-3

Manufacturer: Pratt & Whitney

Application: B747-100 (option)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 3824 \text{ kg} = 8430 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 193497 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 43500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.98 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.35 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.2 OPR = 22

FPR = 1.51 TET = °K

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JT9D-3A

Manufacturer: Pratt & Whitney

Application: B747-100

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 3905 \text{ kg} = 8609 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 196833 \text{ N}$ $T_{ssl}^{AB} = 203728 \text{ N}$

$= 44250 \text{ lbf}$ $= 45800 \text{ lbf}$

$SFC_{ssl} = 0.98 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.35 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 684.5 \text{ kg/s} = 1509.1 \text{ lb/s}$

BPR = 5.2 OPR = 21.5

FPR = 1.51 TET = °K

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 45372 \text{ N}$

$= 10200 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.62 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-59

Manufacturer: Pratt & Whitney

Application: A300B4-120/-220/-220F/-220FF (option)

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4146 \text{ kg} = 9140 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 235755 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 53000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.06 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 743.4 \text{ kg/s} = 1638.9 \text{ lb/s}$

$BPR = 4.9$ $OPR = 24.5$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 53156 \text{ N}$

$= 11950 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-59A

Manufacturer: Pratt & Whitney

Application: A300B4-120/-220/-220F/-220FF, DC-10-40(D)/-40(I)/-40F, A300B4-320 (option)

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4146 \text{ kg} = 9140 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 230150 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 51740 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.06 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 743.4 \text{ kg/s} = 1638.9 \text{ lb/s}$

$BPR = 4.9$ $OPR = 24.5$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 53156 \text{ N}$

$= 11950 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-59B

Manufacturer: Pratt & Whitney

Application:

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4155 \text{ kg} = 9160 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 242427 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 54500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 753 \text{ kg/s} = 1660.1 \text{ lb/s}$

$BPR = 4.8$ $OPR = 25.2$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 54268 \text{ N}$

$= 12200 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7
Manufacturer: Pratt & Whitney

Application: B747-100/-200B/C/F/SR

Composition: 1 / 3B / 11 / 2 / - / 4

 $D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$
 $W_{eng} = 4014 \text{ kg} = 8849 \text{ lb}$ $= \text{in}$
Static Sea Level:
 $T_{ssl} = 205952 \text{ N}$ $T_{ssl}^{AB} = 213069 \text{ N}$
 $= 46300 \text{ lbf}$ $= 47900 \text{ lbf}$
 $SFC_{ssl} = 1.01 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 689.9 \text{ kg/s} = 1521 \text{ lb/s}$
 $BPR = 5.2$ $OPR = 22.3$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 3.917 \text{ m}$
 $= 154.2 \text{ in}$
Cruise:
 $T_{cr} = 45372 \text{ N}$
 $= 10200 \text{ lbf}$
 $SFC_{cr} = 1.76 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.62 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$
JT9D-70A
Manufacturer: Pratt & Whitney

Application: B747-200B/-200B(M)/-200B(SF)/-200F

Composition: 1 / 4B / 11 / 2 / - / 4

 $D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$
 $W_{eng} = 4153 \text{ kg} = 9156 \text{ lb}$ $= \text{in}$
Static Sea Level:
 $T_{ssl} = 235755 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 53000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.06 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 743.4 \text{ kg/s} = 1638.9 \text{ lb/s}$
 $BPR = 4.9$ $OPR = 24.5$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 3.901 \text{ m}$
 $= 153.6 \text{ in}$
Cruise:
 $T_{cr} = 53156 \text{ N}$
 $= 11950 \text{ lbf}$
 $SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.63 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$
JT9D-70B
Manufacturer: Pratt & Whitney

Application:
Composition: 1 / 4B / 11 / 2 / - / 4

 $D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$
 $W_{eng} = 4162 \text{ kg} = 9176 \text{ lb}$ $= \text{in}$
Static Sea Level:
 $T_{ssl} = 242427 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 54500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 753 \text{ kg/s} = 1660.1 \text{ lb/s}$
 $BPR = 4.8$ $OPR = 25.2$
 $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 3.901 \text{ m}$
 $= 153.6 \text{ in}$
Cruise:
 $T_{cr} = 54268 \text{ N}$
 $= 12200 \text{ lbf}$
 $SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.63 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7A

Manufacturer: Pratt & Whitney

Application: B747-SF/-SP/-100/-100A/-100(SF)/-100F/-100SR/-100SRB/-100SR(SF)/-200/-200B/-200C

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 3982 \text{ kg} = 8779 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 208843 \text{ N}$ $T_{ssl}^{AB} = 216049 \text{ N}$

$= 46950 \text{ lbf}$ $= 48570 \text{ lbf}$

$SFC_{ssl} = 1.03 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 695.8 \text{ kg/s} = 1534 \text{ lb/s}$

$BPR = 5.1$ $OPR = 22.5$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 48174 \text{ N}$

$= 10830 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7AH

Manufacturer: Pratt & Whitney

Application: B747-SP/-100/-100(SF)/-100F/-200B

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4014 \text{ kg} = 8849 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 208843 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 46950 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 5.2$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

JT9D-7ASP

Manufacturer: Pratt & Whitney

Application: B747-SP (option)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 3983 \text{ kg} = 8781 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 208843 \text{ N}$ $T_{ssl}^{AB} = 216049 \text{ N}$

$= 46950 \text{ lbf}$ $= 48570 \text{ lbf}$

$SFC_{ssl} = 1.03 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 695.8 \text{ kg/s} = 1534 \text{ lb/s}$

$BPR = 5.1$ $OPR = 22.5$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 47507 \text{ N}$

$= 10680 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7AW

Manufacturer: Pratt & Whitney

Application: B747-200B/-200(SF)/-100SR/-200F

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4014 \text{ kg} = 8849 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 208843 \text{ N}$ $T_{ssl}^{AB} = 216049 \text{ N}$

$= 46950 \text{ lbf}$ $= 48570 \text{ lbf}$

$SFC_{ssl} = 1.03 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 695.8 \text{ kg/s} = 1534 \text{ lb/s}$

$BPR = 5.1$ $OPR = 22.5$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 48174 \text{ N}$

$= 10830 \text{ lbf}$

$SFC_{cr} = 1.77 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7F

Manufacturer: Pratt & Whitney

Application: B747-SP/-100B/-200/-200B/-200B(M)/-200(SF)/-200F

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4014 \text{ kg} = 8849 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 213514 \text{ N}$ $T_{ssl}^{AB} = 222410 \text{ N}$

$= 48000 \text{ lbf}$ $= 50000 \text{ lbf}$

$SFC_{ssl} = 1.04 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 709.9 \text{ kg/s} = 1565.1 \text{ lb/s}$

$BPR = 5.1$ $OPR = 22.8$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 49153 \text{ N}$

$= 11050 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7FW

Manufacturer: Pratt & Whitney

Application: B747-SP/-200B(SF)/-200C(M)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4014 \text{ kg} = 8849 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 213514 \text{ N}$ $T_{ssl}^{AB} = 222410 \text{ N}$

$= 48000 \text{ lbf}$ $= 50000 \text{ lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 5.1$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

JT9D-7J

Manufacturer: Pratt & Whitney

Application: B747-100F/-200B/-200B(M)/-200B(SF)/-200C/-200F

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4014 \text{ kg} = 8849 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 721.2 \text{ kg/s} = 1590 \text{ lb/s}$

$BPR = 5.1$ $OPR = 23.5$

$FPR =$ $TET = ^\circ\text{K}$

$\text{Nb of shafts} = 2$

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = 49153 \text{ N}$

$= 11050 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.63 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7Q

Manufacturer: Pratt & Whitney

Application: B747-200B/-200B(M)/-200B(SF)/-200F

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4216 \text{ kg} = 9295 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 235755 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 53000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 743.9 \text{ kg/s} = 1640 \text{ lb/s}$

$BPR = 4.9$ $OPR = 24.5$

$FPR =$ $TET = ^\circ\text{K}$

$\text{Nb of shafts} = 2$

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 53156 \text{ N}$

$= 11950 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.63 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7Q3

Manufacturer: Pratt & Whitney

Application: B747-200B/-200B(M)/-200B(SF)

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = \text{m}$

$W_{eng} = 4216 \text{ kg} = 9295 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 235755 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 53000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 743.9 \text{ kg/s} = 1640 \text{ lb/s}$

$BPR = 4.9$ $OPR = 24.5$

$FPR =$ $TET = ^\circ\text{K}$

$\text{Nb of shafts} = 2$

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 53156 \text{ N}$

$= 11950 \text{ lbf}$

$SFC_{cr} = 1.79 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.63 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7R

Manufacturer: Pratt & Whitney

Application: B767-200/-200ER/-200ET/-200PC/-300

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.372 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4039 \text{ kg} = 8904 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 213514 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 48000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 718.9 \text{ kg/s} = 1584.9 \text{ lb/s}$

BPR = 4.9 OPR = 23.4

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 49820 \text{ N}$

$= 11200 \text{ lbf}$

$SFC_{cr} = 1.74 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.61 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7R4D

Manufacturer: Pratt & Whitney

Application: B767-200/-200ER/-200ET/-200PC/-300

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.372 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4039 \text{ kg} = 8904 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 213514 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 48000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.34 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 718.9 \text{ kg/s} = 1584.9 \text{ lb/s}$

BPR = 4.9 OPR = 23.4

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 49820 \text{ N}$

$= 11200 \text{ lbf}$

$SFC_{cr} = 1.74 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.61 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7R4D1

Manufacturer: Pratt & Whitney

Application: A310-221 (option)

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.372 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4039 \text{ kg} = 8904 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 213600 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 48019 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.34 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 718.9 \text{ kg/s} = 1584.9 \text{ lb/s}$

BPR = 4.9 OPR = 23.4

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 49820 \text{ N}$

$= 11200 \text{ lbf}$

$SFC_{cr} = 1.74 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.61 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7R4E

Manufacturer: Pratt & Whitney

Application: B767-200ER

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.372 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4039 \text{ kg} = 8904 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 732.5 \text{ kg/s} = 1614.9 \text{ lb/s}$

BPR = 4.9 OPR = 24.2

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 52044 \text{ N}$

$= 11700 \text{ lbf}$

$SFC_{cr} = 1.76 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7R4E1

Manufacturer: Pratt & Whitney

Application: A310-222/-222F/-322

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.372 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4039 \text{ kg} = 8904 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 222500 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50020 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 732.5 \text{ kg/s} = 1614.9 \text{ lb/s}$

BPR = 4.9 OPR = 24.2

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 52044 \text{ N}$

$= 11700 \text{ lbf}$

$SFC_{cr} = 1.76 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7R4E3

Manufacturer: Pratt & Whitney

Application: B767-200ER, E-3A

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.372 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4128 \text{ kg} = 9101 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 732.5 \text{ kg/s} = 1614.9 \text{ lb/s}$

BPR = 4.9 OPR = 24.2

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 52044 \text{ N}$

$= 11700 \text{ lbf}$

$SFC_{cr} = 1.76 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

JT9D-7R4E4

Manufacturer: Pratt & Whitney

Application: B767-200ER, E-4A

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.372 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4128 \text{ kg} = 9101 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.97 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 732.5 \text{ kg/s} = 1614.9 \text{ lb/s}$

BPR = 4.9 OPR = 24.2

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 52044 \text{ N}$

$= 11700 \text{ lbf}$

$SFC_{cr} = 1.76 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.62 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85$, $h_{cr} = 10668 \text{ m}$

JT9D-7R4G2

Manufacturer: Pratt & Whitney

Application: B747-200B/-200B(SF)/-200F/-300/-300(M)/-300(SF)

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.372 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4144 \text{ kg} = 9136 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 243539 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 54750 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 768.8 \text{ kg/s} = 1694.9 \text{ lb/s}$

BPR = 4.8 OPR = 26.3

FPR = TET = °K

Nb of shafts = 2

$L = 3.901 \text{ m}$

$= 153.6 \text{ in}$

Cruise:

$T_{cr} = 54490 \text{ N}$

$= 12250 \text{ lbf}$

$SFC_{cr} = 1.81 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.64 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85$, $h_{cr} = 10668 \text{ m}$

JT9D-7R4H1

Manufacturer: Pratt & Whitney

Application: A300B4-620, A310, B767, B747, DC10

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.373 \text{ m} = 93.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4040 \text{ kg} = 8907 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 249200 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 56022 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.03 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 768.8 \text{ kg/s} = 1694.9 \text{ lb/s}$

BPR = 4.8 OPR = 26.7

FPR = 1.68 TET = 1616 °K

Year: 1982

Nb of shafts = 2

$L = 3.92 \text{ m}$

$= 154.3 \text{ in}$

Cruise:

$T_{cr} = 54490 \text{ N}$

$= 12250 \text{ lbf}$

$SFC_{cr} = 1.78 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.63 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85$, $h_{cr} = 10670 \text{ m}$

JT9D-9

Manufacturer: Pratt & Whitney

Application: A300B2/B4

Composition: 1 / 3B / 11 / 2 / - / 4

$D_{fan} = 2.428 \text{ m} = 95.6 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 235755 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 53000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.917 \text{ m}$

$= 154.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JTF16

Manufacturer: Pratt & Whitney

Application:

Composition: 1 / / / /

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 44482 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 10000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

JTF17A-21

Manufacturer: Pratt & Whitney

Application: L-2000-7B (not produced), B-2707-200/-300 (candidate engine)

Composition: 2 / - / 6 / 1 / - / 2

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 170366 \text{ N}$ $T_{ssl}^{AB} = 271340 \text{ N}$
 $= 38300 \text{ lbf}$ $= 61000 \text{ lbf}$

$SFC_{ssl} = 2.12 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = 5.04 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.75 (\text{lb/h})/\text{lbf}$ $= 1.78 (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 306.2 \text{ kg/s} = 675.1 \text{ lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

K-15

Manufacturer: IL : Instytut Lotnictwa

Application: I-22

Composition: - / - / 6 / 1 / - / -

$D_{fan} = 0.725 \text{ m} = 28.5 \text{ in}$ $D = 0.892 \text{ m}$

$W_{eng} = 320 \text{ kg} = 705 \text{ lb}$ $= 35.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 14710 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3307 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.85 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 1.01 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 23.5 \text{ kg/s} = 51.8 \text{ lb/s}$

$BPR = 0$ $OPR = 5.3$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

$L = 1.56 \text{ m}$

$= 61.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Kaveri

Manufacturer: GTRE India

Application:

Composition: / / / /

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 52000 \text{ N}$ $T_{ssl}^{AB} = 81000 \text{ N}$

$= 11690 \text{ lbf}$ $= 18210 \text{ lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts =

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

KJ12

Manufacturer: KHI

Application:

Composition: - / - / 1C / 1 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = 0.315 \text{ m}$

$W_{eng} = 40 \text{ kg} = 88 \text{ lb}$ $= 12.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 1468 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 330 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

$L = 0.653 \text{ m}$

$= 25.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Larzac 04-C20

Manufacturer: Turboméca/SNECMA

Year: 1982

Application: Alpha Jet 2/3 ATS

Composition: 2 / - / 4 / 1 / - / 1

$D_{fan} = 0.452 \text{ m} = 17.8 \text{ in}$ $D = 0.653 \text{ m}$

$W_{eng} = 333 \text{ kg} = 734 \text{ lb}$ $= 25.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 14123 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3175 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.15 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.76 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 28.6 \text{ kg/s} = 63.1 \text{ lb/s}$

BPR = 1.04 OPR = 11.1

FPR = TET = 1433 °K

Nb of shafts = 2

$L = 2.1 \text{ m}$

$= 82.7 \text{ in}$

Cruise:

$T_{cr} = 12150 \text{ N}$

$= 2731 \text{ lbf}$

$SFC_{cr} = 3.16 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 1.12 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = \text{m}$

Larzac 04-C6

Manufacturer: Turboméca/SNECMA

Year: 1969

Application: Alphajet A/E

Composition: 2 / - / 4 / 1 / - / 1

$D_{fan} = 0.452 \text{ m} = 17.8 \text{ in}$ $D = 0.653 \text{ m}$

$W_{eng} = 332 \text{ kg} = 732 \text{ lb}$ $= 25.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 13200 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 2967 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.03 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.72 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 28.1 \text{ kg/s} = 61.9 \text{ lb/s}$

BPR = 1.13 OPR = 10.5

FPR = 2.3 TET = 1403 °K

Nb of shafts = 2

$L = 2.1 \text{ m}$

$= 82.7 \text{ in}$

Cruise:

$T_{cr} = 10900 \text{ N}$

$= 2450 \text{ lbf}$

$SFC_{cr} = 2.81 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.99 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 0 \text{ m}$

Larzac 04-R20

Manufacturer: Turboméca/SNECMA

Application: MiG-AT

Composition: 2 / - / 4 / 1 / - / 1

$D_{fan} = \text{m} = \text{in}$ $D = 0.653 \text{ m}$

$W_{eng} = 302 \text{ kg} = 666 \text{ lb}$ $= 25.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 14123 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3175 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.1 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.74 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 28.6 \text{ kg/s} = 63.1 \text{ lb/s}$

BPR = 1.04 OPR = 11.1

FPR = TET = °K

Nb of shafts = 2

$L = 1.179 \text{ m}$

$= 46.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Larzac 04-V3

Manufacturer: Turboméca/SNECMA

Application: I-22 Iryda

Composition: 2 / - / 4 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16178 N$ $T_{ssl}^{AB} = N$

$= 3637 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Larzac 49-01

Manufacturer: Turboméca/SNECMA

Application: Falcon 10, Corvette

Composition: 2 / - / 4 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 10231 N$ $T_{ssl}^{AB} = N$

$= 2300 lbf$ $= lbf$

$SFC_{ssl} = 1.73 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.61 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 25.9 kg/s = 57.1 lb/s$

BPR = 1.4 OPR = 9

FPR = 2 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

LF507

Manufacturer: ASE : AlliedSignal Engines

Application: BA146-300, Avro RJ

Composition: / / / /

$D_{fan} = 1.272 m = 50.1 in$ $D = m$

$W_{eng} = 628 kg = 1385 lb$ $= in$

Static Sea Level:

$T_{ssl} = 31138 N$ $T_{ssl}^{AB} = N$

$= 7000 lbf$ $= lbf$

$SFC_{ssl} = 1.12 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.4 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 116.1 kg/s = 256 lb/s$

BPR = 5.6 OPR = 13.8

FPR = 1.45 TET = °K

Year: 1991

Nb of shafts =

$L = 1.62 m$

$= 63.8 in$

Cruise:

$T_{cr} = N$

$= 0 lbf$

$SFC_{cr} = 1.98 \cdot 10^{-5} (kg/s)/N$

$= 0.7 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.7, h_{cr} = 8500 m$

LF507-1F

Manufacturer: Avco Lycoming

Application: RJ-70/-85/-100/-115

Composition: 3 / 7B / 1C / 2 / - / 2

$D_{fan} = 1.016 \text{ m} = 40 \text{ in}$ $D = 1.059 \text{ m}$

$W_{eng} = 628 \text{ kg} = 1385 \text{ lb}$ $= 41.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 31137 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.15 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.41 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 87.1 \text{ kg/s} = 192 \text{ lb/s}$

$BPR = 5.7$ $OPR = 13.8$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.487 \text{ m}$

$= 58.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

LF507-1H

Manufacturer: Avco Lycoming

Application: RJ-70/-85/-100/-115

Composition: 3 / 7B / 1C / 2 / - / 2

$D_{fan} = 1.016 \text{ m} = 40 \text{ in}$ $D = 1.059 \text{ m}$

$W_{eng} = 624 \text{ kg} = 1376 \text{ lb}$ $= 41.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 31137 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 5.7$ $OPR = 13.8$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.487 \text{ m}$

$= 58.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

LF507-1N

Manufacturer: Avco Lycoming

Application: Yak-40TL

Composition: 3 / 7B / 1C / 2 / - / 2

$D_{fan} = 1.016 \text{ m} = 40 \text{ in}$ $D = 1.059 \text{ m}$

$W_{eng} = 624 \text{ kg} = 1376 \text{ lb}$ $= 41.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 31137 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 7000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.487 \text{ m}$

$= 58.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

M-701S-50

Manufacturer: Motorlet

Application: L-29/-29A/-29R

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8718 N$ $T_{ssl}^{AB} = N$

$= 1960 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

M-701VC-150

Manufacturer: Motorlet

Application: L-29/-29A/-29R

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8718 N$ $T_{ssl}^{AB} = N$

$= 1960 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

M45H-01

Manufacturer: Rolls-Royce

Year: 1968

Application:

Composition: / / / / /

$D_{fan} = 0.909 m = 35.8 in$ $D = m$

$W_{eng} = 673 kg = 1484 lb$ $= in$

Static Sea Level:

$T_{ssl} = 34531 N$ $T_{ssl}^{AB} = N$

$= 7763 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 104 kg/s = 229.3 lb/s$

BPR = 2.8

OPR = 18

FPR =

TET = 1330 °K

Nb of shafts =

$L = 2.96 m$

$= 116.5 in$

Cruise:

$T_{cr} = 12213 N$

$= 2746 lbf$

$SFC_{cr} = 2.07 \cdot 10^{-5} (kg/s)/N$

$= 0.73 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.65 , h_{cr} = 6100 m$

M45H-C

Manufacturer: Rolls-Royce/SNECMA

Application:

Composition: 1 / 5B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 39144 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 8800 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

M45H-D Mk.501

Manufacturer: Rolls-Royce/SNECMA

Application: VFW 614 (not produced)

Composition: 1 / 5B / 7 / 1 / - / 3

$D_{fan} = 1.059 \text{ m} = 41.7 \text{ in}$ $D = m$

$W_{eng} = 673 \text{ kg} = 1484 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 34518 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 7760 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.28 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.45 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 105.7 \text{ kg/s} = 233 \text{ lb/s}$

BPR = 2.85 OPR = 18.8

FPR = 1.6 TET = °K

Nb of shafts = 2

$L = 2.959 \text{ m}$

$= 116.5 \text{ in}$

Cruise:

$T_{cr} = 12210 \text{ N}$

$= 2745 \text{ lbf}$

$SFC_{cr} = 2.05 \cdot 10^{-5} (kg/s)/N$

$= 0.73 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.65, h_{cr} = 6096 \text{ m}$

M45H-E1

Manufacturer: Rolls-Royce/SNECMA

Application:

Composition: 1 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 41146 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 9250 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

M45H-E2

Manufacturer: Rolls-Royce/SNECMA

Application:

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 42703 \text{ N}$ $T_{ssl}^{AB} = N$

$= 9600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

M53-2

Manufacturer: SNECMA

Application: Mirage 2000 prototypes, Mirage 4000 (not produced)

Composition: 3 / - / 5 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 54401 \text{ N}$ $T_{ssl}^{AB} = 83404 \text{ N}$

$= 12230 \text{ lbf}$ $= 18750 \text{ lbf}$

$SFC_{ssl} = 2.44 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.78 \cdot 10^{-5} (kg/s)/N$

$= 0.86 (lb/h)/lbf$ $= 2.04 (lb/h)/lbf$

$\dot{w}_{ssl} = 83.9 \text{ kg/s} = 185 \text{ lb/s}$

BPR = 0.4

OPR = 8.5

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

M53-5

Manufacturer: SNECMA

Application: Mirage 2000B/-C/-H/-TH/-M/-BM, G.4, G.8, Mirage 4000

Composition: 3 / - / 5 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 1.054 \text{ m}$

$L = 5.07 \text{ m}$

$W_{eng} = 1470 \text{ kg} = 3241 \text{ lb}$ $= 41.5 \text{ in}$

$= 199.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 54401 \text{ N}$ $T_{ssl}^{AB} = 88208 \text{ N}$

$= 12230 \text{ lbf}$ $= 19830 \text{ lbf}$

$SFC_{ssl} = 2.44 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.86 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR = 9

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

M53-P2

Manufacturer: SNECMA

Year: 1998

Application: Mirage 2000C/-D/-N-K1/-N-K2/-H/-TH/-P/-DP, Mirage 2000-5/-5F/-5EI/-5DI/-EDA/-DDA/-5Mk.2, Mirage 2000-9, Mirage 4000

Composition: 3 / - / 5 / 2 / - / -

Nb of shafts = 1

$D_{fan} = 0.792 \text{ m} = 31.2 \text{ in}$ $D = 1.054 \text{ m}$

$L = 5.07 \text{ m}$

$W_{eng} = 1500 \text{ kg} = 3307 \text{ lb}$ $= 41.5 \text{ in}$

$= 199.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 64000 \text{ N}$ $T_{ssl}^{AB} = 95000 \text{ N}$

$= 14388 \text{ lbf}$ $= 21357 \text{ lbf}$

$SFC_{ssl} = 2.56 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5.89 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.9 \text{ (lb/h)/lbf}$ $= 2.08 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 94.3 \text{ kg/s} = 207.9 \text{ lb/s}$

BPR = 0.35 OPR = 9.8

FPR = TET = 1533 °K

Cruise:

$T_{cr} = 35900 \text{ N}$

$= 8071 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= 0 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 2.2, h_{cr} = 16800 \text{ m}$

M88-2

Manufacturer: SNECMA

Year: 1996

Application: Rafale A,B,C,D,M

Composition: 3 / - / 6 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = 0.696 \text{ m} = 27.4 \text{ in}$ $D = \text{m}$

$L = 3.538 \text{ m}$

$W_{eng} = 897 \text{ kg} = 1978 \text{ lb}$ $= \text{in}$

$= 139.3 \text{ in}$

Static Sea Level:

$T_{ssl} = 50000 \text{ N}$ $T_{ssl}^{AB} = 75000 \text{ N}$

$= 11240 \text{ lbf}$ $= 16861 \text{ lbf}$

$SFC_{ssl} = 2.22 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.78 \text{ (lb/h)/lbf}$ $= 1.77 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 65 \text{ kg/s} = 143.3 \text{ lb/s}$

BPR = 0.3 OPR = 24.5

FPR = 3.9 TET = 1850 °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

M88-3

Manufacturer: SNECMA

Application: Rafale A/B/C/D/M

Composition: 3 / - / 6 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = 60051 \text{ N}$ $T_{ssl}^{AB} = 94969 \text{ N}$

$= 13500 \text{ lbf}$ $= 21350 \text{ lbf}$

$SFC_{ssl} = 2.22 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.79 \text{ (lb/h)/lbf}$ $= 1.76 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 71.7 \text{ kg/s} = 158.1 \text{ lb/s}$

BPR = OPR = 26

FPR = TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Marbore 2

Manufacturer: Turboméca

Application: Saulnier Paris 1

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 3923 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 882 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Marbore 2A

Manufacturer: Turboméca

Application: Noratlas N-2502, CM-170-1, CM-173, Sagittario, Noratlas N-2504/-2506/-2508

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 3923 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 882 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Marbore 2C

Manufacturer: Turboméca

Application: Sagittario

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 3923 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 882 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Marbore 2F

Manufacturer: Turboméca

Application: Sagittario

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 3923 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 882 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Marbore 6

Manufacturer: Turboméca

Application: HA-200E

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4706 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 1058 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Marbore 6C

Manufacturer: Turboméca

Application: Saulnier Paris 2, Saulnier Paris 3, CM-170-2/-3, CM-175

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4715 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 1060 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.14 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.11 (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = 9.5 \text{ kg/s} = 20.9 \text{ lb/s}$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Marbore 6F

Manufacturer: Turboméca

Application: CM.191 (not produced)

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4706 N$ $T_{ssl}^{AB} = N$

$= 1058 lbf$ $= lbf$

$SFC_{ssl} = 3.14 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.11 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 9.5 kg/s = 20.9 lb/s$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Marbore 8

Manufacturer: Turboméca

Application:

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 5872 N$ $T_{ssl}^{AB} = N$

$= 1320 lbf$ $= lbf$

$SFC_{ssl} = 3.26 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.15 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

MC-750

Manufacturer: Maverick

Application: MC-2400 Legend

Composition: - / - / 10 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 3336 N$ $T_{ssl}^{AB} = N$

$= 750 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

MTFE

Manufacturer: Pratt & Whitney

Application:

Composition: / / / /

$D_{fan} = 1.397 \text{ m} = 55 \text{ in}$ $D = \text{m}$

$W_{eng} = 1769 \text{ kg} = 3900 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 89000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 20008 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 370 \text{ kg/s} = 815.7 \text{ lb/s}$

$BPR = 5.2$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts =

$L = 2.515 \text{ m}$

$= 99 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Nene Mk.102

Manufacturer: Rolls-Royce

Application: Attacker FB.2, Sea Hawk F.1/F.2/FB.3/FGA.4, Ouragan A, Mystère

I prototype

Composition: - / - / 1C / 1 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = 753 \text{ kg} = 1660 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 22241 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 5000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.09 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 1.09 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 41 \text{ kg/s} = 90.4 \text{ lb/s}$

$BPR =$ $OPR = 4$

$FPR =$ $TET = 1098 ^\circ\text{K}$

Nb of shafts = 1

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Nene Mk.103

Manufacturer: Hispano-Suiza

Application: Br.960-2 Vultur prototype, Sea Hawk FB.5/FGA.6

Composition: - / - / 1C / 1 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 23131 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 5200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Nene Mk.104

Manufacturer: Rolls-Royce

Application: Sea Hawk FGA.6/FGA.50/Mk.100/Mk.101

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 23131 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 5200 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Nene RB.41-1

Manufacturer: Rolls-Royce

Application: F26 (not produced), Meteor F, Vampire F.2, XP-80, SO 6000

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 20462 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 4600 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = 2.97 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 1.05 (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 40.8 kg/s = 89.9 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR = 4

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Nene RB.41-10

Manufacturer: Rolls-Royce

Application: CT-133 Silver Star

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 22686 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 5100 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

$OPR_{cr} =$

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

Nene RB.41-2

Manufacturer: Rolls-Royce

Application: Canberra B.1, I.Ae.33

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 22241 \text{ N}$ $T_{ssl}^{AB} = N$

$= 5000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Nene RB.41-3 Mk.101

Manufacturer: Rolls-Royce

Application: Attacker F.1/FB.1, Sea Hawk prototype, Br.960-1 Vultur prototype

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 22686 \text{ N}$ $T_{ssl}^{AB} = N$

$= 5100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Nene RB.41-6/21

Manufacturer: Rolls-Royce

Application: G.82

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24020 \text{ N}$ $T_{ssl}^{AB} = N$

$= 5400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-144

Manufacturer: Kuznetsov

Application: Tu-144/-144D/-144LL

Composition: 2 / 3B / 11 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 127485 \text{ N}$ $T_{ssl}^{AB} = 171612 \text{ N}$

$= 28660 \text{ lbf}$ $= 38580 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 249.9 \text{ kg/s} = 550.9 \text{ lb/s}$

BPR = 0.6 OPR = 14.2

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-144-22

Manufacturer: Kuznetsov

Application: Tu-22M0 'Backfire-A', Tu-22M1 'Backfire-A'

Composition: 2 / 3B / 11 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 147102 \text{ N}$ $T_{ssl}^{AB} = 177928 \text{ N}$

$= 33070 \text{ lbf}$ $= 40000 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-144A

Manufacturer: Kuznetsov

Application: Tu-144S (not produced)

Composition: 2 / 3B / 11 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 147102 \text{ N}$ $T_{ssl}^{AB} = 177928 \text{ N}$

$= 33070 \text{ lbf}$ $= 40000 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.53 OPR = 17

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-22

Manufacturer: Kuznetsov

Application: Tu-22M0 'Backfire-A', Tu-22M1 'Backfire-A'

Composition: / / / /

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 158867 N$ $T_{ssl}^{AB} = 214915 N$
 $= 35715 lbf$ $= 48315 lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

NK-25

Manufacturer: Kuznetsov

Application: Tu-22M3 'Backfire-C', Tu-22MR (Tu-22M3R) 'Backfire-D', Tu-22ME, Tu-22M2Ye

Composition: / / / /

$D_{fan} = m = in$ $D = m$ $L = m$
 $W_{eng} = kg = lb$ $= in$ $= in$

Static Sea Level:

$T_{ssl} = 186380 N$ $T_{ssl}^{AB} = 245163 N$
 $= 41900 lbf$ $= 55115 lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

NK-321

Manufacturer: Kuznetsov

Application: Tu-144, Tu-160 'Blackjack'

Composition: 3 / 5 / 7 / 1 / 1 / 2

$D_{fan} = m = in$ $D = 1.461 m$ $L = 5.994 m$
 $W_{eng} = 3442 kg = 7588 lb$ $= 57.5 in$ $= 236 in$

Static Sea Level:

$T_{ssl} = 137196 N$ $T_{ssl}^{AB} = 244994 N$
 $= 30843 lbf$ $= 55077 lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 365.1 kg/s = 804.9 lb/s$
 $BPR = 1.4$ $OPR = 28.4$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

NK-8-2

Manufacturer: Kuznetsov

Application: Tu-154 'Careless-A'

Composition: 2 / 2B / 6 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.443 m$

$W_{eng} = 2100 kg = 4630 lb$ $= 56.8 in$

Static Sea Level:

$T_{ssl} = 93163 N$ $T_{ssl}^{AB} = N$

$= 20944 lbf$ $= lbf$

$SFC_{ssl} = 1.64 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.58 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 209.6 kg/s = 462.1 lb/s$

BPR = 1 OPR = 21.5

FPR = 2.15 TET = °K

Nb of shafts = 2

$L = 4.762 m$

$= 187.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-8-2U

Manufacturer: Kuznetsov

Application: Tu-154A/B 'Careless-A'

Composition: 2 / 2B / 6 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.443 m$

$W_{eng} = 2100 kg = 4630 lb$ $= 56.8 in$

Static Sea Level:

$T_{ssl} = 102976 N$ $T_{ssl}^{AB} = N$

$= 23150 lbf$ $= lbf$

$SFC_{ssl} = 1.61 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.57 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 228.2 kg/s = 503.1 lb/s$

BPR = 1.05 OPR = 23.2

FPR = 2.15 TET = °K

Nb of shafts = 2

$L = 4.763 m$

$= 187.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-8-3

Manufacturer: Kuznetsov

Application: Il-62

Composition: 2 / 2B / 6 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 93190 N$ $T_{ssl}^{AB} = N$

$= 20950 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-8-4

Manufacturer: Kuznetsov

Application: Il-62

Composition: 2 / 2B / 6 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.443 m$

$W_{eng} = 2100 kg = 4630 lb$ $= 56.8 in$

Static Sea Level:

$T_{ssl} = 102976 N$ $T_{ssl}^{AB} = N$

$= 23150 lbf$ $= lbf$

$SFC_{ssl} = 1.67 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.59 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 221.8 kg/s = 489 lb/s$

BPR = 1.02 OPR = 23.2

FPR = 2.15 TET = °K

Nb of shafts = 2

$L = 5.105 m$

$= 201 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-84

Manufacturer: Kuznetsov

Application:

Composition: / / / /

$D_{fan} = 1.442 m = 56.8 in$ $D = m$

$W_{eng} = 2200 kg = 4850 lb$ $= in$

Static Sea Level:

$T_{ssl} = 103005 N$ $T_{ssl}^{AB} = N$

$= 23156 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 232 kg/s = 511.5 lb/s$

BPR = 1 OPR = 23.2

FPR = TET = 1145 °K

Year:

Nb of shafts =

$L = 5.1 m$

$= 200.8 in$

Cruise:

$T_{cr} = 26978 N$

$= 6065 lbf$

$SFC_{cr} = 2.2 \cdot 10^{-5} (kg/s)/N$

$= 0.78 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 11000 m$

NK-86

Manufacturer: Kuznetsov

Application: Il-86

Composition: 2 / 2B / 6 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.6 m$

$W_{eng} = 2450 kg = 5401 lb$ $= 63 in$

Static Sea Level:

$T_{ssl} = 127485 N$ $T_{ssl}^{AB} = N$

$= 28660 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 292.1 kg/s = 644 lb/s$

BPR = 1.15 OPR = 13.4

FPR = TET = °K

Nb of shafts = 2

$L = 3.632 m$

$= 143 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

NK-93

Manufacturer: Kuznetsov

Application: Il-96M, Tu-204-230, Tu-330 (proposed)

Composition: 2 DPF / 7 / 8 / 1 / 1 / 3

$D_{fan} = 2.901 \text{ m} = 114.2 \text{ in}$ $D = \text{m}$

$W_{eng} = 3650 \text{ kg} = 8047 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 176518 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 39683 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.67 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.23 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 1000.2 \text{ kg/s} = 2205.1 \text{ lb/s}$

BPR = 16.6 OPR = 28.9

FPR = 1.22 TET = 1520 °K

Nb of shafts = 3

$L = 5.972 \text{ m}$

$= 235.1 \text{ in}$

Cruise:

$T_{cr} = 32000 \text{ N}$

$= 7194 \text{ lbf}$

$SFC_{cr} = 1.39 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.49 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 36.6

$M_{cr} = 0.75$, $h_{cr} = 11000 \text{ m}$

Olympus 593 Mk.601

Manufacturer: Rolls-Royce/SNECMA

Application: Concorde

Composition: - / 7 / 7 / 1 / - / 1

$D_{fan} = \text{m} = \text{in}$ $D = 1.215 \text{ m}$

$W_{eng} = 2637 \text{ kg} = 5814 \text{ lb}$ $= 47.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 145011 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 32600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.98 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.7 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 186 \text{ kg/s} = 410.1 \text{ lb/s}$

BPR = OPR = 15.5

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

Olympus 593 Mk.610

Manufacturer: Rolls-Royce/SNECMA

Application: Concorde

Composition: - / 7 / 7 / 1 / - / 1

$D_{fan} = 1.15 \text{ m} = 45.3 \text{ in}$ $D = 1.215 \text{ m}$

$W_{eng} = 4529 \text{ kg} = 9985 \text{ lb}$ $= 47.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 139460 \text{ N}$ $T_{ssl}^{AB} = 164945 \text{ N}$

$= 31352 \text{ lbf}$ $= 37081 \text{ lbf}$

$SFC_{ssl} = 2.5 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.88 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 194 \text{ kg/s} = 427.7 \text{ lb/s}$

BPR = 0 OPR = 14.5

FPR = TET = 1440 °K

Nb of shafts = 2

$L = 7.2 \text{ m}$

$= 283.5 \text{ in}$

Cruise:

$T_{cr} = 44600 \text{ N}$

$= 10026 \text{ lbf}$

$SFC_{cr} = 3.36 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 1.19 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} = 11.3

$M_{cr} = 2$, $h_{cr} = 16130 \text{ m}$

Olympus 593 Mk.611

Manufacturer: Rolls-Royce/SNECMA

Application: Concorde

Composition: - / 7 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 1.215 m$

$W_{eng} = 2637 kg = 5814 lb$ $= 47.8 in$

Static Sea Level:

$T_{ssl} = 170811 N$ $T_{ssl}^{AB} = N$
 $= 38400 lbf$ $= lbf$

$SFC_{ssl} = 1.98 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.7 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 204.1 kg/s = 450 lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Olympus 593 Mk.621

Manufacturer: Rolls-Royce/SNECMA

Application: Concorde

Composition: - / 7 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = 1.215 m$

$W_{eng} = 2637 kg = 5814 lb$ $= 47.8 in$

Static Sea Level:

$T_{ssl} = 170811 N$ $T_{ssl}^{AB} = N$
 $= 38400 lbf$ $= lbf$

$SFC_{ssl} = 1.98 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.7 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 204.1 kg/s = 450 lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Olympus Mk.101

Manufacturer: Rolls-Royce

Application: Vulcan B.1

Composition: - / 6 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 44482 N$ $T_{ssl}^{AB} = N$
 $= 10000 lbf$ $= lbf$

$SFC_{ssl} = 2.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.77 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 74.8 kg/s = 164.9 lb/s$

BPR = OPR = 11

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Olympus Mk.102

Manufacturer: Rolls-Royce

Application: Vulcan B.1

Composition: - / 6 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 53378 \text{ N}$ $T_{ssl}^{AB} = N$

$= 12000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Olympus Mk.104

Manufacturer: Rolls-Royce

Application: Vulcan B.1/B.1A

Composition: - / 6 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 60051 \text{ N}$ $T_{ssl}^{AB} = N$

$= 13500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Olympus Mk.201

Manufacturer: Rolls-Royce

Application: Vulcan B.2/B.2A

Composition: - / 6 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 75619 \text{ N}$ $T_{ssl}^{AB} = N$

$= 17000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Olympus Mk.301

Manufacturer: Rolls-Royce

Application: Vulcan B.2/SR.2/K.2

Composition: - / 6 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 88964 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 20000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = 2.28 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.8 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 131.5 \text{ kg/s} = 289.9 \text{ lb/s}$
 $BPR =$ $OPR = 13.2$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Olympus Mk.320

Manufacturer: Rolls-Royce

Application: TSR.2 (not produced)

Composition: - / 6 / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 136159 \text{ N}$ $T_{ssl}^{AB} = 146791 \text{ N}$
 $= 30610 \text{ lbf}$ $= 33000 \text{ lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Orenda 10

Manufacturer: Orenda

Application: CL-13A Sabre Mk.5

Composition: - / - / 10 / ?? / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28179 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 6335 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Orenda 11

Manufacturer: Orenda

Application: CF-100 Mk.4B/Mk.5

Composition: - / - / 10 / ?? / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32072 \text{ N}$ $T_{ssl}^{AB} = N$

$= 7210 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orenda 14

Manufacturer: Orenda

Application: CF-100 Mk.5, CL-13B Sabre Mk.6

Composition: - / - / 10 / ?? / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32361 \text{ N}$ $T_{ssl}^{AB} = N$

$= 7275 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orenda 2

Manufacturer: Orenda

Application: CF-100 Mk.2

Composition: - / - / 10 / ?? / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26689 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orenda 3

Manufacturer: Orenda

Application: CF-100 Mk.2

Composition: - / - / 10 / ?? / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26689 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Orenda 8

Manufacturer: Orenda

Application: CF-100 Mk.3

Composition: - / - / 10 / ?? / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26689 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Orenda 9

Manufacturer: Orenda

Application: CF-100 Mk.3/Mk.4/Mk.4A

Composition: - / - / 10 / ?? / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28268 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6355 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Orpheus BOr.100 (pre-prod)

Manufacturer: Bristol Siddeley

Application: Gnat prototype

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 14612 N$ $T_{ssl}^{AB} = N$

$= 3285 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.100-04

Manufacturer: Bristol Siddeley

Application: Gnat T.1

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 18816 N$ $T_{ssl}^{AB} = N$

$= 4230 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.101

Manufacturer: Bristol Siddeley

Application:

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 20106 N$ $T_{ssl}^{AB} = N$

$= 4520 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.12

Manufacturer: Bristol Siddeley

Application: Br.1003 (not produced)

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 36342 N$

$= lbf$ $= 8170 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.3

Manufacturer: Bristol Siddeley

Application: Etendard VI (Mystère XXVI), Br.1001/1002 (not produced)

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 9786 N$ $T_{ssl}^{AB} = N$

$= 2200 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.500

Manufacturer: Bristol Siddeley

Application: C-119 (booster)

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 25577 N$ $T_{ssl}^{AB} = N$

$= 5750 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.701

Manufacturer: Bristol Siddeley

Application: Gnat evaluation aircraft

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 20017 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.701-01

Manufacturer: Bristol Siddeley

Application: Gnat (HAL-built), Ajeet

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 20907 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4700 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.703

Manufacturer: Bristol Siddeley

Application: HF-24 Mk.1

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 21574 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4850 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/\text{lbf}$ $= (lb/h)/\text{lbf}$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/\text{lbf}$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Orpheus BOr.803

Manufacturer: Fiat

Application: G.91R/1, G.91R/1A, G.91R/1B, G.91R/3, G.91R/4

Composition: - / - / 7 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 22241 N$ $T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 5000 lbf$ $= lbf$

$= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR =

$OPR_{cr} =$

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

Orpheus BOr.803-02

Manufacturer: Fiat

Application: G.91T/1, G.91T/3, G.91T/4

Composition: - / - / 7 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 22241 N$ $T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 5000 lbf$ $= lbf$

$= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR =

$OPR_{cr} =$

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

Orpheus BOr.805

Manufacturer: Bristol Siddeley

Application: T-1A

Composition: - / - / 7 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 17793 N$ $T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 4000 lbf$ $= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 38.1 kg/s = 84 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR = 4.4

$OPR_{cr} =$

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

Pegasus 11 Mk.101

Manufacturer: Rolls-Royce

Application: Harrier GR.1/T.2

Composition: 3 / - / 8 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.219 m$

$W_{eng} = 1642 kg = 3620 lb$ $= 48 in$

Static Sea Level:

$T_{ssl} = 84516 N$ $T_{ssl}^{AB} = N$

$= 19000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 14.6

FPR = TET = °K

Nb of shafts = 2

$L = 3.485 m$

$= 137.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pegasus 11 Mk.102

Manufacturer: Rolls-Royce

Application: Harrier GR.1A/T.2A

Composition: 3 / - / 8 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.219 m$

$W_{eng} = 1642 kg = 3620 lb$ $= 48 in$

Static Sea Level:

$T_{ssl} = 91188 N$ $T_{ssl}^{AB} = N$

$= 20500 lbf$ $= lbf$

$SFC_{ssl} = 1.7 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.6 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 190.5 kg/s = 420 lb/s$

BPR = 1.3 OPR = 14.6

FPR = 2 TET = °K

Nb of shafts = 2

$L = 3.485 m$

$= 137.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pegasus 11 Mk.103

Manufacturer: Rolls-Royce

Application: Harrier GR.3/GR.3A/T.4/T.4A

Composition: 3 / - / 8 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.219 m$

$W_{eng} = 1642 kg = 3620 lb$ $= 48 in$

Static Sea Level:

$T_{ssl} = 91188 N$ $T_{ssl}^{AB} = N$

$= 20500 lbf$ $= lbf$

$SFC_{ssl} = 1.7 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.6 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 204.1 kg/s = 450 lb/s$

BPR = 1.5 OPR = 14.6

FPR = 2.15 TET = °K

Nb of shafts = 2

$L = 3.485 m$

$= 137.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pegasus 11 Mk.104

Manufacturer: Rolls-Royce

Application: Harrier FRS.1/FA.2/FRS.51/T.4N/T.8/T.8N/T.60

Composition: 3 / - / 8 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 1.219 m$ $L = 3.485 m$

$W_{eng} = 1642 kg = 3620 lb$ $= 48 in$ $= 137.2 in$

Static Sea Level:

$T_{ssl} = 91188 N$ $T_{ssl}^{AB} = N$

$= 20500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 1.2 OPR = 14.6

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pegasus 11-21 Mk.105

Manufacturer: Rolls-Royce

Year:

Application: AV8B, Harrier GR.5/GR.5A/GR.7/T.6/T.10

Composition: 3 / - / 8 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = 1.22 m = 48 in$ $D = 1.219 m$ $L = 2.51 m$

$W_{eng} = 1475 kg = 3252 lb$ $= 48 in$ $= 98.8 in$

Static Sea Level:

$T_{ssl} = 97000 N$ $T_{ssl}^{AB} = N$

$= 21806 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 201.9 kg/s = 445.1 lb/s$

BPR = 1.34 OPR = 12.9

FPR = TET = 1496 °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= 0 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pegasus 11-21 Mk.106

Manufacturer: Rolls-Royce

Application: Harrier FRS.1/FA.2/FRS.51/T.60

Composition: 3 / - / 8 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = m = in$ $D = 1.219 m$ $L = 3.485 m$

$W_{eng} = 1796 kg = 3960 lb$ $= 48 in$ $= 137.2 in$

Static Sea Level:

$T_{ssl} = 95636 N$ $T_{ssl}^{AB} = N$

$= 21500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 1.2 OPR = 15.3

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pegasus 11-61 Mk.107

Manufacturer: Rolls-Royce

Application: Harrier GR.7/GR.9/T.10/T.12

Composition: 3 / - / 8 / 2 / - / 2

$D_{fan} = 1.222 \text{ m} = 48.1 \text{ in}$ $D = 1.219 \text{ m}$

$W_{eng} = 1932 \text{ kg} = 4259 \text{ lb}$ $= 48 \text{ in}$

Static Sea Level:

$T_{ssl} = 105900 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 23807 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 208 \text{ kg/s} = 458.6 \text{ lb/s}$

BPR = 1.2 OPR = 16.3

FPR = TET = °K

Nb of shafts = 2

$L = 3.485 \text{ m}$

$= 137.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Pegasus 15

Manufacturer: Rolls-Royce

Application:

Composition: 3 / - / 8 / 2 / - / 2

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 106757 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 24000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Pegasus 2

Manufacturer: Bristol Siddeley

Application: P1127

Composition: 2 / - / 8 / 1 / - / 2

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 48930 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Pegasus 3

Manufacturer: Bristol Siddeley

Application: P1127

Composition: 2 / - / 8 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 53378 \text{ N}$ $T_{ssl}^{AB} = N$

$= 12000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pegasus 5-1

Manufacturer: Bristol Siddeley

Application: Kestrel FGA.1

Composition: 2 / - / 8 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 68947 \text{ N}$ $T_{ssl}^{AB} = N$

$= 15500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pegasus 5-2

Manufacturer: Bristol Siddeley

Application: Do 31E

Composition: 2 / - / 8 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 68947 \text{ N}$ $T_{ssl}^{AB} = N$

$= 15500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pirna 014A0

Manufacturer: Pirna

Application: Baade 152

Composition: - / - / 12 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 30915 N$ $T_{ssl}^{AB} = N$
 $= 6950 lbf$ $= lbf$

$SFC_{ssl} = 2.42 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.85 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 49.9 kg/s = 110 lb/s$

BPR = OPR = 7

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pirna 014A1

Manufacturer: Pirna

Application: Baade 152

Composition: - / - / 12 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 32294 N$ $T_{ssl}^{AB} = N$
 $= 7260 lbf$ $= lbf$

$SFC_{ssl} = 2.36 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.83 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 53.1 kg/s = 117.1 lb/s$

BPR = OPR = 7

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Pirna 016

Manufacturer: Pirna

Application: Technology demonstrator

Composition: - / - / 12 / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 34251 N$ $T_{ssl}^{AB} = N$
 $= 7700 lbf$ $= lbf$

$SFC_{ssl} = 2 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.71 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 59.9 kg/s = 132.1 lb/s$

BPR = OPR = 10

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

PS-12

Manufacturer: Perm Aviadvigatel - Soloviev

Application: MS-21-100/-200/-300, MS-21K, MS-12KP (candidate engine)

Composition: / / / /

Nb of shafts =

$D_{fan} = 1.869 \text{ m} = 73.6 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 2449 \text{ kg} = 5399 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = 132387 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = 25199 \text{ N}$

$= 29762 \text{ lbf}$ $= \text{lbf}$

$= 5665 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$SFC_{cr} = 1.56 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$= 0.55 (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 541.1 \text{ kg/s} = 1192.9 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$BPR = 8.39$ $OPR = 40.2$

$OPR_{cr} =$

$FPR =$ $TET = ^\circ\text{K}$

$M_{cr} = 0.8, h_{cr} = 10973 \text{ m}$

PS-12M

Manufacturer: Perm Aviadvigatel - Soloviev

Application:

Composition: / / / /

Nb of shafts =

$D_{fan} = 1.869 \text{ m} = 73.6 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 2449 \text{ kg} = 5399 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = 145634 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = 26965 \text{ N}$

$= 32740 \text{ lbf}$ $= \text{lbf}$

$= 6062 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$SFC_{cr} = 1.57 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$= 0.55 (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$OPR_{cr} =$

$FPR =$ $TET = ^\circ\text{K}$

$M_{cr} = 0.8, h_{cr} = 10973 \text{ m}$

PS-30V-12

Manufacturer: Perm Aviadvigatel - Soloviev

Application: M-55 (M-17RM) 'Mystic-B'

Composition: / / / /

Nb of shafts =

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = 93412 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 21000 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$OPR_{cr} =$

$FPR =$ $TET = ^\circ\text{K}$

$M_{cr} = , h_{cr} = \text{m}$

PS-7**Manufacturer:** Perm Aviadvigatel - Soloviev**Application:****Composition:** / / / / $D_{fan} = 1.209 \text{ m} = 47.6 \text{ in}$ $D = \text{m}$ $W_{eng} = 1350 \text{ kg} = 2976 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 75619 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 17000 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $\text{BPR} =$ $\text{OPR} =$ $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$ **Nb of shafts =** $L = \text{m}$ $= \text{in}$ **Cruise:** $T_{cr} = 15199 \text{ N}$ $= 3417 \text{ lbf}$ $SFC_{cr} = 1.76 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $= 0.62 (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $\text{OPR}_{cr} =$ $M_{cr} = 0.8, h_{cr} = 10973 \text{ m}$ **PS-9****Manufacturer:** Perm Aviadvigatel - Soloviev**Application:** IL-214-100, IL-214T (candidate engine)**Composition:** / / / / $D_{fan} = 1.435 \text{ m} = 56.5 \text{ in}$ $D = \text{m}$ $W_{eng} = 1750 \text{ kg} = 3858 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 22000 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $\text{BPR} =$ $\text{OPR} =$ $\text{FPR} =$ $\text{TET} = ^\circ\text{K}$ **Nb of shafts =** $L = \text{m}$ $= \text{in}$ **Cruise:** $T_{cr} = 20595 \text{ N}$ $= 4630 \text{ lbf}$ $SFC_{cr} = 1.67 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $= 0.59 (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $\text{OPR}_{cr} =$ $M_{cr} = 0.8, h_{cr} = 10973 \text{ m}$ **PS-90****Manufacturer:** Perm Aviadvigatel - Soloviev**Application:** IL96-300, Tu-204**Composition:** 1 / 2 / 13 / 12 / 2 / 4 $D_{fan} = 1.9 \text{ m} = 74.8 \text{ in}$ $D = \text{m}$ $W_{eng} = 2950 \text{ kg} = 6504 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 156800 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 35250 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.07 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= 0.38 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 470 \text{ kg/s} = 1036.2 \text{ lb/s}$ $\text{BPR} = 4.6$ $\text{OPR} = 31.9$ $\text{FPR} = 1.6$ $\text{TET} = 1640 ^\circ\text{K}$ **Year:** 1992**Nb of shafts = 2** $L = 4.964 \text{ m}$ $= 195.4 \text{ in}$ **Cruise:** $T_{cr} = 34300 \text{ N}$ $= 7711 \text{ lbf}$ $SFC_{cr} = 1.69 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $= 0.6 (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $\text{OPR}_{cr} = 36.4$ $M_{cr} = 0.8, h_{cr} = 11000 \text{ m}$

PS-90A

Manufacturer: Perm Aviadvigatel - Soloviev

Year: 1992

Application: Il-96-300, Tu-204-100/-100C/-200/-200C, Tu-214, Tu-330 (Tu-204-330), Tu-134D (proposed), Tu-154M2 (not produced)

Composition: 1 / 2B / 13 / 2 / - / 4

$D_{fan} = 1.9 \text{ m} = 74.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 2950 \text{ kg} = 6504 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 156911 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 35275 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 470 \text{ kg/s} = 1036.2 \text{ lb/s}$

BPR = 4.6 OPR = 35.5

FPR = TET = 1609 °K

Nb of shafts = 2

$L = 4.964 \text{ m}$

$= 195.4 \text{ in}$

Cruise:

$T_{cr} = 34322 \text{ N}$

$= 7716 \text{ lbf}$

$SFC_{cr} = 1.69 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.6 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8$, $h_{cr} = 11000 \text{ m}$

PS-90A10

Manufacturer: Perm Aviadvigatel - Soloviev

Application:

Composition: 1 / - / 12 / 2 / - / 2

$D_{fan} = 1.4 \text{ m} = 55.1 \text{ in}$ $D = \text{m}$

$W_{eng} = 1896 \text{ kg} = 4180 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 90223 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 20283 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 264 \text{ kg/s} = 582 \text{ lb/s}$

BPR = 3.76 OPR = 23.1

FPR = TET = °K

Nb of shafts = 2

$L = 4.28 \text{ m}$

$= 168.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

PS-90A12

Manufacturer: Perm Aviadvigatel - Soloviev

Application: Yak-242

Composition: 1 / - / 13 / 2 / - / 3

$D_{fan} = 1.671 \text{ m} = 65.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 2300 \text{ kg} = 5071 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 117677 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 26455 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 370.1 \text{ kg/s} = 815.9 \text{ lb/s}$

BPR = 5.05 OPR = 25.3

FPR = TET = °K

Nb of shafts = 2

$L = 4.78 \text{ m}$

$= 188.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

PS-90AN-76**Manufacturer:** Perm Aviadvigatel - Soloviev**Application:** Il-76TF, Il-76MF**Composition:** 1 / 2B / 13 / 2 / - / 4 $D_{fan} = 1.9 \text{ m} = 74.8 \text{ in}$ $D = \text{m}$ $W_{eng} = 2950 \text{ kg} = 6504 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 156910 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 35275 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 469.9 \text{ kg/s} = 1036 \text{ lb/s}$ $BPR = 4.6$ $OPR = 35.5$ $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 4.963 \text{ m}$ $= 195.4 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **PW1120****Manufacturer:** Pratt & Whitney**Application:** F4, LAVI**Composition:** 3 / - / 10 / 2 / - / 1 $D_{fan} = 0.775 \text{ m} = 30.5 \text{ in}$ $D = 1.021 \text{ m}$ $W_{eng} = 1323 \text{ kg} = 2917 \text{ lb}$ $= 40.2 \text{ in}$ **Static Sea Level:** $T_{ssl} = 61300 \text{ N}$ $T_{ssl}^{AB} = 91700 \text{ N}$
 $= 13781 \text{ lbf}$ $= 20615 \text{ lbf}$ $SFC_{ssl} = 2.29 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = 5.28 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.81 (\text{lb/h})/\text{lbf}$ $= 1.86 (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 82.1 \text{ kg/s} = 181 \text{ lb/s}$ $BPR = 0.2$ $OPR = 26.8$ $FPR =$ $TET = 1523 ^\circ\text{K}$

Nb of shafts = 2

 $L = 4.115 \text{ m}$ $= 162 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= 0 (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **PW1128****Manufacturer:** Pratt & Whitney**Application:** Lavi**Composition:** 3 / - / 10 / 2 / - / 1 $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 74285 \text{ N}$ $T_{ssl}^{AB} = 121881 \text{ N}$
 $= 16700 \text{ lbf}$ $= 27400 \text{ lbf}$ $SFC_{ssl} = 2.42 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = 5.67 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.85 (\text{lb/h})/\text{lbf}$ $= 2 (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 111.1 \text{ kg/s} = 244.9 \text{ lb/s}$ $BPR =$ $OPR = 27$ $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = \text{m}$ $= \text{in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$

PW2037

Manufacturer: Pratt & Whitney

Year: 1983

Application: B757-200/-200ET, C-17

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = 1.994 \text{ m} = 78.5 \text{ in}$ $D = 2.154 \text{ m}$

$W_{eng} = 3259 \text{ kg} = 7185 \text{ lb}$ $= 84.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 170144 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 38250 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.94 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 548.8 \text{ kg/s} = 1209.9 \text{ lb/s}$

BPR = 5.8 OPR = 27.4

FPR = 1.63 TET = 1678 °K

Nb of shafts = 2

$L = 3.592 \text{ m}$

$= 141.4 \text{ in}$

Cruise:

$T_{cr} = 28913 \text{ N}$

$= 6500 \text{ lbf}$

$SFC_{cr} = 1.65 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = 151.9 \text{ kg/s} = 334.9 \text{ lb/s}$

OPR_{cr} = 30.8

$M_{cr} = 0.85$, $h_{cr} = 10668 \text{ m}$

PW2040

Manufacturer: Pratt & Whitney

Application: B757-200/-200ET/-200F, VC-32A

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = 1.994 \text{ m} = 78.5 \text{ in}$ $D = 2.154 \text{ m}$

$W_{eng} = 3259 \text{ kg} = 7185 \text{ lb}$ $= 84.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 178373 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 40100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 569.3 \text{ kg/s} = 1255.1 \text{ lb/s}$

BPR = 5.9 OPR = 29.9

FPR = 1.66 TET = °K

Nb of shafts = 2

$L = 3.592 \text{ m}$

$= 141.4 \text{ in}$

Cruise:

$T_{cr} = 28913 \text{ N}$

$= 6500 \text{ lbf}$

$SFC_{cr} = 1.65 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85$, $h_{cr} = 10668 \text{ m}$

PW2043

Manufacturer: Pratt & Whitney

Application: B757-300/-200/-200ET/-200F (option)

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = 1.994 \text{ m} = 78.5 \text{ in}$ $D = 2.154 \text{ m}$

$W_{eng} = 3248 \text{ kg} = 7161 \text{ lb}$ $= 84.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 189493 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 42600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 6 OPR = 31.9

FPR = TET = °K

Nb of shafts = 2

$L = 3.592 \text{ m}$

$= 141.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

PW2143

Manufacturer: Pratt & Whitney

Application: A340-521, A340-621 (proposed)

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = 1.994 \text{ m} = 78.5 \text{ in}$ $D = 2.154 \text{ m}$

$W_{eng} = 3248 \text{ kg} = 7161 \text{ lb}$ $= 84.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 189493 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 42600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 6 OPR = 31.2

FPR = TET = °K

Nb of shafts = 2

$L = 3.592 \text{ m}$

$= 141.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

PW2237

Manufacturer: Pratt & Whitney

Application: Tu-204-140/-140C (proposed)

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = 1.994 \text{ m} = 78.5 \text{ in}$ $D = 2.154 \text{ m}$

$W_{eng} = 3259 \text{ kg} = 7185 \text{ lb}$ $= 84.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 162804 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 36600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.95 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 548.8 \text{ kg/s} = 1209.9 \text{ lb/s}$

BPR = 5.8 OPR = 27.9

FPR = 1.63 TET = °K

Nb of shafts = 2

$L = 3.592 \text{ m}$

$= 141.4 \text{ in}$

Cruise:

$T_{cr} = 28913 \text{ N}$

$= 6500 \text{ lbf}$

$SFC_{cr} = 1.65 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

PW2240

Manufacturer: Pratt & Whitney

Application: Tu-204-240/-240C, Tu-330 (Tu-204-330) (proposed)

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = 1.994 \text{ m} = 78.5 \text{ in}$ $D = 2.154 \text{ m}$

$W_{eng} = 3259 \text{ kg} = 7185 \text{ lb}$ $= 84.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 178373 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 40100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 569.3 \text{ kg/s} = 1255.1 \text{ lb/s}$

BPR = 5.9 OPR = 27.6

FPR = 1.66 TET = °K

Nb of shafts = 2

$L = 3.592 \text{ m}$

$= 141.4 \text{ in}$

Cruise:

$T_{cr} = 28913 \text{ N}$

$= 6500 \text{ lbf}$

$SFC_{cr} = 1.65 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

PW2337

Manufacturer: Pratt & Whitney

Application: Il-96M/T

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = 1.994 \text{ m} = 78.5 \text{ in}$ $D = 2.154 \text{ m}$

$W_{eng} = 3259 \text{ kg} = 7185 \text{ lb}$ $= 84.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 162804 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 36600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.95 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 548.8 \text{ kg/s} = 1209.9 \text{ lb/s}$

$BPR = 5.8$ $OPR = 27.4$

$FPR = 1.63$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.592 \text{ m}$

$= 141.4 \text{ in}$

Cruise:

$T_{cr} = 28913 \text{ N}$

$= 6500 \text{ lbf}$

$SFC_{cr} = 1.65 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

PW2643

Manufacturer: Pratt & Whitney

Application:

Composition: 1 / 4B / 12 / 2 / - / 5

$D_{fan} = 1.994 \text{ m} = 78.5 \text{ in}$ $D = 2.154 \text{ m}$

$W_{eng} = 3248 \text{ kg} = 7161 \text{ lb}$ $= 84.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 189493 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 42600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 6$ $OPR = 31.2$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.592 \text{ m}$

$= 141.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW305A

Manufacturer: Pratt & Whitney

Application: Learjet 60

Composition: 1 / - / 4 + 1C / 2 / - / 3

$D_{fan} = 0.779 \text{ m} = 30.7 \text{ in}$ $D = 0.927 \text{ m}$

$W_{eng} = 450 \text{ kg} = 992 \text{ lb}$ $= 36.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 20813 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 4679 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.1 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 4.3$ $OPR = 15.5$

$FPR = 1.5$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.07 \text{ m}$

$= 81.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW305B**Manufacturer:** Pratt & Whitney**Application:** BAe (Hawker) 1000**Composition:** 1 / - / 4 + 1C / 2 / - / 3 $D_{fan} = 0.779 \text{ m} = 30.7 \text{ in}$ $D = 0.927 \text{ m}$ $W_{eng} = 450 \text{ kg} = 992 \text{ lb}$ $= 36.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 23389 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 5258 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.11 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = 81.6 \text{ kg/s} = 179.9 \text{ lb/s}$ $BPR = 4.3$ $OPR = 15.5$ $FPR = 1.8$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 2.083 \text{ m}$ $= 82 \text{ in}$ **Cruise:** $T_{cr} = 4951 \text{ N}$ $= 1113 \text{ lbf}$ $SFC_{cr} = 1.91 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.68 \text{ (lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = 0.8$, $h_{cr} = 12192 \text{ m}$ **PW306****Manufacturer:** Pratt & Whitney**Application:****Composition:** / / / / / $D_{fan} = 0.97 \text{ m} = 38.2 \text{ in}$ $D = \text{m}$ $W_{eng} = 473 \text{ kg} = 1043 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 25400 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 5710 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 4.5$ $OPR =$ $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts =

 $L = 1.92 \text{ m}$ $= 75.6 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} =$, $h_{cr} = \text{m}$ **PW306A****Manufacturer:** Pratt & Whitney**Application:** G200 (Galaxy)**Composition:** 1 / - / 4 + 1C / 2 / - / 3 $D_{fan} = 0.804 \text{ m} = 31.7 \text{ in}$ $D = \text{m}$ $W_{eng} = 473 \text{ kg} = 1043 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 26867 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 6040 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.12 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.39 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 4.5$ $OPR = 18.3$ $FPR = 1.57$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 1.92 \text{ m}$ $= 75.6 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} =$, $h_{cr} = \text{m}$

PW306B**Manufacturer:** Pratt & Whitney**Application:** 328JET, Envoy 3**Composition:** 1 / - / 4 + 1C / 2 / - / 3 $D_{fan} = 0.804 \text{ m} = 31.7 \text{ in}$ $D = \text{m}$ $W_{eng} = 473 \text{ kg} = 1043 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 26912 \text{ N}$ $= 6050 \text{ lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.5

FPR =

 $T_{ssl}^{AB} = \text{N}$ $= \text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 2

 $L = 1.92 \text{ m}$ $= 75.6 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$ **PW306C****Manufacturer:** Pratt & Whitney**Application:** Citation Sovereign**Composition:** 1 / - / 4 + 1C / 2 / - / 3 $D_{fan} = 0.804 \text{ m} = 31.7 \text{ in}$ $D = \text{m}$ $W_{eng} = 473 \text{ kg} = 1043 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 25292 \text{ N}$ $= 5686 \text{ lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.5

FPR =

 $T_{ssl}^{AB} = \text{N}$ $= \text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 2

 $L = 1.92 \text{ m}$ $= 75.6 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$ **PW307A****Manufacturer:** Pratt & Whitney**Application:** Falcon 7X**Composition:** 1 / - / 4 + 1C / 2 / - / 3 $D_{fan} = 0.804 \text{ m} = 31.7 \text{ in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 27134 \text{ N}$ $= 6100 \text{ lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

FPR =

 $T_{ssl}^{AB} = \text{N}$ $= \text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 2

 $L = 1.92 \text{ m}$ $= 75.6 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$

PW308A

Manufacturer: Pratt & Whitney

Application: Hawker Horizon

Composition: 1 / - / 4 + 1C / 2 / - / 3

$D_{fan} = 0.804 \text{ m} = 31.7 \text{ in}$ $D = \text{m}$

$W_{eng} = 597 \text{ kg} = 1316 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 29247 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 6575 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 4.1$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.92 \text{ m}$

$= 75.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW308B

Manufacturer: Pratt & Whitney

Application: 428JET (not produced)

Composition: 1 / - / 4 + 1C / 2 / - / 3

$D_{fan} = 0.804 \text{ m} = 31.7 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 35981 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 8089 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 4.1$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.92 \text{ m}$

$= 75.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW308C

Manufacturer: Pratt & Whitney

Application: Falcon 2000EX

Composition: 1 / - / 4 + 1C / 2 / - / 3

$D_{fan} = 0.804 \text{ m} = 31.7 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 31137 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 7000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 4.1$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.92 \text{ m}$

$= 75.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW4052**Manufacturer:** Pratt & Whitney**Year:** 1986**Application:** B767-200ER/-300ER**Composition:** 1 / 4B / 11 / 2 / - / 4 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$ $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$

Nb of shafts = 2

 $L = 3.358 \text{ m}$ $= 132.2 \text{ in}$ **Static Sea Level:** $T_{ssl} = 232196 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 52200 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = 0.88 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$ $= 0.31 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$

BPR = 4.85 OPR = 26.4

FPR = 1.7 TET = °K

Cruise: $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$ **PW4056****Manufacturer:** Pratt & Whitney**Year:** 1987**Application:** B747-400/-400(M)/-400F, B767-200ER/-300/-300ER**Composition:** 1 / 4B / 11 / 2 / - / 4 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$ $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$

Nb of shafts = 2

 $L = 3.358 \text{ m}$ $= 132.2 \text{ in}$ **Static Sea Level:** $T_{ssl} = 252435 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 56750 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$ $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$

BPR = 4.85 OPR = 28.4

FPR = 1.7 TET = °K

Cruise: $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = 30.2 $M_{cr} = , h_{cr} = \text{m}$ **PW4060****Manufacturer:** Pratt & Whitney**Application:** B767-300/-300ER, An-218-200/-300 (proposed)**Composition:** 1 / 4B / 11 / 2 / - / 4 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$ $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$

Nb of shafts = 2

 $L = 3.358 \text{ m}$ $= 132.2 \text{ in}$ **Static Sea Level:** $T_{ssl} = 266892 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 60000 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$ $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$

BPR = 4.85 OPR = 30

FPR = TET = °K

Cruise: $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$

PW4060A**Manufacturer:** Pratt & Whitney**Application:** B767-200ER**Composition:** 1 / 4B / 11 / 2 / - / 4 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$ $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$ **Static Sea Level:** $T_{ssl} = 266892 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 60000 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$ $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$ $BPR = 4.85$ $OPR = 31.5$ $FPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 3.358 \text{ m}$ $= 132.2 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **PW4062****Manufacturer:** Pratt & Whitney**Application:** B747-400/-400ER/-400F/-400FER, B767-200ER/-200FER/-300F/-300ER/-400ER (option)**Composition:** 1 / 4B / 11 / 2 / - / 4 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$ $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$ **Static Sea Level:** $T_{ssl} = 281571 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 63300 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 4.85$ $OPR = 32.3$ $FPR = 1.8$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 3.358 \text{ m}$ $= 132.2 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **PW4074****Manufacturer:** Pratt & Whitney**Application:** B777-200**Composition:** 1 / 6B / 11 / 2 / - / 7 $D_{fan} = 2.845 \text{ m} = 112 \text{ in}$ $D = 3.01 \text{ m}$ $W_{eng} = 6597 \text{ kg} = 14544 \text{ lb}$ $= 118.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 331391 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 74500 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = 1156.7 \text{ kg/s} = 2550.1 \text{ lb/s}$ $BPR = 6$ $OPR = 30.3$ $FPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 4.869 \text{ m}$ $= 191.7 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$

PW4077**Manufacturer:** Pratt & Whitney**Application:** B777-200**Composition:** 1 / 6B / 11 / 2 / - / 7 $D_{fan} = 2.845 \text{ m} = 112 \text{ in}$ $D = 3.01 \text{ m}$ $W_{eng} = 6597 \text{ kg} = 14544 \text{ lb}$ $= 118.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 342511 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 77000 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 1156.7 \text{ kg/s} = 2550.1 \text{ lb/s}$ $BPR = 6.2$ $OPR = 31.5$ $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 4.869 \text{ m}$ $= 191.7 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **PW4084****Manufacturer:** Pratt & Whitney**Year:** 1994**Application:** B777-200**Composition:** 1 / 6B / 11 / 2 / - / 7 $D_{fan} = 2.845 \text{ m} = 112 \text{ in}$ $D = 3.01 \text{ m}$ $W_{eng} = 6597 \text{ kg} = 14544 \text{ lb}$ $= 118.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 373649 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 84000 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 1156.7 \text{ kg/s} = 2550.1 \text{ lb/s}$ $BPR = 6.41$ $OPR = 36.3$ $FPR = 1.68$ $TET = 1634 ^\circ\text{K}$

Nb of shafts = 2

 $L = 4.869 \text{ m}$ $= 191.7 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **PW4090****Manufacturer:** Pratt & Whitney**Application:** B777-200ER/-300**Composition:** 1 / 6B / 11 / 2 / - / 7 $D_{fan} = 2.845 \text{ m} = 112 \text{ in}$ $D = 3.01 \text{ m}$ $W_{eng} = 7069 \text{ kg} = 15584 \text{ lb}$ $= 118.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 401228 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 90200 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 1230.1 \text{ kg/s} = 2711.9 \text{ lb/s}$ $BPR = 6.3$ $OPR = 38.6$ $FPR = 1.7$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 4.869 \text{ m}$ $= 191.7 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$

PW4098
Manufacturer: Pratt & Whitney

Application: B777-300

Composition: 1 / 7B / 11 / 2 / - / 7

 $D_{fan} = 2.845 \text{ m} = 112 \text{ in}$ $D = 3.035 \text{ m}$
 $W_{eng} = 7484 \text{ kg} = 16499 \text{ lb}$ $= 119.5 \text{ in}$
Static Sea Level:
 $T_{ssl} = 435924 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 98000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 1270.1 \text{ kg/s} = 2800.1 \text{ lb/s}$
 $BPR = 5.8$ $OPR = 42.8$
 $FPR = 1.75$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 4.945 \text{ m}$
 $= 194.7 \text{ in}$
Cruise:
 $T_{cr} = 62275 \text{ N}$
 $= 14000 \text{ lbf}$
 $SFC_{cr} = 1.65 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.58 (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.83, h_{cr} = 10668 \text{ m}$
PW4152
Manufacturer: Pratt & Whitney

Application: A310-324/-324ET/-324F

Composition: 1 / 4B / 11 / 2 / - / 4

 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$
 $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$
Static Sea Level:
 $T_{ssl} = 231310 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 52001 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 0.88 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.31 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$
 $BPR = 4.85$ $OPR = 27.3$
 $FPR = 1.7$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 3.358 \text{ m}$
 $= 132.2 \text{ in}$
Cruise:
 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$
PW4156
Manufacturer: Pratt & Whitney

Application: A310-325ET

Composition: 1 / 4B / 11 / 2 / - / 4

 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$
 $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$
Static Sea Level:
 $T_{ssl} = 252435 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 56750 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 0.91 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.32 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$
 $BPR = 4.85$ $OPR = 30.2$
 $FPR = 1.7$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = 3.358 \text{ m}$
 $= 132.2 \text{ in}$
Cruise:
 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = \text{m}$

PW4156A

Manufacturer: Pratt & Whitney

Application: A310-325ET

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$

$W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$

Static Sea Level:

$T_{ssl} = 249080 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 55995 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$

$BPR = 4.85$ $OPR = 29.8$

$FPR = 1.7$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.358 \text{ m}$

$= 132.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW4158

Manufacturer: Pratt & Whitney

Application: A300B4-622/-622R/-622RF, A300F4-622R

Composition: 1 / 4B / 11 / 2 / - / 4

$D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$

$W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$

Static Sea Level:

$T_{ssl} = 257996 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 58000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.91 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$

$BPR = 4.75$ $OPR = 30.7$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 3.358 \text{ m}$

$= 132.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW4164

Manufacturer: Pratt & Whitney

Application: A330-321, A330-221 (option)

Composition: 1 / 5B / 11 / 2 / - / 5

$D_{fan} = 2.535 \text{ m} = 99.8 \text{ in}$ $D = 2.715 \text{ m}$

$W_{eng} = 5625 \text{ kg} = 12401 \text{ lb}$ $= 106.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 286920 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 64502 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 877.2 \text{ kg/s} = 1933.9 \text{ lb/s}$

$BPR = 5.1$ $OPR = 32$

$FPR = 1.75$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 4.143 \text{ m}$

$= 163.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW4168**Manufacturer:** Pratt & Whitney**Year:** 1993**Application:** A330-222/-322**Composition:** 1 / 5B / 11 / 2 / - / 5 $D_{fan} = 2.535 \text{ m} = 99.8 \text{ in}$ $D = 2.715 \text{ m}$ $W_{eng} = 5625 \text{ kg} = 12401 \text{ lb}$ $= 106.9 \text{ in}$ **Static Sea Level:** $T_{ssl} = 305148 \text{ N}$
 $= 68600 \text{ lbf}$ $T_{ssl}^{AB} = \text{N}$
 $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 877.2 \text{ kg/s} = 1933.9 \text{ lb/s}$ $BPR = 5.1$ $OPR = 33.4$ $FPR = 1.75$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 4.143 \text{ m}$ $= 163.1 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$
 $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **PW4168A****Manufacturer:** Pratt & Whitney**Application:** A330-223/-323X**Composition:** 1 / 5B / 11 / 2 / - / 5 $D_{fan} = 2.535 \text{ m} = 99.8 \text{ in}$ $D = 2.715 \text{ m}$ $W_{eng} = 5625 \text{ kg} = 12401 \text{ lb}$ $= 106.9 \text{ in}$ **Static Sea Level:** $T_{ssl} = 305148 \text{ N}$
 $= 68600 \text{ lbf}$ $T_{ssl}^{AB} = \text{N}$
 $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 877.2 \text{ kg/s} = 1933.9 \text{ lb/s}$ $BPR = 5.1$ $OPR = 32$ $FPR = 1.75$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 4.143 \text{ m}$ $= 163.1 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$
 $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **PW4358****Manufacturer:** Pratt & Whitney**Year:** 1987**Application:** A300-600R**Composition:** / / / / / $D_{fan} = 2.375 \text{ m} = 93.5 \text{ in}$ $D = \text{m}$ $W_{eng} = 4173 \text{ kg} = 9200 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 258000 \text{ N}$
 $= 58001 \text{ lbf}$ $T_{ssl}^{AB} = \text{N}$
 $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$
 $= 0 (\text{lb/h})/\text{lbf}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 767 \text{ kg/s} = 1690.9 \text{ lb/s}$ $BPR = 5.2$ $OPR = 29.6$ $FPR = 1.7$ $TET = 1538 ^\circ\text{K}$ **Nb of shafts** = $L = 3.37 \text{ m}$ $= 132.7 \text{ in}$ **Cruise:** $T_{cr} = 59500 \text{ N}$
 $= 13376 \text{ lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$
 $= 0 (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} = 32.3$ $M_{cr} = 0.85, h_{cr} = 10670 \text{ m}$

PW4460

Manufacturer: Pratt & Whitney

Application: MD-11/-11F/-11F(AF)

Composition: 1 / 4B / 11 / 2 / - / 4

 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$
 $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$

Static Sea Level:

 $T_{ssl} = 266892 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 60000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 0.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.33 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 773.4 \text{ kg/s} = 1705.1 \text{ lb/s}$

BPR = 4.85 OPR = 31.5

FPR = TET = °K

Nb of shafts = 2

 $L = 3.358 \text{ m}$
 $= 132.2 \text{ in}$

Cruise:

 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = \text{m}$
PW4462

Manufacturer: Pratt & Whitney

Application: MD-11/-11F/-11F(CF)

Composition: 1 / 4B / 11 / 2 / - / 4

 $D_{fan} = 2.377 \text{ m} = 93.6 \text{ in}$ $D = 2.464 \text{ m}$
 $W_{eng} = 4179 \text{ kg} = 9213 \text{ lb}$ $= 97 \text{ in}$

Static Sea Level:

 $T_{ssl} = 281571 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 63300 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.85 OPR = 32.3

FPR = 1.8 TET = °K

Nb of shafts = 2

 $L = 3.358 \text{ m}$
 $= 132.2 \text{ in}$

Cruise:

 $T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = , h_{cr} = \text{m}$
PW530

Manufacturer: Pratt & Whitney

Application: Cessna Citation Bravo

Composition: / / / / /

 $D_{fan} = 0.58 \text{ m} = 22.8 \text{ in}$ $D = \text{m}$
 $W_{eng} = 275 \text{ kg} = 606 \text{ lb}$ $= \text{in}$

Static Sea Level:

 $T_{ssl} = 13000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2923 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.24 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.44 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4 OPR =

FPR = TET = °K

Year: 1995

Nb of shafts =

 $L = 1.622 \text{ m}$
 $= 63.9 \text{ in}$

Cruise:

 $T_{cr} = 2700 \text{ N}$
 $= 607 \text{ lbf}$
 $SFC_{cr} = 2.16 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.76 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

 OPR_{cr} =

 $M_{cr} = 0.8, h_{cr} = 12200 \text{ m}$

PW530A

Manufacturer: Pratt & Whitney

Application: Citation Bravo

Composition: 1 / - / 2 + 1C / 1 / - / 2

$D_{fan} = 0.579 \text{ m} = 22.8 \text{ in}$ $D = 0.701 \text{ m}$

$W_{eng} = 279 \text{ kg} = 615 \text{ lb}$ $= 27.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 12224 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2748 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 3.7$ $OPR = 13.3$

$FPR = 1.62$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.524 \text{ m}$

$= 60 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW535A

Manufacturer: Pratt & Whitney

Year: 1999

Application: Citation Encore

Composition: 1 / 1B / 2 + 1C / 1 / - / 3

$D_{fan} = \text{m} = \text{in}$ $D = 0.701 \text{ m}$

$W_{eng} = \text{kg} = \text{lb}$ $= 27.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 14950 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3361 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 2.55$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.524 \text{ m}$

$= 60 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW535B

Manufacturer: Pratt & Whitney

Year: 2006

Application: Citation Encore+

Composition: 1 / 1B / 2 + 1C / 1 / - / 3

$D_{fan} = \text{m} = \text{in}$ $D = 0.701 \text{ m}$

$W_{eng} = \text{kg} = \text{lb}$ $= 27.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 15120 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 3399 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 2.55$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.524 \text{ m}$

$= 60 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

PW545A

Manufacturer: Pratt & Whitney

Year: 1997

Application: Citation Excel

Composition: 1 / 1B / 2 + 1C / 1 / - / 3

$D_{fan} = 0.691 \text{ m} = 27.2 \text{ in}$ $D = 0.813 \text{ m}$

$W_{eng} = 370 \text{ kg} = 816 \text{ lb}$ $= 32 \text{ in}$

Static Sea Level:

$T_{ssl} = 16832 \text{ N}$

$= 3784 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.12

FPR = 1.59

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 15.7

TET = 993 °K

Nb of shafts = 2

$L = 1.727 \text{ m}$

$= 68 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

PW545B

Manufacturer: Pratt & Whitney

Year: 2003

Application: Citation XLS

Composition: 1 / 1B / 2 + 1C / 1 / - / 3

$D_{fan} = \text{m} = \text{in}$ $D = 1.047 \text{ m}$

$W_{eng} = 377 \text{ kg} = 830 \text{ lb}$ $= 41.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 17750 \text{ N}$

$= 3990 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 3.8

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 42

TET = 1013 °K

Nb of shafts = 2

$L = 1.914 \text{ m}$

$= 75.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

PW545C

Manufacturer: Pratt & Whitney

Year: 2003

Application: Citation XLS+

Composition: 1 / 1B / 2 + 1C / 1 / - / 3

$D_{fan} = \text{m} = \text{in}$ $D = 1.047 \text{ m}$

$W_{eng} = 377 \text{ kg} = 830 \text{ lb}$ $= 41.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 18320 \text{ N}$

$= 4118 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 3.8

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 42

TET = 1013 °K

Nb of shafts = 2

$L = 1.914 \text{ m}$

$= 75.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

PW610F

Manufacturer: Pratt & Whitney

Application: Eclipse 500

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4946 N$ $T_{ssl}^{AB} = N$

$= 1112 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

PW6122

Manufacturer: Pratt & Whitney

Application: A318-121, Il-214 (candidate engine), A316/A317 (A31X) (not produced)

Composition: 1 / 4B / 5 / 1 / - / 3

$D_{fan} = 1.435 m = 56.5 in$ $D = 1.524 m$

$W_{eng} = 1867 kg = 4116 lb$ $= 60 in$

Static Sea Level:

$T_{ssl} = 97860 N$ $T_{ssl}^{AB} = N$

$= 22000 lbf$ $= lbf$

$SFC_{ssl} = 1.02 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.36 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 4.9 OPR = 27.2

FPR = TET = °K

Nb of shafts = 2

$L = 2.337 m$

$= 92 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

PW6124

Manufacturer: Pratt & Whitney

Year: 2005

Application: A318-122

Composition: 1 / 4B / 5 / 1 / - / 3

$D_{fan} = 1.435 m = 56.5 in$ $D = 1.524 m$

$W_{eng} = kg = lb$ $= 60 in$

Static Sea Level:

$T_{ssl} = 105700 N$ $T_{ssl}^{AB} = N$

$= 23762 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 4.9 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 2.7 m$

$= 106.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

PW615F

Manufacturer: Pratt & Whitney

Application: Citation Mustang, Eclipse 500, ProJet (candidate engine)

Composition: / / / / /

$D_{fan} = m = in$ $D = m$ Nb of shafts =
 $W_{eng} = kg = lb$ $= in$ $L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 6005 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 1350 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

PW6162

Manufacturer: Pratt & Whitney

Application: A318-122

Composition: 1 / 4B / 5 / 1 / - / 3

$D_{fan} = 1.435 \text{ m} = 56.5 \text{ in}$ $D = 1.524 \text{ m}$ Nb of shafts = 2
 $W_{eng} = 1867 \text{ kg} = 4116 \text{ lb}$ $= 60 \text{ in}$ $L = 2.337 \text{ m}$
 $= 92 \text{ in}$

Static Sea Level:

$T_{ssl} = 106757 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 24000 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.05 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.37 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR = 4.9$ $OPR = 29.6$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

PW625F

Manufacturer: Pratt & Whitney

Application: Technology demonstrator

Composition: / / / / /

$D_{fan} = m = in$ $D = m$ Nb of shafts =
 $W_{eng} = kg = lb$ $= in$ $L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 11121 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 2500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

PW800 (AFTI)

Manufacturer: Pratt & Whitney

Application: Technology demonstrator

Composition: 1G / - / 4 + 1C / 2 / - / 3

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 55603 \text{ N}$

$= 12500 \text{ lbf}$

$T_{ssl}^{AB} = N$

$= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 7.8

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

PW8160

Manufacturer: Pratt & Whitney

Application: A340-521, A340-621 (proposed)

Composition: 1G / 3B / 5 / 1 / - / 3

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 289133 \text{ N}$

$= 65000 \text{ lbf}$

$T_{ssl}^{AB} = N$

$= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-11AF-300

Manufacturer: Tumansky

Application: Yak-28B 'Brewer-A'

Composition: - / 3 / 3 / 1 / - / 1

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = N$

$= \text{lbf}$

$T_{ssl}^{AB} = 56715 \text{ N}$

$= 12750 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-11AF2-300

Manufacturer: Tumansky

Application: Yak-28R 'Brewer-D'

Composition: - / 3 / 3 / 1 / - / 1

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = N$

$T_{ssl}^{AB} = 58494 N$

Cruise:

$T_{cr} = N$

$= lbf$

$= 13150 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

R-11B-300

Manufacturer: Tumansky

Application: Yak-25RV 'Mandrake'

Composition: - / 3 / 3 / 1 / - / 1

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 38255 N$

$T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 8600 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

R-11F-300

Manufacturer: Tumansky

Application: MiG-21F/G 'Fishbed-C', Yak-28P 'Firebar'

Composition: - / 3 / 3 / 1 / - / 1

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 38255 N$

$T_{ssl}^{AB} = 49820 N$

$T_{cr} = N$

$= 8600 lbf$

$= 11200 lbf$

$= lbf$

$SFC_{ssl} = 2.67 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = 6.25 \cdot 10^{-5} (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.94 (lb/h)/lbf$

$= 2.21 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 64.9 kg/s = 143.1 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR = 8.7

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

R-11F2S-300**Manufacturer:** Tumansky**Application:** MiG-21FL 'Fishbed-C', Su-15 'Flagon-A', Su-15UT 'Flagon-C', Su-15 'Flagon-D'**Composition:** - / 3 / 3 / 1 / - / 1

Nb of shafts = 2

 $D_{fan} = m = in$ $D = m$ $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:****Cruise:** $T_{ssl} = 38477 N$ $T_{ssl}^{AB} = 52934 N$ $T_{cr} = N$ $= 8650 lbf$ $= 11900 lbf$ $= lbf$ $SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.47 \cdot 10^{-5} (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= 0.96 (lb/h)/lbf$ $= 2.28 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = 65.8 kg/s = 145.1 lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR = 8.8

OPR_{cr} =

FPR = TET = °K

 $M_{cr} = , h_{cr} = m$ **R-13-300****Manufacturer:** Tumansky**Application:** Su-15T 'Flagon-E', Su-15TM 'Flagon-F', Su-25 'Frogfoot-A'**Composition:** - / 2 / 5 / 1 / - / 1

Nb of shafts = 2

 $D_{fan} = m = in$ $D = m$ $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:****Cruise:** $T_{ssl} = 40212 N$ $T_{ssl}^{AB} = 64944 N$ $T_{cr} = N$ $= 9040 lbf$ $= 14600 lbf$ $= lbf$ $SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.11 \cdot 10^{-5} (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= 0.96 (lb/h)/lbf$ $= 2.16 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = 66.2 kg/s = 145.9 lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR = 8.9

OPR_{cr} =

FPR = TET = °K

 $M_{cr} = , h_{cr} = m$ **R-13F-300****Manufacturer:** Tumansky**Application:** MiG-21MF 'Fishbed-J'**Composition:** - / 2 / 5 / 1 / - / 1

Nb of shafts = 2

 $D_{fan} = m = in$ $D = m$ $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:****Cruise:** $T_{ssl} = N$ $T_{ssl}^{AB} = 68947 N$ $T_{cr} = N$ $= lbf$ $= 15500 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR = OPR =

OPR_{cr} =

FPR = TET = °K

 $M_{cr} = , h_{cr} = m$

R-13F2-300**Manufacturer:** Tumansky**Application:** Su-15 'Flagon-F'**Composition:** - / 2 / 5 / 1 / - / 1 $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = N$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $FPR =$ $T_{ssl}^{AB} = 68947 N$ $= 15500 lbf$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $OPR =$ $TET = ^\circ K$ **Nb of shafts = 2** $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **R-15-300****Manufacturer:** Tumansky**Application:** MiG-21bis 'Fishbed-N'**Composition:** - / - / 5 / ?? / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 73551 N$ $= 16535 lbf$ $SFC_{ssl} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $FPR =$ $T_{ssl}^{AB} = N$ $= lbf$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $OPR =$ $TET = ^\circ K$ **Nb of shafts = 1** $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **R-15B-300****Manufacturer:** Tumansky**Application:** E-155P**Composition:** / / / / / $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 73551 N$ $= 16535 lbf$ $SFC_{ssl} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $FPR =$ $T_{ssl}^{AB} = 100085 N$ $= 22500 lbf$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= (lb/h)/lbf$ $OPR =$ $TET = ^\circ K$ **Nb of shafts =** $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

R-15BD-300

Manufacturer: Tumansky

Application: MiG-25 'Foxbat', E-155R

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 73551 \text{ N}$ $T_{ssl}^{AB} = 109871 \text{ N}$
 $= 16535 \text{ lbf}$ $= 24700 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-19-300

Manufacturer: Tumansky

Application: Yak-30 'Magnum'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 10298 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2315 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-195

Manufacturer: Tumansky

Application: Su-39 (Su-25TM) 'Super Frogfoot'

Composition: - / 3 / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.914 \text{ m}$
 $W_{eng} = 990 \text{ kg} = 2183 \text{ lb}$ $= 36 \text{ in}$

Static Sea Level:

$T_{ssl} = 44131 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 9921 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 2

$L = 3.302 \text{ m}$

$= 130 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-25-300

Manufacturer: Tumansky

Application: MiG-21bis 'Fishbed-N', Su-15bis (not produced)

Composition: - / 3 / 5 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 40256 N$ $T_{ssl}^{AB} = 69614 N$

$= 9050 lbf$ $= 15650 lbf$

$SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.25 \cdot 10^{-5} (kg/s)/N$

$= 0.96 (lb/h)/lbf$ $= 2.21 (lb/h)/lbf$

$\dot{w}_{ssl} = 68 kg/s = 149.9 lb/s$

BPR = OPR = 9.6

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-27F2M-300

Manufacturer: Tumansky

Application: MiG-23MF 'Flogger-B', MiG-23MS 'Flogger-E', MiG-23UB 'Flogger-C'

Composition: - / 5 / 6 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = m = in$ $D = 1.059 m$

$L = 4.851 m$

$W_{eng} = 1497 kg = 3300 lb$ $= 41.7 in$

$= 191 in$

Static Sea Level:

$T_{ssl} = 63698 N$ $T_{ssl}^{AB} = 98061 N$

$= 14320 lbf$ $= 22045 lbf$

$SFC_{ssl} = 2.78 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.92 \cdot 10^{-5} (kg/s)/N$

$= 0.98 (lb/h)/lbf$ $= 2.09 (lb/h)/lbf$

$\dot{w}_{ssl} = 104.3 kg/s = 229.9 lb/s$

BPR = OPR = 10.9

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-27M-300

Manufacturer: Tumansky

Application: MiG-23S 'Flogger-A'

Composition: - / 5 / 6 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = m = in$ $D = 1.059 m$

$L = m$

$W_{eng} = kg = lb$ $= 41.7 in$

$= in$

Static Sea Level:

$T_{ssl} = 63698 N$ $T_{ssl}^{AB} = 98061 N$

$= 14320 lbf$ $= 22045 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-27V-300

Manufacturer: Tumansky

Application: Yak-36 'Freehand', Yak-38 'Forger-A'

Composition: - / 5 / 6 / 1 / - / 1

$D_{fan} = m = in$ $D = 1.012 m$

$W_{eng} = 1350 kg = 2976 lb$ $= 39.8 in$

Static Sea Level:

$T_{ssl} = 65700 N$ $T_{ssl}^{AB} = N$

$= 14770 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = 3.706 m$

$= 145.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-28-300

Manufacturer: Tumansky

Application: Yak-38 'Forger-A'

Composition: - / 5 / 6 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 68057 N$ $T_{ssl}^{AB} = N$

$= 15300 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-29-300

Manufacturer: Khachaturov/Tumansky

Application: MiG-23MF 'Flogger-B', MiG-23MS 'Flogger-E', MiG-23UB 'Flogger-C', MiG-27 'Flogger-D'

Composition: - / 5 / 6 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.912 m$

$W_{eng} = 1880 kg = 4145 lb$ $= 35.9 in$

Static Sea Level:

$T_{ssl} = 78444 N$ $T_{ssl}^{AB} = 120769 N$

$= 17635 lbf$ $= 27150 lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.67 \cdot 10^{-5} (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= 2 (lb/h)/lbf$

$\dot{w}_{ssl} = 109.8 kg/s = 242.1 lb/s$

BPR = OPR = 13.1

FPR = TET = °K

Nb of shafts = 2

$L = 4.953 m$

$= 195 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-29B-300

Manufacturer: Khachaturov/Tumansky

Application: MiG-27M 'Flogger-J', Su-22 'Fitter-F'

Composition: - / 5 / 6 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = 1760 \text{ kg} = 3880 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 78444 \text{ N}$ $T_{ssl}^{AB} = 112762 \text{ N}$

$= 17635 \text{ lbf}$ $= 25350 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 106.6 \text{ kg/s} = 235 \text{ lb/s}$

BPR = OPR = 12.4

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-29BS-300

Manufacturer: Khachaturov/Tumansky

Application: Su-22 'Fitter-F', Su-22UM3 'Fitter-G', Su-22M 'Fitter-J'

Composition: - / 5 / 6 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 78444 \text{ N}$ $T_{ssl}^{AB} = N$

$= 17635 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-29PN-300

Manufacturer: Khachaturov/Tumansky

Application: MiG-23MF 'Flogger-B'

Composition: - / 5 / 6 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 78444 \text{ N}$ $T_{ssl}^{AB} = 122583 \text{ N}$

$= 17635 \text{ lbf}$ $= 27558 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-31

Manufacturer: Tumansky

Application: MiG-25 'Foxbat-A'

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 107873 N$

$= lbf$ $= 24251 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-31-300

Manufacturer: Tumansky

Application: MiG-25 'Foxbat-A'

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 120101 N$

$= lbf$ $= 27000 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-31F-300

Manufacturer: Tumansky

Application: MiG-31 'Foxhound-A'

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 136493 N$

$= lbf$ $= 30685 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

R-32-300

Manufacturer: Tumansky

Application: Su-27UB

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = N$

$T_{ssl}^{AB} = 133246 N$

$= lbf$

$= 29955 lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

R-35-300

Manufacturer: Khachaturov/Tumansky

Application: MiG-23MF 'Flogger-E', MiG-23ML 'Flogger-G', MiG-23MLD 'Flogger-K'

Composition: - / 5 / 6 / 1 / - / 1

$D_{fan} = m = in$

$D = 0.912 m$

$W_{eng} = 1765 kg = 3891 lb$

$= 35.9 in$

Static Sea Level:

$T_{ssl} = 83849 N$

$T_{ssl}^{AB} = 127485 N$

$= 18850 lbf$

$= 28660 lbf$

$SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = 5.56 \cdot 10^{-5} (kg/s)/N$

$= 0.96 (lb/h)/lbf$

$= 1.96 (lb/h)/lbf$

$\dot{w}_{ssl} = 110.2 kg/s = 242.9 lb/s$

BPR =

OPR = 13.1

FPR =

TET = °K

Nb of shafts = 2

$L = 4.95 m$

$= 194.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

R-37F-300

Manufacturer: Tumansky

Application: MiG-21F 'Fishbed-C'

Composition: / / / / /

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 56492 N$

$T_{ssl}^{AB} = N$

$= 12700 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

R-79-300

Manufacturer: Kobchyenko/Tumansky

Application: Yak-141 'Freestyle'

Composition: 5 / - / 6 / 1 / / 1

$D_{fan} = 1.1 \text{ m} = 43.3 \text{ in}$ $D = 1.716 \text{ m}$

$W_{eng} = 2750 \text{ kg} = 6063 \text{ lb}$ $= 67.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 107646 \text{ N}$ $T_{ssl}^{AB} = 151995 \text{ N}$

$= 24200 \text{ lbf}$ $= 34170 \text{ lbf}$

$SFC_{ssl} = 1.87 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.66 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 120.2 \text{ kg/s} = 265 \text{ lb/s}$

$BPR = 1$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 5.229 \text{ m}$

$= 205.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

R-79M-300

Manufacturer: Kobchyenko/Tumansky

Application: Yak-141 'Freestyle'

Composition: / / / / /

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 176149 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 39600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts =

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

R-79V-300

Manufacturer: Kobchyenko/Tumansky

Application: Yak-141 'Freestyle'

Composition: / / / / /

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 152128 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 34200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts =

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

R-95

Manufacturer: Tumansky

Application: Su-25 'Frogfoot-A', Su-25UB 'Frogfoot-B'

Composition: - / 3 / 5 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 39233 \text{ N}$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 8820 \text{ lbf}$

$= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

R-9F

Manufacturer: Tumansky

Application: MiG-19F 'Farmer'

Composition: - / 3 / 3 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = N$

$T_{ssl}^{AB} = 56715 \text{ N}$

$T_{cr} = N$

$= \text{lbf}$

$= 12750 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

R123-300

Manufacturer: Soyuz

Application:

Composition: 1 / - / 2 + 1C / 1 / - / 1

Nb of shafts = 2

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 13789 \text{ N}$

$T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 3100 \text{ lbf}$

$= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = 6

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

R126-300

Manufacturer: Soyuz

Application: Tu-324

Composition: 1 / - / 5 + 1C / 2 / - / 3

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 39224 N$ $T_{ssl}^{AB} = N$
 $= 8818 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

R127-300

Manufacturer: Soyuz

Application:

Composition: 1 / - / 2C / 2 / - / 2

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8830 N$ $T_{ssl}^{AB} = N$
 $= 1985 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 30.8 kg/s = 67.9 lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RB.108

Manufacturer: Rolls-Royce

Application: SC.1 (lift/cruise engines)

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 10409 N$ $T_{ssl}^{AB} = N$
 $= 2340 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RB.145

Manufacturer: Rolls-Royce/MAN Turbo

Application: VJ 101C X-1/-X-2

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = 0.528 \text{ m}$

$W_{eng} = 207 \text{ kg} = 456 \text{ lb}$ $= 20.8 \text{ in}$

Static Sea Level:

$T_{ssl} = 12233 \text{ N}$ $T_{ssl}^{AB} = 16236 \text{ N}$

$= 2750 \text{ lbf}$ $= 3650 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 1.514 \text{ m}$

$= 59.6 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.153-61

Manufacturer: Rolls-Royce/MAN Turbo

Application: VJ 101D (not produced)

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.749 \text{ m}$

$W_{eng} = 649 \text{ kg} = 1431 \text{ lb}$ $= 29.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 30470 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6850 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 54.9 \text{ kg/s} = 121 \text{ lb/s}$

BPR = 0.7 OPR = 18

FPR = TET = °K

Nb of shafts = 2

$L = 2.261 \text{ m}$

$= 89 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.153-61R

Manufacturer: Rolls-Royce/MAN Turbo

Application: VJ 101D (not produced)

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.749 \text{ m}$

$W_{eng} = kg = lb$ $= 29.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 30470 \text{ N}$ $T_{ssl}^{AB} = 51799 \text{ N}$

$= 6850 \text{ lbf}$ $= 11645 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 54.9 \text{ kg/s} = 121 \text{ lb/s}$

BPR = 0.7 OPR = 18

FPR = TET = °K

Nb of shafts = 2

$L = 4.204 \text{ m}$

$= 165.5 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.162-1

Manufacturer: Rolls-Royce

Application:

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = 0.66 \text{ m}$
 $W_{eng} = 125 \text{ kg} = 276 \text{ lb}$ $= 26 \text{ in}$

Static Sea Level:

$T_{ssl} = 19612 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 4409 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 4.3$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 1.316 \text{ m}$
 $= 51.8 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RB.162-30

Manufacturer: Rolls-Royce

Application: VJ 101C

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24465 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 5500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RB.162-31

Manufacturer: Rolls-Royce

Application: Mirage IIIV, VJ 101D (not produced)

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24465 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 5500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RB.162-32

Manufacturer: Rolls-Royce

Application: Mirage IIIV

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24465 \text{ N}$ $T_{ssl}^{AB} = N$

$= 5500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.162-4

Manufacturer: Rolls-Royce

Application:

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = 0.66 \text{ m}$

$W_{eng} = 125 \text{ kg} = 276 \text{ lb}$ $= 26 \text{ in}$

Static Sea Level:

$T_{ssl} = 20907 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4700 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.3

FPR = TET = °K

Nb of shafts = 1

$L = 1.316 \text{ m}$

$= 51.8 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.162-4D

Manufacturer: Rolls-Royce

Application: Do 31E

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = 0.66 \text{ m}$

$W_{eng} = 125 \text{ kg} = 276 \text{ lb}$ $= 26 \text{ in}$

Static Sea Level:

$T_{ssl} = 19572 \text{ N}$ $T_{ssl}^{AB} = N$

$= 4400 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 1.316 \text{ m}$

$= 51.8 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.162-81

Manufacturer: Rolls-Royce

Application: VAK 191B (not produced)

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26734 N$ $T_{ssl}^{AB} = N$

$= 6010 lbf$ $= lbf$

$SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.96 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 38.6 kg/s = 85.1 lb/s$

BPR = OPR = 4.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.162-86

Manufacturer: Rolls-Royce

Application: Trident 3B (booster)

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = 236 kg = 520 lb$ $= in$

Static Sea Level:

$T_{ssl} = 23353 N$ $T_{ssl}^{AB} = N$

$= 5250 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 39 kg/s = 86 lb/s$

BPR = OPR = 4.3

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.178

Manufacturer: Rolls-Royce

Application:

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 126774 N$ $T_{ssl}^{AB} = N$

$= 28500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.193-12

Manufacturer: Rolls-Royce/MAN Turbo

Application: VAK 191B (lift/cruise, not produced)

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 45207 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 10163 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

RB.199-34R-04 Mk.101

Manufacturer: Turbo-Union

Application: Tornado GR.1 (IDS)

Composition: 3 / 3 / 6 / 1 / 1 / 2

$D_{fan} = m = in$

$D = m$

Nb of shafts = 3

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 39144 N$

$T_{ssl}^{AB} = 71171 N$

$T_{cr} = N$

$= 8800 lbf$

$= 16000 lbf$

$= lbf$

$SFC_{ssl} = 1.75 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = 6.23 \cdot 10^{-5} (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.62 (lb/h)/lbf$

$= 2.2 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 69.9 kg/s = 154.1 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = 1.1

OPR = 23.4

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

RB.199-34R-04 Mk.103

Manufacturer: Turbo-Union

Application: Tornado GR.1/GR.1A/GR.1B/GR.4 (IDS)

Composition: 3 / 3 / 6 / 1 / 1 / 2

$D_{fan} = 0.734 m = 28.9 in$

$D = m$

Nb of shafts = 3

$L = 3.232 m$

$W_{eng} = 1061 kg = 2339 lb$

$= in$

$= 127.2 in$

Static Sea Level:

$T_{ssl} = 40700 N$

$T_{ssl}^{AB} = 71500 N$

$T_{cr} = 35000 N$

$= 9150 lbf$

$= 16074 lbf$

$= 7868 lbf$

$SFC_{ssl} = 1.81 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = 6.94 \cdot 10^{-5} (kg/s)/N$

$SFC_{cr} = 2.78 \cdot 10^{-5} (kg/s)/N$

$= 0.64 (lb/h)/lbf$

$= 2.45 (lb/h)/lbf$

$= 0.98 (lb/h)/lbf$

$\dot{w}_{ssl} = 73.1 kg/s = 161.2 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = 1.06

OPR = 23.5

OPR_{cr} =

FPR = 2.65

TET = 1598 °K

$M_{cr} = 0.9, h_{cr} = 0 m$

RB.199-34R-04 Mk.104

Manufacturer: Turbo-Union

Application: Tornado F.3 (ADV)

Composition: 3 / 3 / 6 / 1 / 1 / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = 976 \text{ kg} = 2152 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 40479 \text{ N}$ $T_{ssl}^{AB} = 72950 \text{ N}$

$= 9100 \text{ lbf}$ $= 16400 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 3

$L = 3.607 \text{ m}$

$= 142 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.199-34R-04 Mk.104D

Manufacturer: Turbo-Union

Application: BAe EAP

Composition: 3 / 3 / 6 / 1 / 1 / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 40034 \text{ N}$ $T_{ssl}^{AB} = 75619 \text{ N}$

$= 9000 \text{ lbf}$ $= 17000 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 3

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.199-34R-04 Mk.105

Manufacturer: Turbo-Union

Application: Tornado ECR

Composition: 3 / 3 / 6 / 1 / 1 / 2

$D_{fan} = m = in$ $D = 0.752 \text{ m}$

$W_{eng} = 980 \text{ kg} = 2161 \text{ lb}$ $= 29.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 42952 \text{ N}$ $T_{ssl}^{AB} = 74730 \text{ N}$

$= 9656 \text{ lbf}$ $= 16800 \text{ lbf}$

$SFC_{ssl} = 1.8 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.64 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 74.8 \text{ kg/s} = 164.9 \text{ lb/s}$

BPR = 0.97 OPR = 23.4

FPR = TET = °K

Nb of shafts = 3

$L = 3.302 \text{ m}$

$= 130 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RB.202

Manufacturer: Rolls-Royce

Application: Do 231C (lift engines, not produced), Do 231M (lift engines, not produced)

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 58271 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 13100 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

RB.207

Manufacturer: Rolls-Royce

Application: A300, L1011-1-1 (candidate engine)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = m = in$

$D = m$

Nb of shafts = 3

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 211290 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 47500 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = 1.53 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.54 (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 753 kg/s = 1660.1 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = 5

OPR = 27

OPR_{cr} =

FPR = 2

TET = °K

$M_{cr} = , h_{cr} = m$

RB.211-22-02

Manufacturer: Rolls-Royce

Application: L1011-1

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = m = in$

$D = m$

Nb of shafts = 3

$L = 3.269 m$

$W_{eng} = 3261 kg = 7189 lb$

$= in$

$= 128.7 in$

Static Sea Level:

$T_{ssl} = 180597 N$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 40600 lbf$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 601 kg/s = 1325 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = 4.8

OPR = 27

OPR_{cr} =

FPR = 1.42

TET = °K

$M_{cr} = , h_{cr} = m$

RB.211-22B

Manufacturer: Rolls-Royce

Application: L1011 Tristar 1-150

Composition: / / / /

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 4171 \text{ kg} = 9195 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 186800 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 41994 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 626 \text{ kg/s} = 1380.1 \text{ lb/s}$

BPR = 5 OPR = 24.5

FPR = TET = °K

Nb of shafts =

$L = 3.033 \text{ m}$

$= 119.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-22B-02

Manufacturer: Rolls-Royce

Application: L1011-1/-1F/-50/-100/-150, L1011-400 (not produced)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 4171 \text{ kg} = 9195 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 186824 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 42000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.06 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.37 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 626 \text{ kg/s} = 1380.1 \text{ lb/s}$

BPR = 4.8 OPR = 24.5

FPR = 1.42 TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 42236 \text{ N}$

$= 9495 \text{ lbf}$

$SFC_{cr} = 1.78 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.63 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-22C-02

Manufacturer: Rolls-Royce

Application: L1011-1/-50/-100/-150 (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 4171 \text{ kg} = 9195 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 186824 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 42000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.8 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = 3.033 \text{ m}$

$= 119.4 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-23

Manufacturer: Rolls-Royce

Application: L1011-1/-50/-100/-150 (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = m = in$

$D = m$

Nb of shafts = 3

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 170722 \text{ N}$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 38380 \text{ lbf}$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

RB.211-24

Manufacturer: Rolls-Royce

Application: (see RB.211-524), L1011-2 (not produced)

Composition: 1 / 7 / 6 / 1 / 1 / 4

Nb of shafts = 3

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 50000 \text{ lbf}$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

RB.211-40

Manufacturer: Rolls-Royce

Application: BAC 311 (not produced)

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = m = in$

$D = m$

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 191451 \text{ N}$

$T_{ssl}^{AB} = N$

Cruise:

$T_{cr} = N$

$= 43040 \text{ lbf}$

$= lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

RB.211-524

Manufacturer: Rolls-Royce

Application: L1011-100/-200, B747-SP (option), L-1011-300 (not produced)

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$L = 3.033 \text{ m}$

$W_{eng} = 4452 \text{ kg} = 9815 \text{ lb}$ $= \text{in}$

$= 119.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 213514 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 48000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.5

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524B

Manufacturer: Rolls-Royce

Application: L1011-200/250/500, Tristar KC.1, K.1, C.2, C.2A

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = 2.18 \text{ m}$

$L = 3.106 \text{ m}$

$W_{eng} = 4452 \text{ kg} = 9815 \text{ lb}$ $= 85.8 \text{ in}$

$= 122.3 \text{ in}$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 50000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 686.3 \text{ kg/s} = 1513 \text{ lb/s}$

BPR = 4.5

OPR = 28.4

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524B-02

Manufacturer: Rolls-Royce

Application: B747-SP, L1011-200/-200F/-500/-500F, B747-100 (option), L-1011-600 (not produced)

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 4452 \text{ kg} = 9815 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 50000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 686.3 \text{ kg/s} = 1513 \text{ lb/s}$

BPR = 4.5

OPR = 28.4

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524B2-02

Manufacturer: Rolls-Royce

Application: L1011-200/-200F/-500, B747-SP/-100 (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 4452 \text{ kg} = 9815 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 50000 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 686.3 \text{ kg/s} = 1513 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 4.5 OPR = 28.4

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524B4-02

Manufacturer: Rolls-Royce

Application: L1011-200/-200F/-250/-500

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.179 \text{ m} = 85.8 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 4452 \text{ kg} = 9815 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = 48930 \text{ N}$

$= 50000 \text{ lbf}$ $= \text{lbf}$

$= 11000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$SFC_{cr} = 1.72 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.61 (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 680.4 \text{ kg/s} = 1500 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 4.4 OPR = 29

OPR_{cr} =

FPR = TET = °K

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-524B4D-02

Manufacturer: Rolls-Royce

Application: L1011-200/-500

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.179 \text{ m} = 85.8 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 4452 \text{ kg} = 9815 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 50000 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 685.8 \text{ kg/s} = 1511.9 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = 4.4 OPR = 28.6

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524BD-02

Manufacturer: Rolls-Royce

Application: L1011-200/-200F/-500, B747-100 (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 4452 \text{ kg} = 9815 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 50000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 686.3 \text{ kg/s} = 1513 \text{ lb/s}$

BPR = 4.5 OPR = 28.4

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524C

Manufacturer: Rolls-Royce

Application: B747-SP/-100B/-200B/-300

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 4472 \text{ kg} = 9859 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 229082 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 51500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 694.9 \text{ kg/s} = 1532 \text{ lb/s}$

BPR = 4.5 OPR = 28.6

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 51110 \text{ N}$

$= 11490 \text{ lbf}$

$SFC_{cr} = 1.82 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.64 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-524C2

Manufacturer: Rolls-Royce

Application: B747-SP/-100B/-200B/-300

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.154 \text{ m} = 84.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 4472 \text{ kg} = 9859 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 229082 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 51500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 694.9 \text{ kg/s} = 1532 \text{ lb/s}$

BPR = 4.5 OPR = 28.6

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 51110 \text{ N}$

$= 11490 \text{ lbf}$

$SFC_{cr} = 1.82 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.64 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-524D4

Manufacturer: Rolls-Royce

Application: B747-SP/-200B/-200B(M)/-200B(SF)/-200F/-300, L1011-500H

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.179 \text{ m} = 85.8 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 4479 \text{ kg} = 9875 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = 235755 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 53000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 702.2 \text{ kg/s} = 1548.1 \text{ lb/s}$

BPR = 4.4 OPR = 29.3

FPR = TET = °K

Cruise:

$T_{cr} = 49953 \text{ N}$

$= 11230 \text{ lbf}$

$SFC_{cr} = 1.75 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.62 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-524D4B

Manufacturer: Rolls-Royce

Application: B747-200/-200F/-300 (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.179 \text{ m} = 85.8 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 4479 \text{ kg} = 9875 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = 235755 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 53000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 702.2 \text{ kg/s} = 1548.1 \text{ lb/s}$

BPR = 4.4 OPR = 29.6

FPR = TET = °K

Cruise:

$T_{cr} = 49953 \text{ N}$

$= 11230 \text{ lbf}$

$SFC_{cr} = 1.7 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.6 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-524G

Manufacturer: Rolls-Royce

Application: B747-400/-400F, B767-300ER (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

Nb of shafts = 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = 4387 \text{ kg} = 9672 \text{ lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = 257996 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 58000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 727.6 \text{ kg/s} = 1604.1 \text{ lb/s}$

BPR = 4.3 OPR = 32.9

FPR = TET = °K

Cruise:

$T_{cr} = 52547 \text{ N}$

$= 11813 \text{ lbf}$

$SFC_{cr} = 1.62 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.57 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-524G-T

Manufacturer: Rolls-Royce

Application: B747-400/-400F, 767-300ER (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4295 \text{ kg} = 9469 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 257996 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 58000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 727.6 \text{ kg/s} = 1604.1 \text{ lb/s}$

BPR = 4.3 OPR = 32.9

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 52547 \text{ N}$

$= 11813 \text{ lbf}$

$SFC_{cr} = 1.62 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.57 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-524G/H-T

Manufacturer: Rolls-Royce

Application: B747-400

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4387 \text{ kg} = 9672 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 257996 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 58000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.3 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 52547 \text{ N}$

$= 11813 \text{ lbf}$

$SFC_{cr} = 1.62 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.57 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85, h_{cr} = 10668 \text{ m}$

RB.211-524G3

Manufacturer: Rolls-Royce

Application: B767-300ER/-300FER (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4387 \text{ kg} = 9672 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 257996 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 58000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.1 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524G4-T

Manufacturer: Rolls-Royce

Application: B767-300ER/-300FER (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4387 \text{ kg} = 9672 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 250878 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 56400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 4.1$

$OPR =$

$FPR =$

$TET = ^\circ\text{K}$

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524H

Manufacturer: Rolls-Royce

Year: 1989

Application: B747-400, B767-300ER/-300F/-300FER/-400F

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4386 \text{ kg} = 9669 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 269562 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 60600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.59 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.56 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 727.6 \text{ kg/s} = 1604.1 \text{ lb/s}$

$BPR = 4.3$

$OPR = 34.5$

$FPR =$

$TET = 1548 ^\circ\text{K}$

Nb of shafts = 3

$L = 3.175 \text{ m}$

$= 125 \text{ in}$

Cruise:

$T_{cr} = 52547 \text{ N}$

$= 11813 \text{ lbf}$

$SFC_{cr} = 1.62 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.57 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85 , h_{cr} = 10668 \text{ m}$

RB.211-524H-T

Manufacturer: Rolls-Royce

Application: B747-400/-400F, B767-300ER, An-124-210 (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4295 \text{ kg} = 9469 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 269561 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 60600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 727.6 \text{ kg/s} = 1604.1 \text{ lb/s}$

$BPR = 4.1$

$OPR = 34.5$

$FPR =$

$TET = ^\circ\text{K}$

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = 52547 \text{ N}$

$= 11813 \text{ lbf}$

$SFC_{cr} = 1.62 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.57 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.85 , h_{cr} = 10668 \text{ m}$

RB.211-524H2

Manufacturer: Rolls-Royce

Application: B747-400/-400F

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4387 \text{ kg} = 9672 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 269561 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 60600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.1 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524H2-T

Manufacturer: Rolls-Royce

Application: B747-400ER (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4295 \text{ kg} = 9469 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 264668 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 59500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.1 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-524H3

Manufacturer: Rolls-Royce

Application: B767-300ER/-300FER (option)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = 2.192 \text{ m} = 86.3 \text{ in}$ $D = \text{m}$

$W_{eng} = 4387 \text{ kg} = 9672 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 269561 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 60600 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.1 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-535C

Manufacturer: Rolls-Royce

Application: B757-200

Composition: / / / /

$D_{fan} = 1.877 \text{ m} = 73.9 \text{ in}$ $D = \text{m}$

$W_{eng} = 3309 \text{ kg} = 7295 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 166400 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 37408 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 518 \text{ kg/s} = 1142 \text{ lb/s}$

$BPR = 4.4$ $OPR = 21.1$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts =

$L = 3.01 \text{ m}$

$= 118.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

RB.211-535C-37

Manufacturer: Rolls-Royce

Application: B757-200/-200(SF)/-200F

Composition: 1 / 6 / 6 / 1 / 1 / 3

$D_{fan} = 1.859 \text{ m} = 73.2 \text{ in}$ $D = \text{m}$

$W_{eng} = 3308 \text{ kg} = 7293 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 166363 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 37400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 518 \text{ kg/s} = 1142 \text{ lb/s}$

$BPR = 4.4$ $OPR = 21.1$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 3.01 \text{ m}$

$= 118.5 \text{ in}$

Cruise:

$T_{cr} = 37601 \text{ N}$

$= 8453 \text{ lbf}$

$SFC_{cr} = 1.83 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.65 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

RB.211-535E4

Manufacturer: Rolls-Royce

Application: B757-200, Tu-204

Composition: / / / /

$D_{fan} = 1.882 \text{ m} = 74.1 \text{ in}$ $D = \text{m}$

$W_{eng} = 3295 \text{ kg} = 7264 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 191718 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 43100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.72 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.61 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 522 \text{ kg/s} = 1150.8 \text{ lb/s}$

$BPR = 4.3$ $OPR = 25.8$

$FPR = 1.7$ $TET = 1500 ^\circ\text{K}$

Year: 1984

Nb of shafts =

$L = 2.995 \text{ m}$

$= 117.9 \text{ in}$

Cruise:

$T_{cr} = 37788 \text{ N}$

$= 8495 \text{ lbf}$

$SFC_{cr} = 1.69 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.6 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

RB.211-535E4-37

Manufacturer: Rolls-Royce

Application: B757-200/-200ER/-200ET/-200F, Tu-204-120/-120C/-220/-220C/-222, Tu-224

Composition: 1 / 6 / 6 / 1 / 1 / 3

$D_{fan} = 1.882 \text{ m} = 74.1 \text{ in}$ $D = \text{m}$

$W_{eng} = 3295 \text{ kg} = 7264 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 178373 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 40100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.92 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.32 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 522.1 \text{ kg/s} = 1151 \text{ lb/s}$

BPR = 4.3 OPR = 25.8

FPR = TET = °K

Nb of shafts = 3

$L = 2.995 \text{ m}$

$= 117.9 \text{ in}$

Cruise:

$T_{cr} = 38699 \text{ N}$

$= 8700 \text{ lbf}$

$SFC_{cr} = 1.69 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

RB.211-535E4B-37

Manufacturer: Rolls-Royce

Application: B757-200/-200ET/-300/-200ER/-200F (option), Tu-214, Tu-330 (Tu-204-330) (proposed)

Composition: 1 / 6 / 6 / 1 / 1 / 3

$D_{fan} = 1.882 \text{ m} = 74.1 \text{ in}$ $D = \text{m}$

$W_{eng} = 3295 \text{ kg} = 7264 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 191717 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 43100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 522.1 \text{ kg/s} = 1151 \text{ lb/s}$

BPR = 4.3 OPR = 25.8

FPR = TET = °K

Nb of shafts = 3

$L = 2.995 \text{ m}$

$= 117.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-535F5-37

Manufacturer: Rolls-Royce

Application: Tu-204-220/-222

Composition: 1 / 6 / 6 / 1 / 1 / 3

$D_{fan} = 1.883 \text{ m} = 74.1 \text{ in}$ $D = \text{m}$

$W_{eng} = 3295 \text{ kg} = 7264 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 191717 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 43100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.3 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = 2.995 \text{ m}$

$= 117.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

RB.211-56

Manufacturer: Rolls-Royce

Application: L1011-3, L1011-8.4 (not produced)

Composition: 1 / 7 / 6 / 1 / 1 / 4

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 232196 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 52200 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 621.4 \text{ kg/s} = 1370 \text{ lb/s}$
 $BPR = 5.04$ $OPR = 26$
 $FPR = 1.59$ $TET = ^\circ K$

Nb of shafts = 3

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RB.211-61

Manufacturer: Rolls-Royce

Application: BAC 311 (not produced)

Composition: 1 / 7 / 6 / 1 / 1 / 3

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 222410 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 50000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 3

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RB.220

Manufacturer: Rolls-Royce

Application: Do 231C/M (not produced)

Composition: / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 106757 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 24000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RB.432

Manufacturer: Rolls-Royce

Application: F29 (not produced)

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 71171 N$ $T_{ssl}^{AB} = N$

$= 16000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-10

Manufacturer: Tumansky

Application: Yak-15, La-150

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8825 N$ $T_{ssl}^{AB} = N$

$= 1984 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-10A

Manufacturer: Tumansky

Application: Yak-17 'Feather'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 9786 N$ $T_{ssl}^{AB} = N$

$= 2200 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-10F

Manufacturer: Tumansky

Application: Yak-19

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 10765 \text{ N}$ $T_{ssl}^{AB} = N$

$= 2420 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

RD-11

Manufacturer: Tumansky

Application: Yak-28P 'Firebar'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 60807 \text{ N}$

$= lbf$ $= 13670 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

RD-1700

Manufacturer: Soyuz

Application: MiG-AT (candidate engine)

Composition: 2 / - / 4 / ?? / - / ??

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16672 \text{ N}$ $T_{ssl}^{AB} = N$

$= 3748 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 0.78$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

RD-20

Manufacturer: Tumansky

Application: MiG-9F 'Fargo'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7829 N$ $T_{ssl}^{AB} = N$

$= 1760 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-20F

Manufacturer: Tumansky

Application: MiG-9FF 'Fargo'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7829 N$ $T_{ssl}^{AB} = N$

$= 1760 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-3

Manufacturer: Mikulin

Application: Tu-104

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 66194 N$ $T_{ssl}^{AB} = N$

$= 14881 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-33

Manufacturer: Klimov

Year:

Application: Mig-29 'Fulcrum-A', Il-102

Composition: 4 / - / 9 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = 0.746 \text{ m} = 29.4 \text{ in}$ $D = 1 \text{ m}$

$L = 4.229 \text{ m}$

$W_{eng} = 1217 \text{ kg} = 2683 \text{ lb}$ $= 39.4 \text{ in}$

$= 166.5 \text{ in}$

Static Sea Level:

Cruise:

$T_{ssl} = 49500 \text{ N}$ $T_{ssl}^{AB} = 81400 \text{ N}$

$T_{cr} = \text{N}$

$= 11128 \text{ lbf}$ $= 18299 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5.94 \cdot 10^{-5} \text{ (kg/s)/N}$

$SFC_{cr} = \text{(kg/s)/N}$

$= 0.77 \text{ (lb/h)/lbf}$ $= 2.1 \text{ (lb/h)/lbf}$

$= 0 \text{ (lb/h)/lbf}$

$\dot{w}_{ssl} = 77 \text{ kg/s} = 169.8 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$BPR = 0.55$ $OPR = 21.7$

$OPR_{cr} =$

$FPR =$ $TET = 1680 \text{ }^\circ\text{K}$

$M_{cr} = , h_{cr} = \text{m}$

RD-33K

Manufacturer: Klimov

Application: MiG-29K 'Fulcrum-D', MiG-33 (MiG-29M) 'Fulcrum-E'

Composition: 4 / - / 9 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = \text{N}$ $T_{ssl}^{AB} = 86006 \text{ N}$

$T_{cr} = \text{N}$

$= \text{lbf}$ $= 19335 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$OPR_{cr} =$

$FPR =$ $TET = \text{ }^\circ\text{K}$

$M_{cr} = , h_{cr} = \text{m}$

RD-35

Manufacturer: Klimov

Application: Yak-130

Composition: 3 / - / 7 / 1 / - / 1

Nb of shafts = 2

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

Cruise:

$T_{ssl} = 21574 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$T_{cr} = \text{N}$

$= 4850 \text{ lbf}$ $= \text{lbf}$

$= \text{lbf}$

$SFC_{ssl} = 1.73 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$SFC_{cr} = \text{(kg/s)/N}$

$= 0.61 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$BPR = 1.41$ $OPR = 14.7$

$OPR_{cr} =$

$FPR =$ $TET = \text{ }^\circ\text{K}$

$M_{cr} = , h_{cr} = \text{m}$

RD-36-35FVR

Manufacturer: Kolesov RKBM

Application: Yak-38 'Forger-A' (lift engines)

Composition: / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = 201 \text{ kg} = 443 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 29914 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 6725 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 45.4 \text{ kg/s} = 100.1 \text{ lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-36-35PR

Manufacturer: Kolesov RKBM

Application: VVA-14

Composition: / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = 201 \text{ kg} = 443 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 29914 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 6725 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 45.4 \text{ kg/s} = 100.1 \text{ lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-36-51V

Manufacturer: Kolesov RKBM

Application: M-17 'Mystic-A'

Composition: / - / 14 / 3 / - / -

$D_{fan} = m = in$ $D = 1.415 \text{ m}$

$W_{eng} = 4125 \text{ kg} = 9094 \text{ lb}$ $= 55.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 68636 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 15430 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 5.227 \text{ m}$

$= 205.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-38

Manufacturer: Kolesov RKBM

Application: Yak-38 'Forger-A' (lift engines)

Composition: / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = 231 \text{ kg} = 509 \text{ lb}$ $= in$

Static Sea Level:

$T_{ssl} = 31871 \text{ N}$ $T_{ssl}^{AB} = N$

$= 7165 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-3M

Manufacturer: Mikulin

Application: Tu-104A/D/V

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 85316 \text{ N}$ $T_{ssl}^{AB} = N$

$= 19180 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-3M-500

Manufacturer: Mikulin

Application: Tu-16, Tu-104B

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 93163 \text{ N}$ $T_{ssl}^{AB} = N$

$= 20944 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 2.83 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 163.3 \text{ kg/s} = 360 \text{ lb/s}$

BPR = OPR = 6.4

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-41

Manufacturer: Kolesov RKBM

Application: Yak-141 'Freestyle' (lift engines)

Composition: / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = 0.635 m$
 $W_{eng} = 290 kg = 639 lb$ $= 25 in$

Static Sea Level:

$T_{ssl} = 40212 N$ $T_{ssl}^{AB} = N$
 $= 9040 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 53.5 kg/s = 117.9 lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 1.594 m$
 $= 62.8 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RD-45FA

Manufacturer: Klimov

Application: Il-28 'Beagle'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26872 N$ $T_{ssl}^{AB} = N$
 $= 6041 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RD-500

Manufacturer: Tumansky

Application: La-15 'Fantail', Yak-23 'Flora', Yak-25 'Flashlight-A', Yak-30 'Magnum'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 15702 N$ $T_{ssl}^{AB} = N$
 $= 3530 lbf$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

RD-60K**Manufacturer:** Klimov**Application:** A-40 'Mermaid' (booster)**Composition:** / / / / / $D_{fan} = m = in$ $D = m$

Nb of shafts =

 $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:** $T_{ssl} = 24510 N$ $T_{ssl}^{AB} = N$ **Cruise:** $T_{cr} = N$ $= 5510 lbf$ $= lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$ **RD-7M2****Manufacturer:** Kolesov**Application:** Tu-22/-22B 'Blinder-A', Tu-22K/KD/KP/KDP 'Blinder-B', Tu-22P/PD 'Blinder-C', Tu-22U/UD 'Blinder-D', Tu-22R/RD/RK/RDK/RM/RDM 'Blinder-E'**Composition:** / / / / / $D_{fan} = m = in$ $D = m$

Nb of shafts =

 $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:** $T_{ssl} = N$ $T_{ssl}^{AB} = 161808 N$ **Cruise:** $T_{cr} = N$ $= lbf$ $= 36376 lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$ **RD-9****Manufacturer:** Tumansky**Application:** Yak-25 'Flashlight-A'**Composition:** - / - / 9 / 2 / - / - $D_{fan} = m = in$ $D = m$

Nb of shafts = 1

 $L = m$ $W_{eng} = kg = lb$ $= in$ $= in$ **Static Sea Level:** $T_{ssl} = 27490 N$ $T_{ssl}^{AB} = N$ **Cruise:** $T_{cr} = N$ $= 6180 lbf$ $= lbf$ $= lbf$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

 $M_{cr} = , h_{cr} = m$

RD-9AF

Manufacturer: Tumansky

Application: Yak-27R/V 'Flashlight-D'

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 32361 N$

$= lbf$ $= 7275 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-9B

Manufacturer: Tumansky

Application: MiG-19 'Farmer'

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 24999 N$ $T_{ssl}^{AB} = 32361 N$

$= 5620 lbf$ $= 7275 lbf$

$SFC_{ssl} = 2.67 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 4.53 \cdot 10^{-5} (kg/s)/N$

$= 0.94 (lb/h)/lbf$ $= 1.6 (lb/h)/lbf$

$\dot{w}_{ssl} = 43.1 kg/s = 95 lb/s$

BPR = OPR = 7.1

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-9BF

Manufacturer: Tumansky

Application: MiG-19SF 'Farmer-B'

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 32361 N$

$= lbf$ $= 7275 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-9E

Manufacturer: Tumansky

Application: Ye-50

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 29358 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6600 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RD-9F

Manufacturer: Tumansky

Application: Yak-120M/MF

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 27579 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6200 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM1

Manufacturer: De Havilland

Application: A 21RA, J 28A

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 13345 \text{ N}$ $T_{ssl}^{AB} = N$

$= 3000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM10

Manufacturer: Rolls-Royce

Application: TP 85

Composition: - / - / 16 / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 50709 N$ $T_{ssl}^{AB} = N$

$= 11400 lbf$ $= lbf$

$SFC_{ssl} = 2.42 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.85 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM11

Manufacturer: Pratt & Whitney

Application: TP 86

Composition: - / - / 9 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 14679 N$ $T_{ssl}^{AB} = N$

$= 3300 lbf$ $= lbf$

$SFC_{ssl} = 2.82 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.99 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 23.1 kg/s = 50.9 lb/s$

BPR =

OPR = 6.7

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM12

Manufacturer: Volvo

Application: JAS 39

Composition: 3 / - / 7 / 1 / - / 1

$D_{fan} = m = in$ $D = m$

$W_{eng} = 1050 kg = 2315 lb$ $= in$

Static Sea Level:

$T_{ssl} = 54001 N$ $T_{ssl}^{AB} = 80512 N$

$= 12140 lbf$ $= 18100 lbf$

$SFC_{ssl} = 2.33 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.04 \cdot 10^{-5} (kg/s)/N$

$= 0.82 (lb/h)/lbf$ $= 1.78 (lb/h)/lbf$

$\dot{w}_{ssl} = 68 kg/s = 149.9 lb/s$

BPR = 0.31

OPR = 27.5

FPR =

TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM14

Manufacturer: Rolls-Royce

Application: TP 102A, S 102B

Composition: 1 / 3B / 12 / 2 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 61608 \text{ N}$ $T_{ssl}^{AB} = N$

$= 13850 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 1.22 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.43 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 176 \text{ kg/s} = 388 \text{ lb/s}$

BPR = 3.04 OPR = 15.8

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM15

Manufacturer: Williams/Rolls-Royce

Application: SK 60A/B/C

Composition: 1 / 1B / 1C / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 6672 \text{ N}$ $T_{ssl}^{AB} = N$

$= 1500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 1.3 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.46 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 26.3 \text{ kg/s} = 58 \text{ lb/s}$

BPR = 3.4 OPR = 10.3

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM1A

Manufacturer: De Havilland

Application: A 21RB, J 28B/C

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 14679 \text{ N}$ $T_{ssl}^{AB} = N$

$= 3300 \text{ lbf}$ $= lbf$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM2A

Manufacturer: De Havilland

Application: J 29A/B/E/F, S 29C/E

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 22241 \text{ N}$ $T_{ssl}^{AB} = 27445 \text{ N}$

$= 5000 \text{ lbf}$ $= 6170 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM2B

Manufacturer: De Havilland

Application: J 29A/B/E/F, S 29C/E

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 22241 \text{ N}$ $T_{ssl}^{AB} = 27445 \text{ N}$

$= 5000 \text{ lbf}$ $= 6170 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM3A

Manufacturer: Rolls-Royce

Application: TP 52

Composition: - / - / 12 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 28913 \text{ N}$ $T_{ssl}^{AB} = N$

$= 6500 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM6B

Manufacturer: Rolls-Royce

Application: A/J 32B, S 32C, J 35A/B/C, S 35C

Composition: / / / /

$D_{fan} = m = in$

$D = m$

Nb of shafts =

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 47151 N$

$T_{ssl}^{AB} = 67666 N$

Cruise:

$T_{cr} = N$

$= 10600 lbf$

$= 15212 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR =

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

RM6C

Manufacturer: Rolls-Royce

Application: J 35D/F/H/J-1/J-2/O/S/X, S 35E/XD, F-35 (J 35XD), RF-35 (S 35XD), TF-35 (SK 35XD)

Composition: - / - / 16 / 2 / - / -

$D_{fan} = m = in$

$D = m$

Nb of shafts = 1

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 53823 N$

$T_{ssl}^{AB} = 69903 N$

Cruise:

$T_{cr} = N$

$= 12100 lbf$

$= 15715 lbf$

$= lbf$

$SFC_{ssl} = 2.64 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = 5.25 \cdot 10^{-5} (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.93 (lb/h)/lbf$

$= 1.85 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 77.1 kg/s = 170 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR =

OPR = 8.4

OPR_{cr} =

FPR =

TET = °K

$M_{cr} = , h_{cr} = m$

RM8A

Manufacturer: Volvo

Application: AJ/SF/SH/SK 27

Composition: 2 / 4B / 7 / 1 / - / 3

$D_{fan} = m = in$

$D = m$

Nb of shafts = 2

$L = m$

$W_{eng} = kg = lb$

$= in$

$= in$

Static Sea Level:

$T_{ssl} = 62275 N$

$T_{ssl}^{AB} = 115653 N$

Cruise:

$T_{cr} = N$

$= 14000 lbf$

$= 26000 lbf$

$= lbf$

$SFC_{ssl} = 1.66 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$SFC_{cr} = (kg/s)/N$

$= 0.58 (lb/h)/lbf$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 143.3 kg/s = 315.9 lb/s$

$\dot{w}_{cr} = kg/s = lb/s$

BPR = 1.07

OPR = 15.4

OPR_{cr} =

FPR = 1.93

TET = °K

$M_{cr} = , h_{cr} = m$

RM8B

Manufacturer: Volvo

Application: JA 37

Composition: 2 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 72950 \text{ N}$ $T_{ssl}^{AB} = 124994 \text{ N}$

$= 16400 \text{ lbf}$ $= 28100 \text{ lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 0.96 OPR = 16.9

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM9A

Manufacturer: Turboméca

Application: SK 6A/B/C/D/E

Composition: 1G / - / 1 + 1C / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7273 \text{ N}$ $T_{ssl}^{AB} = N$

$= 1635 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 21.8 \text{ kg/s} = 48.1 \text{ lb/s}$

BPR = 2 OPR = 6.9

FPR = 1.5 TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

RM9B

Manufacturer: Turboméca

Application: SK 6A/B/C/D/E

Composition: 1G / - / 1 + 1C / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8229 \text{ N}$ $T_{ssl}^{AB} = N$

$= 1850 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 21.8 \text{ kg/s} = 48.1 \text{ lb/s}$

BPR = 2 OPR = 6.9

FPR = 1.5 TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

S.1

Manufacturer: Heinkel

Application: Prototype

Composition: - / - / 1C / 1R / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 783 N$ $T_{ssl}^{AB} = N$

$= 176 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

S.2

Manufacturer: Heinkel

Application: Prototype

Composition: - / - / 1C / 1R / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 1272 N$ $T_{ssl}^{AB} = N$

$= 286 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

S.3A

Manufacturer: Heinkel

Application: He 110, He 18

Composition: - / - / 1C / 1R / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4413 N$ $T_{ssl}^{AB} = N$

$= 992 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

S.3B

Manufacturer: Heinkel

Application: He 178

Composition: - / - / 1C / 1R / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 4413 N$ $T_{ssl}^{AB} = N$
 $= 992 lbf$ $= lbf$

$SFC_{ssl} = 4.53 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.6 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 11.8 kg/s = 26 lb/s$

BPR = OPR = 2.8

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

S.6

Manufacturer: Heinkel

Application:

Composition: - / - / 1C / 1R / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 5787 N$ $T_{ssl}^{AB} = N$
 $= 1301 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

SaM146

Manufacturer: PowerJet

Application: RRJ, Il-214 (candidate engine)

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 66723 N$ $T_{ssl}^{AB} = N$
 $= 15000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Sapphire ASSa.1 Mk.100

Manufacturer: Armstrong Siddeley

Application: Valient prototype

Composition: - / - / 13 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 33362 \text{ N}$ $T_{ssl}^{AB} = N$

$= 7500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Sapphire ASSa.6 Mk.101

Manufacturer: Armstrong Siddeley

Application: Hunter F.2/F.5, Hunter prototype, Javelin

F(AW).1/F(AW).2/T.3/F(AW).4/F(AW).5/F(AW).6, FFA P-16

Composition: - / - / 13 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 36920 \text{ N}$ $T_{ssl}^{AB} = N$

$= 8300 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Sapphire ASSa.7 Mk.200

Manufacturer: Armstrong Siddeley

Application: Javelin F(AW).7, P-16, Victor B.1/B.1A/B(K).1/B(K).1A

Composition: - / - / 13 / 2 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

$T_{ssl} = 48930 \text{ N}$ $T_{ssl}^{AB} = N$

$= 11000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Sapphire ASSa.7R Mk.200R

Manufacturer: Armstrong Siddeley

Application: Javelin F(AW).8/F(AW).9R

Composition: - / - / 13 / 2 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 48930 \text{ N}$ $T_{ssl}^{AB} = 54713 \text{ N}$
 $= 11000 \text{ lbf}$ $= 12300 \text{ lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

SM-X

Manufacturer: SNECMA

Application: Bizjets

Composition: 1 / - / 4C / 1 / - / 3

$D_{fan} = 0.925 \text{ m} = 36.4 \text{ in}$ $D = 0.108 \text{ m}$
 $W_{eng} = kg = lb$ $= 4.3 \text{ in}$

Static Sea Level:

$T_{ssl} = 45000 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 10116 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR = 5$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2
 $L = 1.5 \text{ m}$
 $= 59.1 \text{ in}$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

SO-1

Manufacturer: PZL Rzeszów

Application: TS-11A/B/C/D

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7847 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 1764 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = 2.95 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.04 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 18.1 \text{ kg/s} = 39.9 \text{ lb/s}$
 $BPR =$ $OPR = 4.8$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

SO-3

Manufacturer: PZL Rzeszów

Application: TS-11A/B/C/D

Composition: - / - / 7 / 1 / - / -

$D_{fan} = 0.707 \text{ m} = 27.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 321 \text{ kg} = 708 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 10790 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 2426 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 0$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

$L = 2.151 \text{ m}$

$= 84.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

SO-3W

Manufacturer: PZL Rzeszów

Application: TS-11DF

Composition: - / - / 7 / 1 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 10787 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 2425 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Spey Jr. RB.183-2 Mk.555-15

Manufacturer: Rolls-Royce

Application: F28 Mk.1000/Mk.1000C/Mk.2000

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = \text{m}$

$W_{eng} = 1024 \text{ kg} = 2258 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 43815 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 9850 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.12 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.75 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 90.3 \text{ kg/s} = 199.1 \text{ lb/s}$

$BPR = 1$ $OPR = 15.4$

$FPR = 2.46$ $TET = 990 ^\circ\text{K}$

Year: 1965

Nb of shafts = 2

$L = 2.464 \text{ m}$

$= 97 \text{ in}$

Cruise:

$T_{cr} = 16481 \text{ N}$

$= 3705 \text{ lbf}$

$SFC_{cr} = 2.24 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.79 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.7, h_{cr} = 7620 \text{ m}$

Spey Jr. RB.183-2 Mk.555-15H

Manufacturer: Rolls-Royce

Application: F28 Mk.6000, F28 Mk.5000/Mk.6600 (not produced)

Composition: 4 / - / 12 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = \text{m}$

$L = 2.464 \text{ m}$

$W_{eng} = 1024 \text{ kg} = 2258 \text{ lb}$ $= \text{in}$

$= 97 \text{ in}$

Static Sea Level:

$T_{ssl} = \text{N}$ $T_{ssl}^{AB} = \text{N}$

$= \text{lb}$ $= \text{lb}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lb}$ $= (\text{lb/h})/\text{lb}$

$\dot{w}_{ssl} = 90.3 \text{ kg/s} = 199.1 \text{ lb/s}$

BPR = 1 OPR = 15.4

FPR = 2.46 TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lb}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lb}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Spey Jr. RB.183-2 Mk.555-15P

Manufacturer: Rolls-Royce

Application: F28 Mk.3000/Mk.4000

Composition: 4 / - / 12 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = \text{m}$

$L = 2.464 \text{ m}$

$W_{eng} = 1024 \text{ kg} = 2258 \text{ lb}$ $= \text{in}$

$= 97 \text{ in}$

Static Sea Level:

$T_{ssl} = 44037 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 9900 \text{ lb}$ $= \text{lb}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lb}$ $= (\text{lb/h})/\text{lb}$

$\dot{w}_{ssl} = 90.3 \text{ kg/s} = 199.1 \text{ lb/s}$

BPR = 1 OPR = 15.4

FPR = 2.46 TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lb}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lb}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Spey RB.168-?? Mk.511-8

Manufacturer: Rolls-Royce

Application: C-20A/B/D

Composition: 5 / - / 12 / 2 / - / 2

Nb of shafts = 2

$D_{fan} = \text{m} = \text{in}$ $D = 0.826 \text{ m}$

$L = 2.784 \text{ m}$

$W_{eng} = 1126 \text{ kg} = 2482 \text{ lb}$ $= 32.5 \text{ in}$

$= 109.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 50709 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11400 \text{ lb}$ $= \text{lb}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.6 (\text{lb/h})/\text{lb}$ $= (\text{lb/h})/\text{lb}$

$\dot{w}_{ssl} = 89.4 \text{ kg/s} = 197.1 \text{ lb/s}$

BPR = 0.64 OPR = 18.4

FPR = 2.7 TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lb}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lb}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Spey RB.168 Mk.807

Manufacturer: Rolls-Royce

Application: AMX

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.826 m$

$W_{eng} = 1096 kg = 2416 lb$ $= 32.5 in$

Static Sea Level:

$T_{ssl} = 49064 N$ $T_{ssl}^{AB} = N$

$= 11030 lbf$ $= lbf$

$SFC_{ssl} = 1.87 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.66 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 91.6 kg/s = 201.9 lb/s$

$BPR = 0.96$ $OPR = 16.8$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = 2.456 m$

$= 96.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Spey RB.168-1A RSp.2 Mk.101

Manufacturer: Rolls-Royce

Application: Buccaneer S.2/S.2A/S.2B/S.2C/S.2D/S.50

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.826 m$

$W_{eng} = 1121 kg = 2471 lb$ $= 32.5 in$

Static Sea Level:

$T_{ssl} = 49064 N$ $T_{ssl}^{AB} = N$

$= 11030 lbf$ $= lbf$

$SFC_{ssl} = 1.79 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.63 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 0.7$ $OPR = 16.5$

$FPR = 2.7$ $TET = ^\circ K$

Nb of shafts = 2

$L = 2.911 m$

$= 114.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Spey RB.168-20 Mk.251

Manufacturer: Rolls-Royce

Application: Nimrod MR.1/R.1/MR.2/AEW.3

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.826 m$

$W_{eng} = 1243 kg = 2740 lb$ $= 32.5 in$

Static Sea Level:

$T_{ssl} = 53356 N$ $T_{ssl}^{AB} = N$

$= 11995 lbf$ $= lbf$

$SFC_{ssl} = 1.79 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.63 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 0.7$ $OPR = 19.2$

$FPR = 2.7$ $TET = ^\circ K$

Nb of shafts = 2

$L = 2.972 m$

$= 117 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Spey RB.168-20 RSp.5-1 Mk.250

Manufacturer: Rolls-Royce

Application: Nimrod MR.1/R.1/MR.2/AEW.3

Composition: 5 / - / 12 / 2 / - / 2

 $D_{fan} = m = in$ $D = 0.826 \text{ m}$
 $W_{eng} = 1243 \text{ kg} = 2740 \text{ lb}$ $= 32.5 \text{ in}$

Static Sea Level:

 $T_{ssl} = 53356 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 11995 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.63 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR = 0.7$ $OPR = 19.2$
 $FPR = 2.7$ $TET = ^\circ K$

Nb of shafts = 2

 $L = 2.972 \text{ m}$
 $= 117 \text{ in}$

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
Spey RB.168-25R RSp.2 Mk.201

Manufacturer: Rolls-Royce

Application: Phantom FG.1 (F-4K)

Composition: 5 / - / 12 / 2 / - / 2

 $D_{fan} = m = in$ $D = 1.118 \text{ m}$
 $W_{eng} = \text{kg} = \text{lb}$ $= 44 \text{ in}$

Static Sea Level:

 $T_{ssl} = 55825 \text{ N}$ $T_{ssl}^{AB} = 91255 \text{ N}$
 $= 12550 \text{ lbf}$ $= 20515 \text{ lbf}$
 $SFC_{ssl} = 1.79 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5.52 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.63 \text{ (lb/h)/lbf}$ $= 1.95 \text{ (lb/h)/lbf}$
 $\dot{w}_{ssl} = 95.3 \text{ kg/s} = 210.1 \text{ lb/s}$
 $BPR = 0.7$ $OPR = 20.1$
 $FPR = 2.7$ $TET = ^\circ K$

Nb of shafts = 2

 $L = 5.204 \text{ m}$
 $= 204.9 \text{ in}$

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
Spey RB.168-25R RSp.2 Mk.202

Manufacturer: Rolls-Royce

Application: Phantom FG.1/FGR.2 (F-4M)

Composition: 5 / - / 12 / 2 / - / 2

 $D_{fan} = m = in$ $D = 1.118 \text{ m}$
 $W_{eng} = 1857 \text{ kg} = 4094 \text{ lb}$ $= 44 \text{ in}$

Static Sea Level:

 $T_{ssl} = 54490 \text{ N}$ $T_{ssl}^{AB} = 91255 \text{ N}$
 $= 12250 \text{ lbf}$ $= 20515 \text{ lbf}$
 $SFC_{ssl} = 1.93 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.68 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR = 0.7$ $OPR = 19.5$
 $FPR = 2.7$ $TET = ^\circ K$

Nb of shafts = 2

 $L = 5.204 \text{ m}$
 $= 204.9 \text{ in}$

Cruise:

 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Spey RB.168-25R RSp.2 Mk.203

Manufacturer: Rolls-Royce

Application: Phantom FG.1/FGR.2

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.118 \text{ m}$

$W_{eng} = 1857 \text{ kg} = 4094 \text{ lb}$ $= 44 \text{ in}$

Static Sea Level:

$T_{ssl} = 54490 \text{ N}$ $T_{ssl}^{AB} = 91255 \text{ N}$

$= 12250 \text{ lbf}$ $= 20515 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 0.7$ $OPR = 19.5$

$FPR = 2.7$ $TET = ^\circ K$

Nb of shafts = 2

$L = 5.204 \text{ m}$

$= 204.9 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Spey RSp.1 Mk.505-5

Manufacturer: Rolls-Royce

Application: Trident 1/1C

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.94 \text{ m}$

$W_{eng} = 998 \text{ kg} = 2200 \text{ lb}$ $= 37 \text{ in}$

Static Sea Level:

$T_{ssl} = 55825 \text{ N}$ $T_{ssl}^{AB} = N$

$= 12550 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 92.1 \text{ kg/s} = 203 \text{ lb/s}$

$BPR = 0.71$ $OPR =$

$FPR = 2.7$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = 2.16 \cdot 10^{-5} (kg/s)/N$

$= 0.76 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.3 Mk.506-14

Manufacturer: Rolls-Royce

Application: BAC 111-200

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.94 \text{ m}$

$W_{eng} = 1024 \text{ kg} = 2258 \text{ lb}$ $= 37 \text{ in}$

Static Sea Level:

$T_{ssl} = 46306 \text{ N}$ $T_{ssl}^{AB} = N$

$= 10410 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 0.71$ $OPR =$

$FPR = 2.7$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = 2.16 \cdot 10^{-5} (kg/s)/N$

$= 0.76 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.3 Mk.506-14A

Manufacturer: Rolls-Royce

Application:

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.94 m$

$W_{eng} = 1024 kg = 2258 lb$ $= 37 in$

Static Sea Level:

$T_{ssl} = 46306 N$ $T_{ssl}^{AB} = N$

$= 10410 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.71 OPR =

FPR = 2.7 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = 13656 N$

$= 3070 lbf$

$SFC_{cr} = 2.16 \cdot 10^{-5} (kg/s)/N$

$= 0.76 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 m$

Spey RSp.3 Mk.506-14D

Manufacturer: Rolls-Royce

Application:

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.94 m$

$W_{eng} = 1024 kg = 2258 lb$ $= 37 in$

Static Sea Level:

$T_{ssl} = 46306 N$ $T_{ssl}^{AB} = N$

$= 10410 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.71 OPR =

FPR = 2.7 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = 13656 N$

$= 3070 lbf$

$SFC_{cr} = 2.16 \cdot 10^{-5} (kg/s)/N$

$= 0.76 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 m$

Spey RSp.3 Mk.506-2

Manufacturer: Rolls-Royce

Application:

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.94 m$

$W_{eng} = kg = lb$ $= 37 in$

Static Sea Level:

$T_{ssl} = 46306 N$ $T_{ssl}^{AB} = N$

$= 10410 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.71 OPR =

FPR = 2.7 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = 13656 N$

$= 3070 lbf$

$SFC_{cr} = 2.16 \cdot 10^{-5} (kg/s)/N$

$= 0.76 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 m$

Spey RSp.3W Mk.506-14AW

Manufacturer: Rolls-Royce

Application: BAC 111-200

Composition: 4 / - / 12 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.94 m$

$W_{eng} = 1038 kg = 2288 lb$ $= 37 in$

Static Sea Level:

$T_{ssl} = 46306 N$

$= 10410 lbf$

$SFC_{ssl} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.71

FPR = 2.7

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR =

TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = 13656 N$

$= 3070 lbf$

$SFC_{cr} = 2.16 \cdot 10^{-5} (kg/s)/N$

$= 0.76 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 m$

Spey RSp.4 Mk.510-14

Manufacturer: Rolls-Royce

Application: BAC 111-300/-400

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 m = 32.5 in$ $D = 0.942 m$

$W_{eng} = 1058 kg = 2332 lb$ $= 37.1 in$

Static Sea Level:

$T_{ssl} = 48930 N$

$= 11000 lbf$

$SFC_{ssl} = 1.7 \cdot 10^{-5} (kg/s)/N$

$= 0.6 (lb/h)/lbf$

$\dot{w}_{ssl} = 93.4 kg/s = 205.9 lb/s$

BPR = 0.71

FPR = 2.7

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR = 18.4

TET = °K

Nb of shafts = 2

$L = 2.784 m$

$= 109.6 in$

Cruise:

$T_{cr} = 13656 N$

$= 3070 lbf$

$SFC_{cr} = 2.18 \cdot 10^{-5} (kg/s)/N$

$= 0.77 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 m$

Spey RSp.4 Mk.510-14W

Manufacturer: Rolls-Royce

Application: BAC 111-300/-400

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 m = 32.5 in$ $D = 0.942 m$

$W_{eng} = 1189 kg = 2621 lb$ $= 37.1 in$

Static Sea Level:

$T_{ssl} = 48930 N$

$= 11000 lbf$

$SFC_{ssl} = 1.7 \cdot 10^{-5} (kg/s)/N$

$= 0.6 (lb/h)/lbf$

$\dot{w}_{ssl} = 93.4 kg/s = 205.9 lb/s$

BPR = 0.71

FPR = 2.7

$T_{ssl}^{AB} = N$

$= lbf$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

OPR = 18.4

TET = °K

Nb of shafts = 2

$L = 2.784 m$

$= 109.6 in$

Cruise:

$T_{cr} = 13656 N$

$= 3070 lbf$

$SFC_{cr} = 2.18 \cdot 10^{-5} (kg/s)/N$

$= 0.77 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 m$

Spey RSp.4 Mk.510-5

Manufacturer: Rolls-Royce

Application: Trident 1D

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1049 \text{ kg} = 2313 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 48930 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 0.71

OPR =

FPR = 2.7

TET = °K

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = 2.18 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.77 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.511-1

Manufacturer: Rolls-Royce

Application:

Composition: / / / / /

$D_{fan} = 0.824 \text{ m} = 32.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 1050 \text{ kg} = 2315 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 50718 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11402 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 92 \text{ kg/s} = 202.8 \text{ lb/s}$

BPR = 0.64

OPR = 19

FPR =

TET = 1350 °K

Nb of shafts =

$L = 2.91 \text{ m}$

$= 114.6 \text{ in}$

Cruise:

$T_{cr} = 19375 \text{ N}$

$= 4356 \text{ lbf}$

$SFC_{cr} = 2.24 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.79 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.7, h_{cr} = 7620 \text{ m}$

Spey RSp.4 Mk.511-14

Manufacturer: Rolls-Royce

Application: BAC 111-300/-400

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1126 \text{ kg} = 2482 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 50709 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.6 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 93.4 \text{ kg/s} = 205.9 \text{ lb/s}$

BPR = 0.71

OPR = 18.4

FPR = 2.7

TET = °K

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = 2.18 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.77 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.511-14W

Manufacturer: Rolls-Royce

Application: BAC 111-300/-400

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1189 \text{ kg} = 2621 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 50709 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 93.4 \text{ kg/s} = 205.9 \text{ lb/s}$

BPR = 0.71 OPR = 18.4

FPR = 2.7 TET = °K

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.77 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.511-5

Manufacturer: Rolls-Royce

Application: Trident 1E/2

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1049 \text{ kg} = 2313 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 50709 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 93.4 \text{ kg/s} = 205.9 \text{ lb/s}$

BPR = 0.71 OPR = 18.4

FPR = 2.7 TET = °K

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.77 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.511-5W

Manufacturer: Rolls-Royce

Application: Trident 1E/2

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1051 \text{ kg} = 2317 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 50709 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 93.4 \text{ kg/s} = 205.9 \text{ lb/s}$

BPR = 0.71 OPR = 18.4

FPR = 2.7 TET = °K

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.77 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.511-8

Manufacturer: Rolls-Royce

Year: 1968

Application: Gulfstream II/II-B/III

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1126 \text{ kg} = 2482 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 50709 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 11400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 89.4 \text{ kg/s} = 197.1 \text{ lb/s}$

BPR = 0.64 OPR = 18.4

FPR = 2.7 TET = °K

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = 2.18 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.77 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.512

Manufacturer: Rolls-Royce

Application: BAC 111-475/500

Composition: / / / /

$D_{fan} = 0.942 \text{ m} = 37.1 \text{ in}$ $D = \text{m}$

$W_{eng} = 1168 \text{ kg} = 2575 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 55800 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 12544 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 94.3 \text{ kg/s} = 207.9 \text{ lb/s}$

BPR = 0.71 OPR =

FPR = TET = °K

Nb of shafts =

$L = 2.911 \text{ m}$

$= 114.6 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Spey RSp.4 Mk.512-14

Manufacturer: Rolls-Royce

Application: BAC 111-475/-500, ROMBAC 111-560

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1183 \text{ kg} = 2608 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 55825 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 12550 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 93.4 \text{ kg/s} = 205.9 \text{ lb/s}$

BPR = 0.71 OPR = 20.7

FPR = 2.6 TET = °K

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.512-14DW

Manufacturer: Rolls-Royce

Application: BAC 111-475/-500, ROMBAC 111-560

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1183 \text{ kg} = 2608 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 55825 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 12550 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 93.4 \text{ kg/s} = 205.9 \text{ lb/s}$

$BPR = 0.71$ $OPR = 20.7$

$FPR = 2.6$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.512-14DWE

Manufacturer: Rolls-Royce

Application:

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1183 \text{ kg} = 2608 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 55825 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 12550 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 0.71$ $OPR =$

$FPR = 2.6$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.512-25

Manufacturer: Rolls-Royce

Application: BAC 111-475/-500, ROMBAC 111-560

Composition: 5 / - / 12 / 2 / - / 2

$D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$

$W_{eng} = 1183 \text{ kg} = 2608 \text{ lb}$ $= 37.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 55825 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 12550 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 93.4 \text{ kg/s} = 205.9 \text{ lb/s}$

$BPR = 0.71$ $OPR = 20.7$

$FPR = 2.6$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 2.784 \text{ m}$

$= 109.6 \text{ in}$

Cruise:

$T_{cr} = 13656 \text{ N}$

$= 3070 \text{ lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$

Spey RSp.4 Mk.512-5W**Manufacturer:** Rolls-Royce**Application:** Trident 2E/3B**Composition:** 5 / - / 12 / 2 / - / 2 $D_{fan} = 0.826 \text{ m} = 32.5 \text{ in}$ $D = 0.942 \text{ m}$ $W_{eng} = 1183 \text{ kg} = 2608 \text{ lb}$ $= 37.1 \text{ in}$ **Static Sea Level:** $T_{ssl} = 53378 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 12000 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 1.7 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$ $= 0.6 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = 93.4 \text{ kg/s} = 205.9 \text{ lb/s}$ $BPR = 0.71$ $OPR = 20.7$ $FPR = 2.6$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = 2.784 \text{ m}$ $= 109.6 \text{ in}$ **Cruise:** $T_{cr} = 13656 \text{ N}$ $= 3070 \text{ lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = 0.77, h_{cr} = 9754 \text{ m}$ **SPW14****Manufacturer:** Snecma/PWC**Application:** (cancelled)**Composition:** 1G / - / 4 + 1C / 2 / - / 3 $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 62275 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 14000 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = 2 $L = \text{m}$ $= \text{in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **Tay Mk.250 (Nene + AB)****Manufacturer:** Rolls-Royce**Application:** Mystère IIA/IIB, Mystère IV prototype**Composition:** / / / / / $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 27935 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 6280 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ\text{K}$ **Nb of shafts** = $L = \text{m}$ $= \text{in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = \text{(kg/s)/N}$ $= \text{(lb/h)/lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$

Tay RB.183-3 Mk.611

Manufacturer: Rolls-Royce
Application: F100.70, Gulfst.V
Composition: / / / /

Year: 1988

$D_{fan} = 1.52 \text{ m} = 59.8 \text{ in}$ $D = \text{m}$
 $W_{eng} = 1339 \text{ kg} = 2952 \text{ lb}$ $= \text{in}$

Nb of shafts =
 $L = 2.59 \text{ m}$
 $= 102 \text{ in}$

Static Sea Level:

$T_{ssl} = 61608 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 13850 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.22 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.43 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 186 \text{ kg/s} = 410.1 \text{ lb/s}$
 $BPR = 3.04$ $OPR = 15.8$
 $FPR =$ $TET = ^\circ\text{K}$

Cruise:

$T_{cr} = 11343 \text{ N}$
 $= 2550 \text{ lbf}$
 $SFC_{cr} = 1.95 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.69 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8$, $h_{cr} = 10668 \text{ m}$

Tay RB.183-3 Mk.611-8

Manufacturer: Rolls-Royce
Application: G300, G400 (Gulfstream IV/IV-SP), C-20G/H
Composition: 1 / 3B / 12 / 2 / - / 3

Nb of shafts = 2
 $L = 2.405 \text{ m}$
 $= 94.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 61608 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 13850 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.22 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.43 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 186 \text{ kg/s} = 410.1 \text{ lb/s}$
 $BPR = 3.04$ $OPR = 15.8$
 $FPR =$ $TET = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = 2.01 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.71 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8$, $h_{cr} = 13106 \text{ m}$

Tay RB.183-3 Mk.611-8C

Manufacturer: Rolls-Royce
Application: G350, G400
Composition: 1 / 3B / 12 / 2 / - / 3

Nb of shafts = 2
 $L = 2.405 \text{ m}$
 $= 94.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 61608 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 13850 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 1.22 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.43 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = 186 \text{ kg/s} = 410.1 \text{ lb/s}$
 $BPR = 3.04$ $OPR = 15.8$
 $FPR =$ $TET = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$
 $SFC_{cr} = 2.01 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 0.71 \text{ (lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = 0.8$, $h_{cr} = 13106 \text{ m}$

Tay RB.183-3 Mk.620-15

Manufacturer: Rolls-Royce

Application: Fokker 70

Composition: 1 / 3B / 12 / 2 / - / 3

$D_{fan} = 1.118 \text{ m} = 44 \text{ in}$ $D = \text{m}$

$W_{eng} = 1445 \text{ kg} = 3186 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 61608 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 13850 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 186 \text{ kg/s} = 410.1 \text{ lb/s}$

BPR = 3.04 OPR = 15.8

FPR = TET = °K

Nb of shafts = 2

$L = 2.405 \text{ m}$

$= 94.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = 1.95 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.69 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.73$, $h_{cr} = 9144 \text{ m}$

Tay RB.183-3 Mk.650

Manufacturer: Rolls-Royce

Application: Fokker100, Gulfstream IV

Composition: 1 / 3B / 12 / 2 / - / 3

$D_{fan} = 1.138 \text{ m} = 44.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 1515 \text{ kg} = 3340 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 67150 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 15096 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 192.8 \text{ kg/s} = 425.1 \text{ lb/s}$

BPR = 3.1 OPR = 16.4

FPR = TET = 1370 °K

Year:

Nb of shafts = 2

$L = 2.405 \text{ m}$

$= 94.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = 2 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.71 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8$, $h_{cr} = 10670 \text{ m}$

Tay RB.183-3 Mk.650-14

Manufacturer: Rolls-Royce

Application: BAC 111-475/-500/-560

Composition: 1 / 3B / 12 / 2 / - / 3

$D_{fan} = 1.138 \text{ m} = 44.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 1515 \text{ kg} = 3340 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 67168 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 15100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 189.6 \text{ kg/s} = 418 \text{ lb/s}$

BPR = 3.06 OPR = 16.2

FPR = TET = °K

Nb of shafts = 2

$L = 2.408 \text{ m}$

$= 94.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = 1.95 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.69 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.73$, $h_{cr} = 9144 \text{ m}$

Tay RB.183-3 Mk.650-15

Manufacturer: Rolls-Royce

Application: Fokker 100

Composition: 1 / 3B / 12 / 2 / - / 3

$D_{fan} = 1.138 \text{ m} = 44.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 1515 \text{ kg} = 3340 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 67168 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 15100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 189.6 \text{ kg/s} = 418 \text{ lb/s}$

BPR = 3.06 OPR = 16.2

FPR = TET = °K

Nb of shafts = 2

$L = 2.408 \text{ m}$

$= 94.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = 1.95 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.69 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.73, h_{cr} = 9144 \text{ m}$

Tay RB.183-3 Mk.651

Manufacturer: Rolls-Royce

Application: F100, B727-100

Composition: 1 / / / /

$D_{fan} = 1.52 \text{ m} = 59.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 1533 \text{ kg} = 3380 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 68503 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 15400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.27 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.45 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 193.2 \text{ kg/s} = 425.9 \text{ lb/s}$

BPR = 3.07 OPR = 16.6

FPR = TET = °K

Nb of shafts =

$L = 2.59 \text{ m}$

$= 102 \text{ in}$

Cruise:

$T_{cr} = 13122 \text{ N}$

$= 2950 \text{ lbf}$

$SFC_{cr} = 1.95 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.69 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 10668 \text{ m}$

Tay RB.183-3 Mk.651-54

Manufacturer: Rolls-Royce

Application: B727-100(QF)/-100C(QF)

Composition: 1 / 3B / 12 / 2 / - / 3

$D_{fan} = 1.138 \text{ m} = 44.8 \text{ in}$ $D = \text{m}$

$W_{eng} = 1533 \text{ kg} = 3380 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 68502 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 15400 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.28 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0.45 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 193.2 \text{ kg/s} = 425.9 \text{ lb/s}$

BPR = 3.07 OPR = 16.6

FPR = TET = °K

Nb of shafts = 2

$L = 2.405 \text{ m}$

$= 94.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = 1.95 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.69 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.78, h_{cr} = 10668 \text{ m}$

Tay RB.183-3 Mk.670

Manufacturer: Rolls-Royce

Application: B727-200RE, DC-9RE, B737-100RE/-200RE, MD-95 (proposed for re-engining)

Composition: 1 / 3B / 12 / 2 / - / 3

$D_{fan} = 1.27 \text{ m} = 50 \text{ in}$ $D = \text{m}$

$W_{eng} = 1701 \text{ kg} = 3750 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 80068 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 18000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 231.8 \text{ kg/s} = 511 \text{ lb/s}$

BPR = 3.2 OPR = 19

FPR = TET = °K

Nb of shafts = 2

$L = 2.845 \text{ m}$

$= 112 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Tay RB.183-55515P

Manufacturer: Rolls-Royce

Application: F28 Mk4000

Composition: / / / / /

$D_{fan} = 0.94 \text{ m} = 37 \text{ in}$ $D = \text{m}$

$W_{eng} = 1037 \text{ kg} = 2286 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 44037 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 9900 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.59 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.56 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 94.3 \text{ kg/s} = 207.9 \text{ lb/s}$

BPR = 0.71 OPR = 15.5

FPR = TET = °K

Year: 1969

Nb of shafts =

$L = 5.245 \text{ m}$

$= 206.5 \text{ in}$

Cruise:

$T_{cr} = 16592 \text{ N}$

$= 3730 \text{ lbf}$

$SFC_{cr} = 2.27 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.8 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.74 , h_{cr} = 7620 \text{ m}$

TF1000

Manufacturer: Agilis Engines

Application: S-26 Safire (candidate engine)

Composition: / / / / /

$D_{fan} = \text{m} = \text{in}$ $D = 0.584 \text{ m}$

$W_{eng} = 129 \text{ kg} = 284 \text{ lb}$ $= 23 \text{ in}$

Static Sea Level:

$T_{ssl} = 4448 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 1000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.13 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.4 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = 1.422 \text{ m}$

$= 56 \text{ in}$

Cruise:

$T_{cr} = 1201 \text{ N}$

$= 270 \text{ lbf}$

$SFC_{cr} = 1.81 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.64 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.6, h_{cr} = 9144 \text{ m}$

TF104

Manufacturer: SNECMA

Application: Mirage IIIV

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 53378 \text{ N}$ $T_{ssl}^{AB} = 88964 \text{ N}$

$= 12000 \text{ lbf}$ $= 20000 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

TF1200

Manufacturer: Agilis Engines

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = 0.584 \text{ m}$

$W_{eng} = 129 \text{ kg} = 284 \text{ lb}$ $= 23 \text{ in}$

Static Sea Level:

$T_{ssl} = 5729 \text{ N}$ $T_{ssl}^{AB} = N$

$= 1288 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 1.16 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.41 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = 1.422 \text{ m}$

$= 56 \text{ in}$

Cruise:

$T_{cr} = 1779 \text{ N}$

$= 400 \text{ lbf}$

$SFC_{cr} = 1.87 \cdot 10^{-5} (kg/s)/N$

$= 0.66 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = 0.6, h_{cr} = 9144 \text{ m}$

TF1400

Manufacturer: Agilis Engines

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = 0.584 \text{ m}$

$W_{eng} = 136 \text{ kg} = 300 \text{ lb}$ $= 23 \text{ in}$

Static Sea Level:

$T_{ssl} = 6227 \text{ N}$ $T_{ssl}^{AB} = N$

$= 1400 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 1.16 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.41 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = 1.422 \text{ m}$

$= 56 \text{ in}$

Cruise:

$T_{cr} = 1779 \text{ N}$

$= 400 \text{ lbf}$

$SFC_{cr} = 1.87 \cdot 10^{-5} (kg/s)/N$

$= 0.66 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = 0.6, h_{cr} = 9144 \text{ m}$

TF1500

Manufacturer: Agilis Engines

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = 0.584 m$

$W_{eng} = 136 kg = 300 lb$ $= 23 in$

Static Sea Level:

$T_{ssl} = 6672 N$ $T_{ssl}^{AB} = N$

$= 1500 lbf$ $= lbf$

$SFC_{ssl} = 1.16 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.41 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = 1.422 m$

$= 56 in$

Cruise:

$T_{cr} = 1766 N$

$= 397 lbf$

$SFC_{cr} = 1.93 \cdot 10^{-5} (kg/s)/N$

$= 0.68 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.6, h_{cr} = 9144 m$

TF30-PW-1

Manufacturer: Pratt & Whitney

Application: F-111A/C

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 47818 N$ $T_{ssl}^{AB} = 82292 N$

$= 10750 lbf$ $= 18500 lbf$

$SFC_{ssl} = 1.8 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.11 \cdot 10^{-5} (kg/s)/N$

$= 0.64 (lb/h)/lbf$ $= 2.51 (lb/h)/lbf$

$\dot{w}_{ssl} = 105.7 kg/s = 233 lb/s$

BPR = 1.1

OPR = 17.1

FPR =

TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-100

Manufacturer: Pratt & Whitney

Application: F-111F, X-27A (not produced)

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = 1.245 m$

$W_{eng} = 1814 kg = 3999 lb$ $= 49 in$

Static Sea Level:

$T_{ssl} = 68057 N$ $T_{ssl}^{AB} = 111650 N$

$= 15300 lbf$ $= 25100 lbf$

$SFC_{ssl} = 1.89 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$

$= 0.67 (lb/h)/lbf$ $= 2.5 (lb/h)/lbf$

$\dot{w}_{ssl} = 117.9 kg/s = 259.9 lb/s$

BPR = 0.73

OPR = 21.8

FPR = 2.43

TET = 1397 °K

Nb of shafts = 2

$L = 6.139 m$

$= 241.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-108

Manufacturer: Pratt & Whitney

Application: F-111C

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 90525 \text{ N}$ $T_{ssl}^{AB} = 90521 \text{ N}$

$= 20351 \text{ lbf}$ $= 20350 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 16.5

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-12

Manufacturer: Pratt & Whitney

Application: F-111B

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 97860 \text{ N}$

$= lbf$ $= 22000 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-18

Manufacturer: Pratt & Whitney

Application: A-7F

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 66723 \text{ N}$ $T_{ssl}^{AB} = N$

$= 15000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 22

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-3

Manufacturer: Pratt & Whitney

Application: F-111A/C, EF-111A

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = 1.346 m$

$W_{eng} = 1769 kg = 3900 lb$ $= 53 in$

Static Sea Level:

$T_{ssl} = 47818 N$ $T_{ssl}^{AB} = 82292 N$

$= 10750 lbf$ $= 18500 lbf$

$SFC_{ssl} = 2.27 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.1 \cdot 10^{-5} (kg/s)/N$

$= 0.8 (lb/h)/lbf$ $= 1.8 (lb/h)/lbf$

$\dot{w}_{ssl} = 105.7 kg/s = 233 lb/s$

BPR = 1.1 OPR = 17.1

FPR = 1.87 TET = 1144 °K

Nb of shafts = 2

$L = 3.454 m$

$= 136 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-408

Manufacturer: Pratt & Whitney

Application: A-7P, EA-7L, TA-7C/P

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 59606 N$ $T_{ssl}^{AB} = N$

$= 13400 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-412

Manufacturer: Pratt & Whitney

Application: F-14A

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 92967 N$

$= lbf$ $= 20900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.73 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-412A

Manufacturer: Pratt & Whitney

Application: F-14A

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 92967 N$
 $= lbf$ $= 20900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-414

Manufacturer: Pratt & Whitney

Application: F-14A

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 92967 N$
 $= lbf$ $= 20900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 19.8

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-414A

Manufacturer: Pratt & Whitney

Application: F-14A

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 92967 N$
 $= lbf$ $= 20900 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 19.6

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-6

Manufacturer: Pratt & Whitney

Application: A-7A

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = 1.069 m$

$W_{eng} = 1231 kg = 2714 lb$ $= 42.1 in$

Static Sea Level:

$T_{ssl} = 50487 N$ $T_{ssl}^{AB} = N$

$= 11350 lbf$ $= lbf$

$SFC_{ssl} = 1.76 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.62 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-7

Manufacturer: Pratt & Whitney

Application: FB-111A

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 90521 N$

$= lbf$ $= 20350 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-8

Manufacturer: Pratt & Whitney

Application: A-7B/C, TA-7C

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = 1.069 m$

$W_{eng} = 1146 kg = 2526 lb$ $= 42.1 in$

Static Sea Level:

$T_{ssl} = 54268 N$ $T_{ssl}^{AB} = N$

$= 12200 lbf$ $= lbf$

$SFC_{ssl} = 1.79 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.63 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 116.1 kg/s = 256 lb/s$

BPR = OPR = 17.1

FPR = 2 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF30-PW-9

Manufacturer: Pratt & Whitney

Application: F-111D/E

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 87185 N$
 $= lbf$ $= 19600 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF306C

Manufacturer: SNECMA

Application: Mirage F2

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 91188 N$
 $= lbf$ $= 20500 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF306E

Manufacturer: SNECMA

Application: Mirage F3

Composition: 3 / 6B / 7 / 1 / - / 3

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 52044 N$ $T_{ssl}^{AB} = 100974 N$
 $= 11700 lbf$ $= 22700 lbf$

$SFC_{ssl} = 1.84 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.67 \cdot 10^{-5} (kg/s)/N$
 $= 0.65 (lb/h)/lbf$ $= 2 (lb/h)/lbf$

$\dot{w}_{ssl} = 122.5 kg/s = 270.1 lb/s$

BPR = 1.1 OPR = 17

FPR = 2 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-100

Manufacturer: Pratt & Whitney

Application: E-8A

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 93412 \text{ N}$ $T_{ssl}^{AB} = N$

$= 21000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 15.6

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-100A

Manufacturer: Pratt & Whitney

Application: E-3A/B/C, E-8A

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 93412 \text{ N}$ $T_{ssl}^{AB} = N$

$= 21000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 15.6

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-102

Manufacturer: Pratt & Whitney

Application: KC-135E, C-18A, E-8C, TC-18A

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 80068 \text{ N}$ $T_{ssl}^{AB} = N$

$= 18000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 1.52 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.53 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 207.7 \text{ kg/s} = 457.9 \text{ lb/s}$

BPR = 1.37 OPR = 13.6

FPR = 1.74 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-102C

Manufacturer: Pratt & Whitney

Application: E-8C

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 80068 N$ $T_{ssl}^{AB} = 85405 N$

$= 18000 lbf$ $= 19200 lbf$

$SFC_{ssl} = 1.52 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.53 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 207.7 kg/s = 457.9 lb/s$

BPR = 1.37 OPR = 13.6

FPR = 1.74 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-11

Manufacturer: Pratt & Whitney

Application: RB-57F

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 80068 N$ $T_{ssl}^{AB} = N$

$= 18000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-11A

Manufacturer: Pratt & Whitney

Application: RB-57F

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 80068 N$ $T_{ssl}^{AB} = N$

$= 18000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-3

Manufacturer: Pratt & Whitney

Application: B-52H, NB-52H

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.346 m$

$W_{eng} = 1769 kg = 3900 lb$ $= 53 in$

Static Sea Level:

$T_{ssl} = 75619 N$ $T_{ssl}^{AB} = N$

$= 17000 lbf$ $= lbf$

$SFC_{ssl} = 1.47 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.52 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 204.1 kg/s = 450 lb/s$

BPR = 1.55 OPR = 13

FPR = 1.7 TET = 1144 °K

Nb of shafts = 2

$L = 3.454 m$

$= 136 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-5

Manufacturer: Pratt & Whitney

Application: C-135E, NC-135W, OC-135B, RC-135V/W, WC-135B

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.346 m$

$W_{eng} = 1891 kg = 4169 lb$ $= 53 in$

Static Sea Level:

$T_{ssl} = 80068 N$ $T_{ssl}^{AB} = N$

$= 18000 lbf$ $= lbf$

$SFC_{ssl} = 1.52 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.53 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-7

Manufacturer: Pratt & Whitney

Application: C-141A/B, E-3A

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.372 m$

$W_{eng} = 2109 kg = 4650 lb$ $= 54 in$

Static Sea Level:

$T_{ssl} = 93412 N$ $T_{ssl}^{AB} = N$

$= 21000 lbf$ $= lbf$

$SFC_{ssl} = 1.59 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.56 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 226.8 kg/s = 500 lb/s$

BPR = 1.21 OPR = 15.6

FPR = 1.9 TET = 1228 °K

Nb of shafts = 2

$L = 3.607 m$

$= 142 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-7A

Manufacturer: Pratt & Whitney

Application: C-141A/B, E-3A

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 93412 \text{ N}$ $T_{ssl}^{AB} = N$

$= 21000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 226.8 \text{ kg/s} = 500 \text{ lb/s}$

BPR = 1.21 OPR = 16

FPR = 1.9 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF33-PW-9

Manufacturer: Pratt & Whitney

Application: EC-135C, RC-135B/C, WC-135C

Composition: 2 / 7B / 7 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.346 \text{ m}$

$W_{eng} = 1891 \text{ kg} = 4169 \text{ lb}$ $= 53 \text{ in}$

Static Sea Level:

$T_{ssl} = 80068 \text{ N}$ $T_{ssl}^{AB} = N$

$= 18000 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 1.52 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.53 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF34-GE-100

Manufacturer: GE : General Electric

Application: A-10A, OA-10A, YA-10B

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = m = in$ $D = 1.27 \text{ m}$

$W_{eng} = 645 \text{ kg} = 1422 \text{ lb}$ $= 50 \text{ in}$

Static Sea Level:

$T_{ssl} = 40323 \text{ N}$ $T_{ssl}^{AB} = N$

$= 9065 \text{ lbf}$ $= lbf$

$SFC_{ssl} = 1.05 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.37 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 151 \text{ kg/s} = 332.9 \text{ lb/s}$

BPR = 6.42 OPR = 20

FPR = 1.5 TET = 1496 °K

Nb of shafts = 2

$L = 2.54 \text{ m}$

$= 100 \text{ in}$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF34-GE-100A

Manufacturer: GE : General Electric

Application: A-10A, OA-10A

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = m = in$ $D = 1.245 m$

$W_{eng} = 653 kg = 1440 lb$ $= 49 in$

Static Sea Level:

$T_{ssl} = 40323 N$ $T_{ssl}^{AB} = N$

$= 9065 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 151 kg/s = 332.9 lb/s$

BPR = 6.24 OPR = 20

FPR = 1.5 TET = °K

Nb of shafts = 2

$L = 2.54 m$

$= 100 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF34-GE-2

Manufacturer: GE : General Electric

Application: S-3A/B

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 41257 N$ $T_{ssl}^{AB} = N$

$= 9275 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 153.3 kg/s = 338 lb/s$

BPR = 6.23 OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF34-GE-400A

Manufacturer: GE : General Electric

Application: S-3B

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = m = in$ $D = 1.321 m$

$W_{eng} = 670 kg = 1477 lb$ $= 52 in$

Static Sea Level:

$T_{ssl} = 41257 N$ $T_{ssl}^{AB} = N$

$= 9275 lbf$ $= lbf$

$SFC_{ssl} = 1.03 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.36 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 153.3 kg/s = 338 lb/s$

BPR = 6.24 OPR = 21

FPR = 1.5 TET = °K

Nb of shafts = 2

$L = 2.54 m$

$= 100 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF34-GE-400B

Manufacturer: GE : General Electric

Application: S-3B

Composition: 1 / - / 14 / 2 / - / 4

$D_{fan} = m = in$ $D = 1.321 m$

$W_{eng} = 670 kg = 1477 lb$ $= 52 in$

Static Sea Level:

$T_{ssl} = 41257 N$ $T_{ssl}^{AB} = N$

$= 9275 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 153.3 kg/s = 338 lb/s$

BPR = 6.24 OPR = 21

FPR = 1.5 TET = °K

Nb of shafts = 2

$L = 2.54 m$

$= 100 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF37-GE-1

Manufacturer: GE : General Electric

Application:

Composition: 1 aft / - / 8 / 2 / - / 1

$D_{fan} = m = in$ $D = 0.843 m$

$W_{eng} = 306 kg = 675 lb$ $= 33.2 in$

Static Sea Level:

$T_{ssl} = 18682 N$ $T_{ssl}^{AB} = N$

$= 4200 lbf$ $= lbf$

$SFC_{ssl} = 1.85 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.65 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 38.1 kg/s = 84 lb/s$

BPR = 1.9 OPR = 6.9

FPR = TET = °K

Nb of shafts = 2

$L = 1.361 m$

$= 53.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF39-GE-1

Manufacturer: GE : General Electric

Application: C-5A

Composition: 1.5 / - / 16 / 3 / - / 6

$D_{fan} = 2.438 m = 96 in$ $D = 2.54 m$

$W_{eng} = 3260 kg = 7187 lb$ $= 100 in$

Static Sea Level:

$T_{ssl} = 181509 N$ $T_{ssl}^{AB} = N$

$= 40805 lbf$ $= lbf$

$SFC_{ssl} = 0.89 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.32 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 702.6 kg/s = 1549 lb/s$

BPR = 8 OPR = 26

FPR = 1.56 TET = 1561 °K

Nb of shafts = 2

$L = 5.156 m$

$= 203 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF39-GE-1C

Manufacturer: GE : General Electric

Application: C-5A

Composition: 1.5 / - / 16 / 3 / - / 6

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 191295 N$ $T_{ssl}^{AB} = N$

$= 43005 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 8 OPR =

FPR = 1.56 TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF39-GE-5CA

Manufacturer: GE : General Electric

Application: Lockheed Galaxy

Composition: / / / / /

$D_{fan} = 2.375 m = 93.5 in$ $D = m$

$W_{eng} = 3583 kg = 7899 lb$ $= in$

Static Sea Level:

$T_{ssl} = 182800 N$ $T_{ssl}^{AB} = N$

$= 41095 lbf$ $= lbf$

$SFC_{ssl} = 0.89 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.31 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 703 kg/s = 1549.8 lb/s$

BPR = 8 OPR = 25.7

FPR = TET = 1643 °K

Nb of shafts =

$L = 4.83 m$

$= 190.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF40-IHI-801A

Manufacturer: IHI : Ishikawajima-Harima Heavy Industries

Application: F-1, T-2A

Composition: 2 / - / 5 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.762 m$

$W_{eng} = 704 kg = 1552 lb$ $= 30 in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 32494 N$

$= lbf$ $= 7305 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = 2.1 \cdot 10^{-5} (kg/s)/N$

$= (lb/h)/lbf$ $= 0.74 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = 0.8 OPR = 11

FPR = TET = °K

Nb of shafts = 2

$L = 2.972 m$

$= 117 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF41-A-1

Manufacturer: Allison

Application: A-7D/H, TA-7H

Composition: 3 / 2B / 11 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.953 m$

$W_{eng} = 1475 kg = 3252 lb$ $= 37.5 in$

Static Sea Level:

$T_{ssl} = 63387 N$ $T_{ssl}^{AB} = N$

$= 14250 lbf$ $= lbf$

$SFC_{ssl} = 1.79 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.63 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 117 kg/s = 257.9 lb/s$

BPR = 0.77 OPR = 20

FPR = 2.45 TET = 1455 °K

Nb of shafts = 2

$L = 2.606 m$

$= 102.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF41-A-1B

Manufacturer: Allison

Application: A-7D K

Composition: 3 / 2B / 11 / 2 / - / 2

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1593 kg = 3512 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 64499 N$ $T_{ssl}^{AB} = N$

$= 14500 lbf$ $= lbf$

$SFC_{ssl} = 1.83 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.65 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 117.9 kg/s = 259.9 lb/s$

BPR = 0.76 OPR = 20

FPR = 2.45 TET = 1458 °K

Nb of shafts = 2

$L = 2.908 m$

$= 114.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF41-A-2

Manufacturer: Allison

Application: A-7E/G

Composition: 3 / 2B / 11 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.953 m$

$W_{eng} = 1475 kg = 3252 lb$ $= 37.5 in$

Static Sea Level:

$T_{ssl} = 66723 N$ $T_{ssl}^{AB} = N$

$= 15000 lbf$ $= lbf$

$SFC_{ssl} = 1.88 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.66 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 119.3 kg/s = 263 lb/s$

BPR = 0.74 OPR = 21.4

FPR = 2.49 TET = °K

Nb of shafts = 2

$L = 2.606 m$

$= 102.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF41-A-2B

Manufacturer: Allison

Application: A-7E/G

Composition: 3 / 2B / 11 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.953 m$

$W_{eng} = 1475 kg = 3252 lb$ $= 37.5 in$

Static Sea Level:

$T_{ssl} = 66723 N$ $T_{ssl}^{AB} = N$

$= 15000 lbf$ $= lbf$

$SFC_{ssl} = 1.88 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.66 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 119.3 kg/s = 263 lb/s$

BPR = 0.74 OPR = 21.4

FPR = 2.49 TET = °K

Nb of shafts = 2

$L = 2.606 m$

$= 102.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TF41-A-400

Manufacturer: Allison

Application: A-7E/G

Composition: 3 / 2B / 11 / 2 / - / 2

$D_{fan} = m = in$ $D = 0.953 m$

$W_{eng} = 1475 kg = 3252 lb$ $= 37.5 in$

Static Sea Level:

$T_{ssl} = 66723 N$ $T_{ssl}^{AB} = N$

$= 15000 lbf$ $= lbf$

$SFC_{ssl} = 1.88 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.66 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 119.3 kg/s = 263 lb/s$

BPR = 0.74 OPR = 21.4

FPR = 2.49 TET = °K

Nb of shafts = 2

$L = 2.606 m$

$= 102.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TFE1042-70

Manufacturer: ITEC

Application: China Indigenous Defense Fighter

Composition: 3 / - / 4 + 1C / 1 / - / 1

$D_{fan} = m = in$ $D = 0.591 m$

$W_{eng} = 617 kg = 1360 lb$ $= 23.3 in$

Static Sea Level:

$T_{ssl} = 26800 N$ $T_{ssl}^{AB} = 41146 N$

$= 6025 lbf$ $= 9250 lbf$

$SFC_{ssl} = 2.27 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.84 \cdot 10^{-5} (kg/s)/N$

$= 0.8 (lb/h)/lbf$ $= 2.06 (lb/h)/lbf$

$\dot{w}_{ssl} = 43.3 kg/s = 95.5 lb/s$

BPR = 0.3 OPR = 18.5

FPR = TET = °K

Nb of shafts = 2

$L = 3.561 m$

$= 140.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TFE109-1

Manufacturer: ASE : AlliedSignal Engines

Application: Jet Squalus ATTA/AWS/NGT

Composition: 2 / - / 2 / 2 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 5916 N$ $T_{ssl}^{AB} = N$

$= 1330 lbf$ $= lbf$

$SFC_{ssl} = 1.11 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.39 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

TFE731-1

Manufacturer: ASE : AlliedSignal Engines

Year: 1969

Application:

Composition: 1 / / 4 / 2 / / 3

$D_{fan} = 0.716 m = 28.2 in$ $D = m$

$W_{eng} = 272 kg = 600 lb$ $= in$

Static Sea Level:

$T_{ssl} = 15549 N$ $T_{ssl}^{AB} = N$

$= 3496 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 51.3 kg/s = 113.1 lb/s$

$BPR = 2.7$ $OPR = 19$

$FPR =$ $TET = 1285 ^\circ K$

Nb of shafts = 2

$L = 1.26 m$

$= 49.6 in$

Cruise:

$T_{cr} = 4002 N$

$= 900 lbf$

$SFC_{cr} = 2.35 \cdot 10^{-5} (kg/s)/N$

$= 0.83 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = 0.8 , h_{cr} = 11000 m$

TFE731-2

Manufacturer: ASE : AlliedSignal Engines

Application: C-21A, Falcon 10, Learjet 31/31A, SA-28T

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 m = 28.2 in$ $D = 1.016 m$

$W_{eng} = 283 kg = 624 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 15569 N$ $T_{ssl}^{AB} = N$

$= 3500 lbf$ $= lbf$

$SFC_{ssl} = 1.43 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.5 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 51.3 kg/s = 113.1 lb/s$

$BPR = 2.67$ $OPR = 17.7$

$FPR = 1.54$ $TET = ^\circ K$

Nb of shafts = 2

$L = 1.27 m$

$= 50 in$

Cruise:

$T_{cr} = 3358 N$

$= 755 lbf$

$SFC_{cr} = 2.31 \cdot 10^{-5} (kg/s)/N$

$= 0.82 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = 0.8 , h_{cr} = 12192 m$

TFE731-2-25

Manufacturer: ASE : AlliedSignal Engines

Application: C-101BB/EB

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.717 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 337 \text{ kg} = 743 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 15569 \text{ N}$

$= 3500 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.66

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 2

$L = 1.52 \text{ m}$

$= 59.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TFE731-2-2B

Manufacturer: ASE : AlliedSignal Engines

Application: Learjet 35/36, C-21A, EC-35A, PC-35A, RC-35A, UC-35A

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 337 \text{ kg} = 743 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 15569 \text{ N}$

$= 3500 \text{ lbf}$

$SFC_{ssl} = 1.43 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.5 (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 51.3 \text{ kg/s} = 113.1 \text{ lb/s}$

BPR = 2.66

FPR = 1.54

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 13

TET = °K

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TFE731-2-2N

Manufacturer: ASE : AlliedSignal Engines

Application: IA 63 NGA, IA 63

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 337 \text{ kg} = 743 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 15569 \text{ N}$

$= 3500 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.56

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TFE731-20

Manufacturer: ASE : AlliedSignal Engines

Application: Learjet 45

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 401 \text{ kg} = 884 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 15569 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = 1.25 \cdot 10^{-5} \text{ (kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.44 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 55.8 \text{ kg/s} = 123 \text{ lb/s}$

$\text{BPR} = 3.1$ $\text{OPR} = 21$

$\text{FPR} = 3.7$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.295 \text{ m}$

$= 51 \text{ in}$

Cruise:

$T_{cr} = 3897 \text{ N}$

$= 876 \text{ lbf}$

$\text{SFC}_{cr} = 2.06 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.73 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = 0.8, h_{cr} = 12192 \text{ m}$

TFE731-20AR

Manufacturer: ASE : AlliedSignal Engines

Application: Learjet 40

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 406 \text{ kg} = 895 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 15569 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 3.1$ $\text{OPR} =$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.295 \text{ m}$

$= 51 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

TFE731-20BR

Manufacturer: ASE : AlliedSignal Engines

Application: Learjet 40XR/45XR

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 406 \text{ kg} = 895 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 15569 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3500 \text{ lbf}$ $= \text{lbf}$

$\text{SFC}_{ssl} = \text{(kg/s)/N}$ $\text{SFC}_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\text{BPR} = 3.1$ $\text{OPR} =$

$\text{FPR} =$ $\text{TET} = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.295 \text{ m}$

$= 51 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$\text{SFC}_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$\text{OPR}_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

TFE731-3

Manufacturer: ASE : AlliedSignal Engines

Application: JetStar II

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 342 \text{ kg} = 754 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 16458 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3700 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.45 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.51 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 53.5 \text{ kg/s} = 117.9 \text{ lb/s}$

BPR = 2.8 OPR = 14.6

FPR = 2.8 TET = °K

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = 3634 \text{ N}$

$= 817 \text{ lbf}$

$SFC_{cr} = 2.32 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.82 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 12192 \text{ m}$

TFE731-3-100S

Manufacturer: ASE : AlliedSignal Engines

Application: Citation III

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 349 \text{ kg} = 769 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 16236 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3650 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 53.5 \text{ kg/s} = 117.9 \text{ lb/s}$

BPR = 2.8 OPR = 14.6

FPR = 2.8 TET = °K

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TFE731-3-1D

Manufacturer: ASE : AlliedSignal Engines

Application: Sabreliner 65

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 342 \text{ kg} = 754 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 16458 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3700 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 53.5 \text{ kg/s} = 117.9 \text{ lb/s}$

BPR = 2.8 OPR = 14.6

FPR = 2.8 TET = °K

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TFE731-3-1G

Manufacturer: ASE : AlliedSignal Engines

Application: 1124 Westwind

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 342 \text{ kg} = 754 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 16458 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3700 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 53.5 \text{ kg/s} = 117.9 \text{ lb/s}$

$BPR = 2.8$ $OPR = 14.6$

$FPR = 2.8$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

TFE731-3-1H

Manufacturer: ASE : AlliedSignal Engines

Application: BAe HS 125-600F/-700B, C-29A

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 342 \text{ kg} = 754 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 16458 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3700 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.45 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.51 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 53.5 \text{ kg/s} = 117.9 \text{ lb/s}$

$BPR = 2.8$ $OPR = 14.6$

$FPR = 2.8$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

TFE731-3A-2B

Manufacturer: ASE : AlliedSignal Engines

Application: Learjet 55B/55C/55C-LR

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 352 \text{ kg} = 776 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 16236 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3650 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.46 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.52 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 53.5 \text{ kg/s} = 117.9 \text{ lb/s}$

$BPR = 2.8$ $OPR = 14.6$

$FPR = 2.8$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = 3728 \text{ N}$

$= 838 \text{ lbf}$

$SFC_{cr} = 2.33 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.82 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.8, h_{cr} = 12192 \text{ m}$

TFE731-3A-300G

Manufacturer: ASE : AlliedSignal Engines

Application: Astra, Astra SP

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 352 \text{ kg} = 776 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 16236 \text{ N}$

$= 3650 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 53.5 \text{ kg/s} = 117.9 \text{ lb/s}$

BPR = 2.8

FPR = 2.8

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 14.6

TET = °K

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TFE731-3B-100

Manufacturer: ASE : AlliedSignal Engines

Application: Citation VI

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 340 \text{ kg} = 750 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 16236 \text{ N}$

$= 3650 \text{ lbf}$

$SFC_{ssl} = 1.44 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.51 (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 53.5 \text{ kg/s} = 117.9 \text{ lb/s}$

BPR = 2.8

FPR = 2.8

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 14.4

TET = °K

Nb of shafts = 2

$L = 1.262 \text{ m}$

$= 49.7 \text{ in}$

Cruise:

$T_{cr} = 3754 \text{ N}$

$= 844 \text{ lbf}$

$SFC_{cr} = 2.31 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.82 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 12192 \text{ m}$

TFE731-4

Manufacturer: ASE : AlliedSignal Engines

Application: Citation VII, Citation IV (not produced)

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 373 \text{ kg} = 822 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 18149 \text{ N}$

$= 4080 \text{ lbf}$

$SFC_{ssl} = 1.46 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.52 (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.4

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 14.8

TET = °K

Nb of shafts = 2

$L = 1.295 \text{ m}$

$= 51 \text{ in}$

Cruise:

$T_{cr} = 4132 \text{ N}$

$= 929 \text{ lbf}$

$SFC_{cr} = 2.26 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.8 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 12192 \text{ m}$

TFE731-4-1T

Manufacturer: ASE : AlliedSignal Engines

Application: L-139

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.729 \text{ m} = 28.7 \text{ in}$ $D = \text{m}$

$W_{eng} = 372 \text{ kg} = 820 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 18149 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 4080 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 2.4$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.477 \text{ m}$

$= 58.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

TFE731-40

Manufacturer: ASE : AlliedSignal Engines

Application: Falcon 50EX, Hawker 450

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 401 \text{ kg} = 884 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 18905 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 4250 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.29 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.46 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 65.8 \text{ kg/s} = 145.1 \text{ lb/s}$

$BPR = 2.9$ $OPR = 22$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.295 \text{ m}$

$= 51 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

TFE731-40AR-200G

Manufacturer: ASE : AlliedSignal Engines

Application: G150

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$

$W_{eng} = 406 \text{ kg} = 895 \text{ lb}$ $= 39.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 19661 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 4420 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 2.9$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 2

$L = 1.295 \text{ m}$

$= 51 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

TFE731-40R**Manufacturer:** ASE : AlliedSignal Engines**Application:** G100 (Astra SP), G150 (Astra SPX), IA 63 NGB**Composition:** 1G / 1C / 4 / 1 / - / 3

Nb of shafts = 2

 $D_{fan} = 0.716 \text{ m} = 28.2 \text{ in}$ $D = 1 \text{ m}$ $L = 1.295 \text{ m}$ $W_{eng} = 406 \text{ kg} = 895 \text{ lb}$ $= 39.4 \text{ in}$ $= 51 \text{ in}$ **Static Sea Level:** $T_{ssl} = 18905 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 4250 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 2.9

OPR =

FPR =

TET = °K

Cruise: $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$ **TFE731-40R-200G****Manufacturer:** ASE : AlliedSignal Engines**Application:** C-38A**Composition:** 1G / 1C / 4 / 1 / - / 3

Nb of shafts = 2

 $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $L = \text{m}$ $W_{eng} = 406 \text{ kg} = 895 \text{ lb}$ $= \text{in}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 18905 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 4250 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = 1.29 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= 0.46 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 65.8 \text{ kg/s} = 145.1 \text{ lb/s}$

BPR = 2.9

OPR = 22

FPR =

TET = °K

Cruise: $T_{cr} = \text{N}$ $= \text{lbf}$ $\text{SFC}_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = , h_{cr} = \text{m}$ **TFE731-5****Manufacturer:** ASE : AlliedSignal Engines**Year:** 1983**Application:** BAe HS 125-800, Sabreliner 85, CASA C-101, Dassault Falcon 900 et 20**Composition:** 1G / 1C / 4 / 1 / - / 3

Nb of shafts = 2

 $D_{fan} = 0.754 \text{ m} = 29.7 \text{ in}$ $D = 1.029 \text{ m}$ $L = 1.389 \text{ m}$ $W_{eng} = 401 \text{ kg} = 884 \text{ lb}$ $= 40.5 \text{ in}$ $= 54.7 \text{ in}$ **Static Sea Level:** $T_{ssl} = 20000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 4496 \text{ lbf}$ $= \text{lbf}$ $\text{SFC}_{ssl} = 1.33 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $\text{SFC}_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= 0.47 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 72.7 \text{ kg/s} = 160.3 \text{ lb/s}$

BPR = 3.15

OPR = 19.4

FPR = 1.67

TET = 1378 °K

Cruise: $T_{cr} = 4400 \text{ N}$ $= 989 \text{ lbf}$ $\text{SFC}_{cr} = 2.27 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $= 0.8 (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ OPR_{cr} = $M_{cr} = 0.8, h_{cr} = 12190 \text{ m}$

TFE731-5-1J

Manufacturer: ASE : AlliedSignal Engines

Application: C-101CC/DD

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = m = in$ $D = 1.029 m$

$W_{eng} = 386 kg = 851 lb$ $= 40.5 in$

Static Sea Level:

$T_{ssl} = 19145 N$ $T_{ssl}^{AB} = N$

$= 4304 lbf$ $= lbf$

$SFC_{ssl} = 1.37 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.48 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 64.9 kg/s = 143.1 lb/s$

BPR = 3.65 OPR = 14.4

FPR = 3.48 TET = °K

Nb of shafts = 2

$L = 1.665 m$

$= 65.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TFE731-5AR

Manufacturer: ASE : AlliedSignal Engines

Application: Falcon 900, Falcon 20RE

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.754 m = 29.7 in$ $D = 1.029 m$

$W_{eng} = 401 kg = 884 lb$ $= 40.5 in$

Static Sea Level:

$T_{ssl} = 20017 N$ $T_{ssl}^{AB} = N$

$= 4500 lbf$ $= lbf$

$SFC_{ssl} = 1.33 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.47 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 64.9 kg/s = 143.1 lb/s$

BPR = 3.65 OPR = 14.6

FPR = 3.48 TET = °K

Nb of shafts = 2

$L = 2.052 m$

$= 80.8 in$

Cruise:

$T_{cr} = 4386 N$

$= 986 lbf$

$SFC_{cr} = 2.18 \cdot 10^{-5} (kg/s)/N$

$= 0.77 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 12192 m$

TFE731-5BR

Manufacturer: ASE : AlliedSignal Engines

Application: Falcon 900B, Falcon 20RE, Hawker 800XP

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.754 m = 29.7 in$ $D = 1.029 m$

$W_{eng} = 408 kg = 899 lb$ $= 40.5 in$

Static Sea Level:

$T_{ssl} = 21129 N$ $T_{ssl}^{AB} = N$

$= 4750 lbf$ $= lbf$

$SFC_{ssl} = 1.33 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.47 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 64.9 kg/s = 143.1 lb/s$

BPR = 3.5 OPR = 15.1

FPR = 3.48 TET = °K

Nb of shafts = 2

$L = 2.052 m$

$= 80.8 in$

Cruise:

$T_{cr} = 4680 N$

$= 1052 lbf$

$SFC_{cr} = 2.14 \cdot 10^{-5} (kg/s)/N$

$= 0.76 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 12192 m$

TFE731-5BR-1C

Manufacturer: ASE : AlliedSignal Engines

Application: Falcon 900C

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.754 \text{ m} = 29.7 \text{ in}$ $D = 1.029 \text{ m}$

$W_{eng} = 408 \text{ kg} = 899 \text{ lb}$ $= 40.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 21129 \text{ N}$

$= 4750 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 3.2

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 2

$L = 2.052 \text{ m}$

$= 80.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TFE731-60

Manufacturer: ASE : AlliedSignal Engines

Application: Falcon 900EX

Composition: 1G / 1C / 4 / 1 / - / 3

$D_{fan} = 0.78 \text{ m} = 30.7 \text{ in}$ $D = 1.077 \text{ m}$

$W_{eng} = 448 \text{ kg} = 988 \text{ lb}$ $= 42.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 22241 \text{ N}$

$= 5000 \text{ lbf}$

$SFC_{ssl} = 1.15 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 0.4 (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 84.8 \text{ kg/s} = 187 \text{ lb/s}$

BPR = 3.9

FPR =

OPR = 22

TET = °K

Nb of shafts = 2

$L = 1.829 \text{ m}$

$= 72 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TJ-50

Manufacturer: Hamilton Sundstrand

Application: ADM-160A

Composition: - / - / 1 / 1 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = 0.176 \text{ m}$

$W_{eng} = 6 \text{ kg} = 13 \text{ lb}$ $= 6.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 245 \text{ N}$

$= 55 \text{ lbf}$

$SFC_{ssl} = 3.97 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= 1.4 (\text{lb/h})/\text{lbf}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

FPR =

OPR =

TET = °K

Nb of shafts = 1

$L = 0.305 \text{ m}$

$= 12 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

TJ400

Manufacturer: Agilis Engines

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = 0.381 \text{ m}$

$W_{eng} = 62 \text{ kg} = 137 \text{ lb}$ $= 15 \text{ in}$

Static Sea Level:

$T_{ssl} = 1793 \text{ N}$ $T_{ssl}^{AB} = N$

$= 403 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.55 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.9 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = 0.762 \text{ m}$

$= 30 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TJ60

Manufacturer: Agilis Engines

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = 0.127 \text{ m}$

$W_{eng} = 4 \text{ kg} = 9 \text{ lb}$ $= 5 \text{ in}$

Static Sea Level:

$T_{ssl} = 267 \text{ N}$ $T_{ssl}^{AB} = N$

$= 60 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.51 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 1.24 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = 0.343 \text{ m}$

$= 13.5 \text{ in}$

Cruise:

$T_{cr} = 133 \text{ N}$

$= 30 \text{ lbf}$

$SFC_{cr} = 4.25 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 1.5 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.9, h_{cr} = 6096 \text{ m}$

TJ75

Manufacturer: Agilis Engines

Application:

Composition: / / / /

$D_{fan} = m = in$ $D = 0.178 \text{ m}$

$W_{eng} = 4 \text{ kg} = 9 \text{ lb}$ $= 7 \text{ in}$

Static Sea Level:

$T_{ssl} = 334 \text{ N}$ $T_{ssl}^{AB} = N$

$= 75 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.51 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 1.24 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = 0.343 \text{ m}$

$= 13.5 \text{ in}$

Cruise:

$T_{cr} = 214 \text{ N}$

$= 48 \text{ lbf}$

$SFC_{cr} = 4.25 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 1.5 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.9, h_{cr} = 6096 \text{ m}$

TJ80

Manufacturer: Agilis Engines

Application:

Composition: / / / / /

$D_{fan} = m = in$ $D = 0.127\ m$
 $W_{eng} = 4\ kg = 9\ lb$ $= 5\ in$

Static Sea Level:

$T_{ssl} = 320\ N$ $T_{ssl}^{AB} = N$
 $= 72\ lbf$ $= lbf$
 $SFC_{ssl} = 3.51\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.24\ (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = 0.343\ m$
 $= 13.5\ in$

Cruise:

$T_{cr} = 214\ N$
 $= 48\ lbf$
 $SFC_{cr} = 4.25\ 10^{-5}\ (kg/s)/N$
 $= 1.5\ (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = 0.9$, $h_{cr} = 6096\ m$

TJM3

Manufacturer: Mitsubishi

Application: Target drone

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = 0.356\ m$
 $W_{eng} = 46\ kg = 101\ lb$ $= 14\ in$

Static Sea Level:

$T_{ssl} = 1962\ N$ $T_{ssl}^{AB} = N$
 $= 441\ lbf$ $= lbf$
 $SFC_{ssl} = 3.31\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.17\ (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 5.6$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 0.864\ m$
 $= 34\ in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} =$, $h_{cr} = m$

TJM4

Manufacturer: Mitsubishi

Application: UAV

Composition: - / - / 2 / 2 / - / -

$D_{fan} = m = in$ $D = 0.356\ m$
 $W_{eng} = 56\ kg = 123\ lb$ $= 14\ in$

Static Sea Level:

$T_{ssl} = 2842\ N$ $T_{ssl}^{AB} = N$
 $= 639\ lbf$ $= lbf$
 $SFC_{ssl} = 3.17\ 10^{-5}\ (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.12\ (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 6.7$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 1.092\ m$
 $= 43\ in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} =$, $h_{cr} = m$

TR-1

Manufacturer: Lyulka

Application: Il-22 'Coot-B'

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = 8661 N$

$= 3000 lbf$ $= 1947 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Trent 1000

Manufacturer: Rolls-Royce

Year: 2008

Application: B787-3/-8/-9, A350-800/-900 (expected)

Composition: 1 / 8 / 6 / 1 / 1 / 6

$D_{fan} = 2.845 m = 112 in$ $D = m$

$W_{eng} = 6437 kg = 14191 lb$ $= in$

Static Sea Level:

$T_{ssl} = 235755 N$ $T_{ssl}^{AB} = N$

$= 53000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 1247.4 kg/s = 2750 lb/s$

BPR = 10.8 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = 3.861 m$

$= 152 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Trent 1700

Manufacturer: Rolls-Royce

Year: 2011

Application: A350-84?

Composition: 1 / 7 / 6 / / /

$D_{fan} = 2.845 m = 112 in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 334000 N$ $T_{ssl}^{AB} = N$

$= 75086 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 3

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Trent 553-61

Manufacturer: Rolls-Royce

Application: A340-541

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4717 \text{ kg} = 10399 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 248130 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 55782 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 837.8 \text{ kg/s} = 1847 \text{ lb/s}$

BPR = 7.7 OPR = 35.1

FPR = TET = °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 556-61

Manufacturer: Rolls-Royce

Application: A340-642

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4717 \text{ kg} = 10399 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 260064 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 58465 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 858.2 \text{ kg/s} = 1892 \text{ lb/s}$

BPR = 7.32 OPR = 35.6

FPR = TET = 1581 °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = 1.65 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.58 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8, h_{cr} = 9144 \text{ m}$

Trent 560-61

Manufacturer: Rolls-Royce

Application:

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4717 \text{ kg} = 10399 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 261500 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 58788 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 7.5 OPR = 36.7

FPR = TET = °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 600

Manufacturer: Rolls-Royce

Application: MD-11 (option)

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = 2.591 \text{ m}$

$W_{eng} = 4719 \text{ kg} = 10404 \text{ lb}$ $= 102 \text{ in}$

Static Sea Level:

$T_{ssl} = 302478 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 68000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 921.7 \text{ kg/s} = 2032 \text{ lb/s}$

$BPR = 8$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Trent 665

Manufacturer: Rolls-Royce

Application: B747-XQLR (candidate engine), B747-500X/-600X (not produced)

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = 2.591 \text{ m}$

$W_{eng} = 5171 \text{ kg} = 11400 \text{ lb}$ $= 102 \text{ in}$

Static Sea Level:

$T_{ssl} = 289133 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 65000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 7$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Trent 672

Manufacturer: Rolls-Royce

Application: B767-400ERX

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = 2.591 \text{ m}$

$W_{eng} = 5171 \text{ kg} = 11400 \text{ lb}$ $= 102 \text{ in}$

Static Sea Level:

$T_{ssl} = 320270 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 72000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR =$ $OPR = 43.2$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Trent 758

Manufacturer: Rolls-Royce

Application: A330-141

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 257996 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 58000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 764

Manufacturer: Rolls-Royce

Application: MD-12 (not built)

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 284685 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 64000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 768-60

Manufacturer: Rolls-Royce

Application: A330-341, A330-241 (option)

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4785 \text{ kg} = 10549 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 300254 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 67500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 876.3 \text{ kg/s} = 1931.9 \text{ lb/s}$

BPR = 4.97 OPR = 35.2

FPR = TET = °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 772-60

Manufacturer: Rolls-Royce

Year: 1995

Application: A330-242/-342

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4785 \text{ kg} = 10549 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 316267 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 71100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 897.2 \text{ kg/s} = 1978 \text{ lb/s}$

BPR = 4.89 OPR = 36.8

FPR = TET = °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = 51154 \text{ N}$

$= 11500 \text{ lbf}$

$SFC_{cr} = 1.6 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.56 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.82, h_{cr} = 10668 \text{ m}$

Trent 772B-60

Manufacturer: Rolls-Royce

Application: A330-243/-343X

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4748 \text{ kg} = 10468 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 316279 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 71102 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 897.2 \text{ kg/s} = 1978 \text{ lb/s}$

BPR = 4.89 OPR = 36.8

FPR = TET = °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 775-60

Manufacturer: Rolls-Royce

Application: A330-244, A330-344 (option)

Composition: 1 / 8 / 6 / 1 / 1 / 4

$D_{fan} = 2.474 \text{ m} = 97.4 \text{ in}$ $D = \text{m}$

$W_{eng} = 4786 \text{ kg} = 10551 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 334282 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 75150 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 917.9 \text{ kg/s} = 2023.6 \text{ lb/s}$

BPR = 4.77 OPR = 39

FPR = TET = °K

Nb of shafts = 3

$L = 3.912 \text{ m}$

$= 154 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 8104

Manufacturer: Rolls-Royce

Application: B777-200X/-300X, Technology demonstrator

Composition: 1 / 8 / 6 / 1 / 1 / 5

Nb of shafts = 3

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$L = 4.369 \text{ m}$

$W_{eng} = 6532 \text{ kg} = 14401 \text{ lb}$ $= \text{in}$

$= 172 \text{ in}$

Static Sea Level:

$T_{ssl} = 462613 \text{ N}$
 $= 104000 \text{ lbf}$

$T_{ssl}^{AB} = \text{N}$
 $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 5.8

OPR = 45

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 871-17

Manufacturer: Rolls-Royce

Application: B777-200

Composition: 1 / 8 / 6 / 1 / 1 / 5

Nb of shafts = 3

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$L = 4.369 \text{ m}$

$W_{eng} = 5942 \text{ kg} = 13100 \text{ lb}$ $= \text{in}$

$= 172 \text{ in}$

Static Sea Level:

$T_{ssl} = 315822 \text{ N}$
 $= 71000 \text{ lbf}$

$T_{ssl}^{AB} = \text{N}$
 $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 875-17

Manufacturer: Rolls-Royce

Application: B777-200

Composition: 1 / 8 / 6 / 1 / 1 / 5

Nb of shafts = 3

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$L = 4.369 \text{ m}$

$W_{eng} = 5942 \text{ kg} = 13100 \text{ lb}$ $= \text{in}$

$= 172 \text{ in}$

Static Sea Level:

$T_{ssl} = 346515 \text{ N}$
 $= 77900 \text{ lbf}$

$T_{ssl}^{AB} = \text{N}$
 $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1125.8 \text{ kg/s} = 2482 \text{ lb/s}$

BPR = 6.21

OPR = 34.9

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 877-17

Manufacturer: Rolls-Royce

Application: B777-200

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 5942 \text{ kg} = 13100 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 359059 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 80720 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1169.4 \text{ kg/s} = 2578.1 \text{ lb/s}$

BPR = 6.15 OPR = 35.9

FPR = TET = °K

Nb of shafts = 3

$L = 4.369 \text{ m}$

$= 172 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 882-17

Manufacturer: Rolls-Royce

Application: B777-200 (option)

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 5942 \text{ kg} = 13100 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 376763 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 84700 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 38.8

FPR = TET = °K

Nb of shafts = 3

$L = 4.369 \text{ m}$

$= 172 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 884-17

Manufacturer: Rolls-Royce

Application: B777-200/-200ER

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 5942 \text{ kg} = 13100 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 386593 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 86910 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1207 \text{ kg/s} = 2661 \text{ lb/s}$

BPR = 5.95 OPR = 39.8

FPR = TET = °K

Nb of shafts = 3

$L = 4.369 \text{ m}$

$= 172 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 890-17

Manufacturer: Rolls-Royce

Application: B777-200ER/-300, Tu-304 (proposed)

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 5942 \text{ kg} = 13100 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 406121 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 91300 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1233.8 \text{ kg/s} = 2720.1 \text{ lb/s}$

$BPR = 5.74$ $OPR = 42.7$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 4.369 \text{ m}$

$= 172 \text{ in}$

Cruise:

$T_{cr} = 57827 \text{ N}$

$= 13000 \text{ lbf}$

$SFC_{cr} = 1.58 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.56 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.83, h_{cr} = 10668 \text{ m}$

Trent 892-17

Manufacturer: Rolls-Royce

Application: B777-200ER/-300/-300ER

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 5957 \text{ kg} = 13133 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 406788 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 91450 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1199.7 \text{ kg/s} = 2644.9 \text{ lb/s}$

$BPR = 5.79$ $OPR = 40.8$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 4.369 \text{ m}$

$= 172 \text{ in}$

Cruise:

$T_{cr} = 57827 \text{ N}$

$= 13000 \text{ lbf}$

$SFC_{cr} = 1.58 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.56 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = 0.83, h_{cr} = 10668 \text{ m}$

Trent 895-17

Manufacturer: Rolls-Royce

Application: B777-200ER/-300/-300ER (option)

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 5981 \text{ kg} = 13186 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 422579 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 95000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1208.4 \text{ kg/s} = 2664.1 \text{ lb/s}$

$BPR = 5.79$ $OPR = 41.6$

$FPR = 1.81$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 4.369 \text{ m}$

$= 172 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} =, h_{cr} = \text{m}$

Trent 895C-17

Manufacturer: Rolls-Royce

Application: B777-200ER/-300/-300ER (option)

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 5981 \text{ kg} = 13186 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 422579 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 95000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1208.4 \text{ kg/s} = 2664.1 \text{ lb/s}$

BPR = 5.79 OPR = 41.6

FPR = 1.81 TET = °K

Nb of shafts = 3

$L = 4.369 \text{ m}$

$= 172 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 900

Manufacturer: Rolls-Royce

Application: A380

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 6271 \text{ kg} = 13825 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 340289 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 76500 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = 0 \text{ lb/s}$

BPR = 7.14 OPR = 41

FPR = TET = 1593 °K

Year: 2004

Nb of shafts = 3

$L = 5.639 \text{ m}$

$= 222 \text{ in}$

Cruise:

$T_{cr} = 62275 \text{ N}$

$= 14000 \text{ lbf}$

$SFC_{cr} = 1.59 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.56 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.85 , h_{cr} = 10668 \text{ m}$

Trent 970-84

Manufacturer: Rolls-Royce

Application: A380-841

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = 3.942 \text{ m}$

$W_{eng} = 6271 \text{ kg} = 13825 \text{ lb}$ $= 155.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 334282 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 75150 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 7.1 OPR =

FPR = TET = °K

Nb of shafts = 3

$L = 4.5 \text{ m}$

$= 177.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 970B-84

Manufacturer: Rolls-Royce

Application: A380-841

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = 3.942 \text{ m}$

$W_{eng} = 6271 \text{ kg} = 13825 \text{ lb}$ $= 155.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 348294 \text{ N}$

$= 78300 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 7.1

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 3

$L = 4.5 \text{ m}$

$= 177.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 975

Manufacturer: Rolls-Royce

Application: B747-500X/-600X (not produced)

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = 3.942 \text{ m}$

$W_{eng} = 6271 \text{ kg} = 13825 \text{ lb}$ $= 155.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 333615 \text{ N}$

$= 75000 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1125.4 \text{ kg/s} = 2481.1 \text{ lb/s}$

BPR = 7.8

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR = 35.8

TET = °K

Nb of shafts = 3

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 976

Manufacturer: Rolls-Royce

Application:

Composition: / / / / /

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = \text{m}$

$W_{eng} = 5806 \text{ kg} = 12800 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 338000 \text{ N}$

$= 75985 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 1179 \text{ kg/s} = 2599.3 \text{ lb/s}$

BPR = 8

FPR =

$T_{ssl}^{AB} = \text{N}$

$= \text{lbf}$

$SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

OPR =

TET = °K

Nb of shafts = 3

$L = 4.369 \text{ m}$

$= 172 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Trent 977-84

Manufacturer: Rolls-Royce

Application: A380-843F

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = 3.942 \text{ m}$

$W_{eng} = 6271 \text{ kg} = 13825 \text{ lb}$ $= 155.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 359326 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 80780 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 7.1$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 4.5 \text{ m}$

$= 177.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Trent 977B-84

Manufacturer: Rolls-Royce

Application: A380-843F

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = 3.942 \text{ m}$

$W_{eng} = 6271 \text{ kg} = 13825 \text{ lb}$ $= 155.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 372915 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 83835 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 7.1$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 4.5 \text{ m}$

$= 177.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Trent 980-84

Manufacturer: Rolls-Royce

Application: A380-84?/-84?F (proposed future engine choice)

Composition: 1 / 8 / 6 / 1 / 1 / 5

$D_{fan} = 2.794 \text{ m} = 110 \text{ in}$ $D = 3.942 \text{ m}$

$W_{eng} = 6271 \text{ kg} = 13825 \text{ lb}$ $= 155.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 374094 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 84100 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$BPR = 7.1$ $OPR =$

$FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 3

$L = 4.5 \text{ m}$

$= 177.2 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

Trent-RB203,08

Manufacturer: Rolls-Royce

Year: 1967

Application:

Composition: / / / / /

$D_{fan} = 0.983 \text{ m} = 38.7 \text{ in}$ $D = \text{m}$

$W_{eng} = 805 \text{ kg} = 1775 \text{ lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 44439 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 9990 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 0 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 136 \text{ kg/s} = 299.8 \text{ lb/s}$

BPR = 3 OPR = 16

FPR = TET = °K

Nb of shafts =

$L = 2.09 \text{ m}$

$= 82.3 \text{ in}$

Cruise:

$T_{cr} = 12900 \text{ N}$

$= 2900 \text{ lbf}$

$SFC_{cr} = 2.04 \cdot 10^{-5} (\text{kg/s})/\text{N}$

$= 0.72 (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.7$, $h_{cr} = 7620 \text{ m}$

TRI 40-4

Manufacturer: Microturbo

Application: NSM

Composition: - / - / 4 / 1 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = 0.284 \text{ m}$

$W_{eng} = 44 \text{ kg} = 97 \text{ lb}$ $= 11.2 \text{ in}$

Static Sea Level:

$T_{ssl} = 3336 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 750 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.34 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 1.18 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 6

FPR = TET = °K

Nb of shafts = 1

$L = 0.678 \text{ m}$

$= 26.7 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

TRI 60-1

Manufacturer: Microturbo

Application: Sea Eagle

Composition: - / - / 3 / 1 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = 0.33 \text{ m}$

$W_{eng} = 49 \text{ kg} = 108 \text{ lb}$ $= 13 \text{ in}$

Static Sea Level:

$T_{ssl} = 3501 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 787 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.37 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= 1.19 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 3.7

FPR = TET = °K

Nb of shafts = 1

$L = 0.749 \text{ m}$

$= 29.5 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} =$, $h_{cr} = \text{m}$

TRI 60-2

Manufacturer: Microturbo

Application: MQM-107B, RBS 15M

Composition: - / - / 3 / 1 / - / -

$D_{fan} = m = in$ $D = 0.33 \text{ m}$

$W_{eng} = 49 \text{ kg} = 108 \text{ lb}$ $= 13 \text{ in}$

Static Sea Level:

$T_{ssl} = 3701 \text{ N}$ $T_{ssl}^{AB} = N$

$= 832 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.57 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 1.26 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

$L = 0.749 \text{ m}$

$= 29.5 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TRI 60-20

Manufacturer: Microturbo

Application: Super MQM-107D, Skua

Composition: - / - / 4 / 1 / - / -

$D_{fan} = m = in$ $D = 0.343 \text{ m}$

$W_{eng} = 64 \text{ kg} = 141 \text{ lb}$ $= 13.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 5338 \text{ N}$ $T_{ssl}^{AB} = N$

$= 1200 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 3.26 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 1.15 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 6.3

FPR = TET = °K

Nb of shafts = 1

$L = 0.841 \text{ m}$

$= 33.1 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TRI 60-3

Manufacturer: Microturbo

Application: C22 drone

Composition: - / - / 3 / 1 / - / -

$D_{fan} = m = in$ $D = 0.343 \text{ m}$

$W_{eng} = 61 \text{ kg} = 134 \text{ lb}$ $= 13.5 \text{ in}$

Static Sea Level:

$T_{ssl} = 4005 \text{ N}$ $T_{ssl}^{AB} = N$

$= 900 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 3.9

FPR = TET = °K

Nb of shafts = 1

$L = 1.067 \text{ m}$

$= 42 \text{ in}$

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TRI 60-30

Manufacturer: Microturbo

Application: APACHE A, Storm Shadow/Scalp EG

Composition: - / - / 4 / 1 / - / -

$D_{fan} = m = in$ $D = 0.343 m$

$W_{eng} = 61 kg = 134 lb$ $= 13.5 in$

Static Sea Level:

$T_{ssl} = 5338 N$ $T_{ssl}^{AB} = N$

$= 1200 lbf$ $= lbf$

$SFC_{ssl} = 2.97 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.05 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 6.3

FPR = TET = °K

Nb of shafts = 1

$L = 1.067 m$

$= 42 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TRI 60-5

Manufacturer: Microturbo

Application: MQM-107D/E, Skua, Lakshya

Composition: - / - / 3 / 1 / - / -

$D_{fan} = m = in$ $D = 0.33 m$

$W_{eng} = 53 kg = 117 lb$ $= 13 in$

Static Sea Level:

$T_{ssl} = 4404 N$ $T_{ssl}^{AB} = N$

$= 990 lbf$ $= lbf$

$SFC_{ssl} = 3.54 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.25 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 0.749 m$

$= 29.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TRS 18-046

Manufacturer: Microturbo

Application: C-22J/R

Composition: - / - / 1 / 1 / - / -

$D_{fan} = m = in$ $D = 0.302 m$

$W_{eng} = 37 kg = 82 lb$ $= 11.9 in$

Static Sea Level:

$T_{ssl} = 1001 N$ $T_{ssl}^{AB} = N$

$= 225 lbf$ $= lbf$

$SFC_{ssl} = 3.34 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.18 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.7

FPR = TET = °K

Nb of shafts = 1

$L = 0.599 m$

$= 23.6 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

TRS 18-1

Manufacturer: Microturbo

Application: Falconet, Mirach 150, Microjet 200, Mirach 100-2/-3/-5

Composition: - / - / 1 / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = 0.302 \text{ m}$

$L = 0.599 \text{ m}$

$W_{eng} = 38 \text{ kg} = 84 \text{ lb}$ $= 11.9 \text{ in}$

$= 23.6 \text{ in}$

Static Sea Level:

$T_{ssl} = 1157 \text{ N}$

$T_{ssl}^{AB} = N$

$= 260 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = 3.34 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 1.18 \text{ (lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR = 4.7

FPR =

TET = °K

Cruise:

$T_{cr} = N$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

V2500-A1

Manufacturer: IAE International Aero Engines : P&W + RR

Year: 1989

Application: A320-231, A319

Composition: 1 / 3B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.681 \text{ m} = 66.2 \text{ in}$ $D = 1.715 \text{ m}$

$L = 3.2 \text{ m}$

$W_{eng} = 2363 \text{ kg} = 5210 \text{ lb}$ $= 67.5 \text{ in}$

$= 126 \text{ in}$

Static Sea Level:

$T_{ssl} = 110310 \text{ N}$

$T_{ssl}^{AB} = N$

$= 24799 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.35 \text{ (lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 354.3 \text{ kg/s} = 781.1 \text{ lb/s}$

BPR = 5.42

OPR = 29.7

FPR = 1.7

TET = 1537 °K

Cruise:

$T_{cr} = 22552 \text{ N}$

$= 5070 \text{ lbf}$

$SFC_{cr} = 1.65 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.58 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 10668 \text{ m}$

V2522-A5

Manufacturer: IAE International Aero Engines : P&W + RR

Year: 1993

Application: MD90-10/30, A319-131

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.681 \text{ m} = 66.2 \text{ in}$ $D = 1.715 \text{ m}$

$L = 3.204 \text{ m}$

$W_{eng} = 2382 \text{ kg} = 5251 \text{ lb}$ $= 67.5 \text{ in}$

$= 126.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 102490 \text{ N}$

$T_{ssl}^{AB} = N$

$= 23041 \text{ lbf}$

$= \text{lbf}$

$SFC_{ssl} = 0.96 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 334.8 \text{ kg/s} = 738.1 \text{ lb/s}$

BPR = 4.9

OPR = 25.2

FPR =

TET = °K

Cruise:

$T_{cr} = 23064 \text{ N}$

$= 5185 \text{ lbf}$

$SFC_{cr} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.57 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 10668 \text{ m}$

V2522-D5

Manufacturer: IAE International Aero Engines : P&W + RR

Application: MD-90-10 (not produced)

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.613 \text{ m} = 63.5 \text{ in}$ $D = 1.715 \text{ m}$

$L = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= 67.5 \text{ in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 22000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.96 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.34 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 384.6 \text{ kg/s} = 847.9 \text{ lb/s}$

BPR = 4.9 OPR = 25.2

FPR = TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

V2524-A5

Manufacturer: IAE International Aero Engines : P&W + RR

Application: A319-132/-132CJ

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.613 \text{ m} = 63.5 \text{ in}$ $D = 1.715 \text{ m}$

$L = 3.201 \text{ m}$

$W_{eng} = 2331 \text{ kg} = 5139 \text{ lb}$ $= 67.5 \text{ in}$

$= 126 \text{ in}$

Static Sea Level:

$T_{ssl} = 108894 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 24480 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 350.2 \text{ kg/s} = 772.1 \text{ lb/s}$

BPR = 4.9 OPR = 26.5

FPR = TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

V2525-D5

Manufacturer: IAE International Aero Engines : P&W + RR

Year: 1994

Application: MD90-30/30ER

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.681 \text{ m} = 66.2 \text{ in}$ $D = 1.715 \text{ m}$

$L = 3.204 \text{ m}$

$W_{eng} = 2382 \text{ kg} = 5251 \text{ lb}$ $= 67.5 \text{ in}$

$= 126.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 111206 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 25000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 355.6 \text{ kg/s} = 784 \text{ lb/s}$

BPR = 4.8 OPR = 27.7

FPR = TET = °K

Cruise:

$T_{cr} = 25680 \text{ N}$

$= 5773 \text{ lbf}$

$SFC_{cr} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.57 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 10668 \text{ m}$

V2527-A5

Manufacturer: IAE International Aero Engines : P&W + RR

Application: A319-133CJ/-133XCJ, A320-232

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.613 \text{ m} = 63.5 \text{ in}$ $D = 1.715 \text{ m}$

$L = 3.2 \text{ m}$

$W_{eng} = 2331 \text{ kg} = 5139 \text{ lb}$ $= 67.5 \text{ in}$

$= 126 \text{ in}$

Static Sea Level:

$T_{ssl} = 110310 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 24799 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 384 \text{ kg/s} = 846.6 \text{ lb/s}$

$BPR = 4.75$ $OPR = 27.4$

$FPR =$ $TET = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

V2528-D5

Manufacturer: IAE International Aero Engines : P&W + RR

Application: MD-90-30/-30ER

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.613 \text{ m} = 63.5 \text{ in}$ $D = 1.715 \text{ m}$

$L = 3.2 \text{ m}$

$W_{eng} = 2382 \text{ kg} = 5251 \text{ lb}$ $= 67.5 \text{ in}$

$= 126 \text{ in}$

Static Sea Level:

$T_{ssl} = 124550 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 28000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 0.99 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.35 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 374.2 \text{ kg/s} = 825 \text{ lb/s}$

$BPR = 4.7$ $OPR = 30.4$

$FPR =$ $TET = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

V2530-A5

Manufacturer: IAE International Aero Engines : P&W + RR

Application: A321-131/-232

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.613 \text{ m} = 63.5 \text{ in}$ $D = 1.715 \text{ m}$

$L = \text{m}$

$W_{eng} = 2331 \text{ kg} = 5139 \text{ lb}$ $= 67.5 \text{ in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = 133000 \text{ N}$ $T_{ssl}^{AB} = \text{N}$
 $= 29900 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 385.1 \text{ kg/s} = 849 \text{ lb/s}$

$BPR = 4.6$ $OPR = 31.6$

$FPR =$ $TET = ^\circ\text{K}$

Cruise:

$T_{cr} = \text{N}$
 $= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = \text{m}$

V2530-D5

Manufacturer: IAE International Aero Engines : P&W + RR

Application: MD-90-50 (not produced)

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.613 \text{ m} = 63.5 \text{ in}$ $D = 1.715 \text{ m}$

$L = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= 67.5 \text{ in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = 133446 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 30000 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.02 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.36 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = 4.6

OPR = 31.6

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

V2533-A5

Manufacturer: IAE International Aero Engines : P&W + RR

Year: 1994

Application: A321-231

Composition: 1 / 4B / 10 / 2 / - / 5

Nb of shafts = 2

$D_{fan} = 1.613 \text{ m} = 63.5 \text{ in}$ $D = 1.715 \text{ m}$

$L = 3.204 \text{ m}$

$W_{eng} = 2331 \text{ kg} = 5139 \text{ lb}$ $= 67.5 \text{ in}$

$= 126.1 \text{ in}$

Static Sea Level:

$T_{ssl} = 140560 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 31599 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 1.05 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.37 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 395.5 \text{ kg/s} = 871.9 \text{ lb/s}$

BPR = 4.5

OPR = 33.4

FPR = 1.79

TET = °K

Cruise:

$T_{cr} = 25466 \text{ N}$

$= 5725 \text{ lbf}$

$SFC_{cr} = 1.63 \cdot 10^{-5} \text{ (kg/s)/N}$

$= 0.57 \text{ (lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 10668 \text{ m}$

VD-19

Manufacturer: Kolesov RKBM

Application: Tu-128S-4 'Fiddler-B'

Composition: / / / / /

Nb of shafts =

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$L = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

$= \text{in}$

Static Sea Level:

$T_{ssl} = \text{N}$ $T_{ssl}^{AB} = 127485 \text{ N}$

$= \text{lbf}$ $= 28660 \text{ lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR =

OPR =

FPR =

TET = °K

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

VD-5

Manufacturer: Dobrynin

Application:

Composition: / / / /

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 127485 N$

$T_{ssl}^{AB} = N$

$= 28660 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$

$OPR =$

$FPR =$

$TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

VD-7

Manufacturer: Dobrynin

Application: M-4 'Bison-A'

Composition: / / / /

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 107869 N$

$T_{ssl}^{AB} = N$

$= 24250 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$

$OPR =$

$FPR =$

$TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

VD-7B

Manufacturer: Dobrynin

Application: M-4 'Bison-A'

Composition: / / / /

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 93168 N$

$T_{ssl}^{AB} = N$

$= 20945 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$

$OPR =$

$FPR =$

$TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

VD-7D

Manufacturer: Dobrynin

Application: VM-T 'Atlant'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 105422 N$ $T_{ssl}^{AB} = N$

$= 23700 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

VD-7F

Manufacturer: Dobrynin

Application: M-52 'Bounder-B'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 177928 N$

$= lbf$ $= 40000 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

VD-7M

Manufacturer: Dobrynin

Application: Tu-22/-22B 'Blinder-A', Tu-22K/KD/KP/KDP 'Blinder-B', Tu-22P/PD 'Blinder-C', Tu-22U/UD 'Blinder-D', Tu-22R/RD/RK/RDK/RM/RDM 'Blinder-E', M-50 'Bounder-A'

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = N$ $T_{ssl}^{AB} = 156910 N$

$= lbf$ $= 35275 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Verdon

Manufacturer: Hispano-Suiza

Application: Mystère IVA

Composition: / / / /

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 34318 N$

$T_{ssl}^{AB} = N$

$= 7715 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper 20F20

Manufacturer: Rolls-Royce

Year: 1965

Application:

Composition: / / / /

$D_{fan} = 0.47 m = 18.5 in$

$D = m$

$W_{eng} = 270 kg = 595 lb$

$= in$

Static Sea Level:

$T_{ssl} = 15156 N$

$T_{ssl}^{AB} = N$

$= 3407 lbf$

$= lbf$

$SFC_{ssl} = (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= 0 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR = 0

OPR = 2.6

FPR =

TET = 1135 °K

Nb of shafts =

$L = 2.16 m$

$= 85 in$

Cruise:

$T_{cr} = 6543 N$

$= 1471 lbf$

$SFC_{cr} = 3.57 \cdot 10^{-5} (kg/s)/N$

$= 1.26 (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = 0.8 , h_{cr} = 11000 m$

Viper ASV.11 Mk.200

Manufacturer: Armstrong Siddeley

Application: T-51

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$

$D = m$

$W_{eng} = kg = lb$

$= in$

Static Sea Level:

$T_{ssl} = 11121 N$

$T_{ssl}^{AB} = N$

$= 2500 lbf$

$= lbf$

$SFC_{ssl} = 3.03 \cdot 10^{-5} (kg/s)/N$

$SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.07 (lb/h)/lbf$

$= (lb/h)/lbf$

$\dot{w}_{ssl} = 20 kg/s = 44.1 lb/s$

BPR =

OPR = 4.3

FPR =

TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper ASV.11 Mk.201

Manufacturer: Armstrong Siddeley

Application: 3A drone

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Nb of shafts = 1

$L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 11121 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 4.3$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Viper ASV.11 Mk.202

Manufacturer: Armstrong Siddeley

Application: Jet Provost T.4/T.5/T.5A/T.52/T.55, T-52

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Nb of shafts = 1

$L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 11121 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = 2.95 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.04 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 20 \text{ kg/s} = 44.1 \text{ lb/s}$
 $BPR =$ $OPR = 4.4$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Viper ASV.11 Mk.203

Manufacturer: Armstrong Siddeley

Application: Shackleton MR.3 (boosters)

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Nb of shafts = 1

$L = m$
 $= in$

Static Sea Level:

$T_{ssl} = 12010 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2700 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Viper ASV.11 Mk.22-1

Manufacturer: Armstrong Siddeley

Application: MB.326A/B/D/E/F

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = 0.836 m$

$W_{eng} = 281 kg = 619 lb$ $= 32.9 in$

Static Sea Level:

$T_{ssl} = 11121 N$ $T_{ssl}^{AB} = N$

$= 2500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 1.626 m$

$= 64 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Viper ASV.11 Mk.22-6

Manufacturer: Armstrong Siddeley

Application: G-2A Galeb

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 11121 N$ $T_{ssl}^{AB} = N$

$= 2500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Viper ASV.11 Mk.22-8

Manufacturer: Armstrong Siddeley

Application: HJT-16 Hiran I/IA

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 11121 N$ $T_{ssl}^{AB} = N$

$= 2500 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

Viper ASV.5

Manufacturer: Armstrong Siddeley

Application:

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7295 N$ $T_{ssl}^{AB} = N$
 $= 1640 lbf$ $= lbf$

$SFC_{ssl} = 3.09 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.09 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 13.6 kg/s = 30 lb/s$

BPR = OPR = 3.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper ASV.8 Mk.101

Manufacturer: Armstrong Siddeley

Application: Fo.139, Midge

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7295 N$ $T_{ssl}^{AB} = N$
 $= 1640 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper ASV.8 Mk.102

Manufacturer: Armstrong Siddeley

Application: Jet Provost T.1/T.3/T.3A/T.51

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7784 N$ $T_{ssl}^{AB} = N$
 $= 1750 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 14.5 kg/s = 32 lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper ASV.8 Mk.104

Manufacturer: Armstrong Siddeley

Application: 3B drone

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7784 N$ $T_{ssl}^{AB} = N$

$= 1750 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper ASV.9 Mk.103

Manufacturer: Armstrong Siddeley

Application: X-14, HP-115

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 8452 N$ $T_{ssl}^{AB} = N$

$= 1900 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.520

Manufacturer: Rolls-Royce

Application: DH 125-1, Dominie T.1

Composition: - / - / 7 / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 13789 N$ $T_{ssl}^{AB} = N$

$= 3100 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.521

Manufacturer: Rolls-Royce

Application: DH 125-1A/-1B/-2

Composition: - / - / 8 / 1 / - / -

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$

Static Sea Level:

 $T_{ssl} = 13789 N$
 $T_{ssl}^{AB} = N$
 $= 3100 lbf$
 $= lbf$
 $SFC_{ssl} = 2.8 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.99 (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 24 kg/s = 52.9 lb/s$
 $BPR =$
 $OPR = 5.6$
 $FPR =$
 $TET = ^\circ K$

Nb of shafts = 1

 $L = m$
 $= in$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
Viper Mk.522

Manufacturer: Rolls-Royce

Application: HS 125-3/-3A/-3B/-400B/-403B/-600, Dominie CC.1/CC.2/CC.3

Composition: - / - / 8 / 1 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$
 $D = 0.734 m$
 $L = 2.36 m$
 $W_{eng} = 345 kg = 761 lb$
 $= 28.9 in$
 $= 92.9 in$

Static Sea Level:

 $T_{ssl} = 14946 N$
 $T_{ssl}^{AB} = N$
 $= 3360 lbf$
 $= lbf$
 $SFC_{ssl} = 2.83 \cdot 10^{-5} (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1 (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR = 5.6$
 $FPR =$
 $TET = ^\circ K$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
Viper Mk.526

Manufacturer: Piaggio

Application: PD-808ECM/RM/TA/VIP, PD-808

Composition: - / - / 8 / 1 / - / -

Nb of shafts = 1

 $D_{fan} = m = in$
 $D = m$
 $L = m$
 $W_{eng} = kg = lb$
 $= in$
 $= in$

Static Sea Level:

 $T_{ssl} = 14946 N$
 $T_{ssl}^{AB} = N$
 $= 3360 lbf$
 $= lbf$
 $SFC_{ssl} = (kg/s)/N$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $OPR =$
 $FPR =$
 $TET = ^\circ K$

Cruise:

 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Viper Mk.531

Manufacturer: Rolls-Royce

Application: J-1 Jastrebov

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$ $D = 0.836 m$

$W_{eng} = 358 kg = 789 lb$ $= 32.9 in$

Static Sea Level:

$T_{ssl} = 13878 N$ $T_{ssl}^{AB} = N$

$= 3120 lbf$ $= lbf$

$SFC_{ssl} = 2.83 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 5.4

FPR = TET = °K

Nb of shafts = 1

$L = 1.806 m$

$= 71.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.535

Manufacturer: Rolls-Royce

Application: BAC 167 Mk.55, 80, 80A, 82, 82A, 83, 84, 87, 88, 89, 90

Composition: - / - / 8 / 1 / - / -

$D_{fan} = 0.711 m = 28 in$ $D = 0.74 m$

$W_{eng} = 358 kg = 789 lb$ $= 29.1 in$

Static Sea Level:

$T_{ssl} = 14946 N$ $T_{ssl}^{AB} = N$

$= 3360 lbf$ $= lbf$

$SFC_{ssl} = 2.83 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 23.9 kg/s = 52.7 lb/s$

BPR = 0 OPR = 5.5

FPR = TET = °K

Nb of shafts = 1

$L = 1.806 m$

$= 71.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.540

Manufacturer: Rolls-Royce

Application: MB.326GB/H/M

Composition: - / - / 8 / 1 / - / -

$D_{fan} = m = in$ $D = 0.711 m$

$W_{eng} = 358 kg = 789 lb$ $= 28 in$

Static Sea Level:

$T_{ssl} = 14946 N$ $T_{ssl}^{AB} = N$

$= 3360 lbf$ $= lbf$

$SFC_{ssl} = 2.83 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 1.806 m$

$= 71.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.600

Manufacturer: Rolls-Royce

Application:

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 26.3 kg/s = 58 lb/s$

BPR = OPR = 5.8

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.601-22

Manufacturer: Rolls-Royce

Application: HS 125-600B

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = 376 kg = 829 lb$ $= in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 2.69 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.95 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 5.8

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.631

Manufacturer: Rolls-Royce

Application:

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 1.044 m$

$W_{eng} = kg = lb$ $= 41.1 in$

Static Sea Level:

$T_{ssl} = 17659 N$ $T_{ssl}^{AB} = N$

$= 3970 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 1.806 m$

$= 71.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.632-41R

Manufacturer: Rolls-Royce

Application: IAR-93A, J-22A, G-4 Super Galeb

Composition: - / - / 8 / 2 / - / -

$D_{fan} = 0.74 \text{ m} = 29.1 \text{ in}$ $D = 0.747 \text{ m}$

$W_{eng} = 376 \text{ kg} = 829 \text{ lb}$ $= 29.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 17659 \text{ N}$ $T_{ssl}^{AB} = 22241 \text{ N}$

$= 3970 \text{ lbf}$ $= 5000 \text{ lbf}$

$SFC_{ssl} = 2.75 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.97 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 26.3 \text{ kg/s} = 58 \text{ lb/s}$

BPR = OPR = 5.9

FPR = TET = °K

Nb of shafts = 1

$L = 1.806 \text{ m}$

$= 71.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Viper Mk.632-43

Manufacturer: Piaggio

Application: MB.326K/L, MB.339A/PAN/RM, G-4 Super Galeb

Composition: - / - / 8 / 2 / - / -

$D_{fan} = 0.74 \text{ m} = 29.1 \text{ in}$ $D = 0.747 \text{ m}$

$W_{eng} = 376 \text{ kg} = 829 \text{ lb}$ $= 29.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 17659 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3970 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 5.9

FPR = TET = °K

Nb of shafts = 1

$L = 1.806 \text{ m}$

$= 71.1 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Viper Mk.633-41

Manufacturer: Rolls-Royce

Application: IAR-93B, J-22B

Composition: - / - / 8 / 2 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = 0.709 \text{ m}$

$W_{eng} = 553 \text{ kg} = 1219 \text{ lb}$ $= 27.9 \text{ in}$

Static Sea Level:

$T_{ssl} = 17659 \text{ N}$ $T_{ssl}^{AB} = \text{N}$

$= 3970 \text{ lbf}$ $= \text{lbf}$

$SFC_{ssl} = 2.75 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$= 0.97 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 4.44 \text{ m}$

$= 174.8 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

Viper Mk.633-47

Manufacturer: Rolls-Royce

Application: IAR-93B

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.709 m$

$W_{eng} = 553 kg = 1219 lb$ $= 27.9 in$

Static Sea Level:

$T_{ssl} = 17659 N$ $T_{ssl}^{AB} = 22241 N$

$= 3970 lbf$ $= 5000 lbf$

$SFC_{ssl} = 2.75 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.97 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts = 1

$L = 4.44 m$

$= 174.8 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.680

Manufacturer: Rolls-Royce

Application: Trainers

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.737 m$

$W_{eng} = 379 kg = 836 lb$ $= 29 in$

Static Sea Level:

$T_{ssl} = 19394 N$ $T_{ssl}^{AB} = N$

$= 4360 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 27.2 kg/s = 60 lb/s$

BPR = 0

OPR = 6.8

FPR =

TET = °K

Nb of shafts = 1

$L = 1.963 m$

$= 77.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Viper Mk.680-43

Manufacturer: Rolls-Royce

Application: MB.339B/C

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.737 m$

$W_{eng} = 379 kg = 836 lb$ $= 29 in$

Static Sea Level:

$T_{ssl} = 19394 N$ $T_{ssl}^{AB} = N$

$= 4360 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 27.2 kg/s = 60 lb/s$

BPR =

OPR = 6.8

FPR =

TET = °K

Nb of shafts = 1

$L = 1.963 m$

$= 77.3 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

VK-1

Manufacturer: Klimov

Application: MiG-15bis 'Fagot', MiG-17 'Fresco-A', Il-28 'Beagle', Tu-14 'Bosun', S-103, LiM-2

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 26476 \text{ N}$ $T_{ssl}^{AB} = N$

$T_{cr} = N$

$= 5952 \text{ lbf}$ $= lbf$

$= lbf$

$SFC_{ssl} = 2.97 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$SFC_{cr} = \text{(kg/s)/N}$

$= 1.05 \text{ (lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 48.1 \text{ kg/s} = 106 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 4.4

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

VK-1A

Manufacturer: Klimov

Application: MiG-15P/-15bisR/-15Sbis/-15UTI, La-200B (not produced)

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 26387 \text{ N}$ $T_{ssl}^{AB} = 30399 \text{ N}$

$T_{cr} = N$

$= 5932 \text{ lbf}$ $= 6834 \text{ lbf}$

$= lbf$

$SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$

$SFC_{cr} = \text{(kg/s)/N}$

$= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

VK-1F

Manufacturer: Klimov

Application: MiG-17F 'Fresco-C', MiG-17PF 'Fresco-D', Il-28 'Beagle'

Composition: - / - / 1C / 1 / - / -

Nb of shafts = 1

$D_{fan} = m = in$ $D = m$

$L = m$

$W_{eng} = kg = lb$ $= in$

$= in$

Static Sea Level:

Cruise:

$T_{ssl} = 26476 \text{ N}$ $T_{ssl}^{AB} = 33144 \text{ N}$

$T_{cr} = N$

$= 5952 \text{ lbf}$ $= 7451 \text{ lbf}$

$= lbf$

$SFC_{ssl} = 3.25 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 5.67 \cdot 10^{-5} \text{ (kg/s)/N}$

$SFC_{cr} = \text{(kg/s)/N}$

$= 1.15 \text{ (lb/h)/lbf}$ $= 2 \text{ (lb/h)/lbf}$

$= \text{(lb/h)/lbf}$

$\dot{w}_{ssl} = 48.1 \text{ kg/s} = 106 \text{ lb/s}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

BPR = OPR = 4.4

OPR_{cr} =

FPR = TET = °K

$M_{cr} = , h_{cr} = m$

W.1X

Manufacturer: PowerJet

Application: E.28/39

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 3825 N$ $T_{ssl}^{AB} = N$

$= 860 lbf$ $= lbf$

$SFC_{ssl} = 3.2 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.13 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 11.3 kg/s = 24.9 lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

Welland 1

Manufacturer: Rolls-Royce

Application: Meteor I, Meteor III

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 7206 N$ $T_{ssl}^{AB} = N$

$= 1620 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 15.4 kg/s = 34 lb/s$

BPR = OPR = 3.5

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

WJ119-2

Manufacturer: Williams

Application:

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = 0.178 m$

$W_{eng} = kg = lb$ $= 7 in$

Static Sea Level:

$T_{ssl} = 467 N$ $T_{ssl}^{AB} = N$

$= 105 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

WP13

Manufacturer: Liyang - LMC China

Application: J-7III, J-8II 'Finback-B'

Composition: / - / - / - / -

$D_{fan} = m = in$ $D = 0.907 m$

$W_{eng} = 1211 kg = 2670 lb$ $= 35.7 in$

Static Sea Level:

$T_{ssl} = 40207 N$ $T_{ssl}^{AB} = 64721 N$

$= 9039 lbf$ $= 14550 lbf$

$SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.37 \cdot 10^{-5} (kg/s)/N$

$= 0.96 (lb/h)/lbf$ $= 2.25 (lb/h)/lbf$

$\dot{w}_{ssl} = 65.8 kg/s = 145.1 lb/s$

BPR = 0

OPR =

FPR =

TET = °K

Nb of shafts =

$L = 4.6 m$

$= 181.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

WP13A

Manufacturer: Liyang - LMC China

Application:

Composition: / / / / /

$D_{fan} = 0.907 m = 35.7 in$ $D = m$

$W_{eng} = 1201 kg = 2648 lb$ $= in$

Static Sea Level:

$T_{ssl} = 47100 N$ $T_{ssl}^{AB} = 65900 N$

$= 10589 lbf$ $= 14815 lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 65.6 kg/s = 144.6 lb/s$

BPR = 0

OPR =

FPR =

TET = °K

Nb of shafts =

$L = 5.15 m$

$= 202.8 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

WP13A II

Manufacturer: Liyang - LMC China

Application: J-7III, J-8II 'Finback-B'

Composition: / - / - / - / -

$D_{fan} = m = in$ $D = 0.907 m$

$W_{eng} = 1201 kg = 2648 lb$ $= 35.7 in$

Static Sea Level:

$T_{ssl} = 42658 N$ $T_{ssl}^{AB} = 65900 N$

$= 9590 lbf$ $= 14815 lbf$

$SFC_{ssl} = 2.8 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.23 \cdot 10^{-5} (kg/s)/N$

$= 0.99 (lb/h)/lbf$ $= 2.2 (lb/h)/lbf$

$\dot{w}_{ssl} = 65.8 kg/s = 145.1 lb/s$

BPR =

OPR =

FPR =

TET = °K

Nb of shafts =

$L = 5.15 m$

$= 202.8 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

WP13B

Manufacturer: Liyang - LMC China

Application: J-8II 'Finback-B'

Composition: / - / / - / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 47100 \text{ N}$ $T_{ssl}^{AB} = 68636 \text{ N}$

$= 10589 \text{ lbf}$ $= 15430 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 0$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

WP13F

Manufacturer: Liyang - LMC China

Application:

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 44100 \text{ N}$ $T_{ssl}^{AB} = 64700 \text{ N}$

$= 9914 \text{ lbf}$ $= 14545 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR = 0$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

WP5

Manufacturer: Liming - LM China

Application:

Composition: / / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 26476 \text{ N}$ $T_{ssl}^{AB} = N$

$= 5952 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

WP6

Manufacturer: Liming - LM China

Application: J-6, JJ-6, Q-5/-5I/-5IA/-5II, A-5C/K

Composition: - / - / 9 / 2 / - / -

$D_{fan} = 0.668 \text{ m} = 26.3 \text{ in}$ $D = 0.95 \text{ m}$

$W_{eng} = 725 \text{ kg} = 1598 \text{ lb}$ $= 37.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 25497 \text{ N}$ $T_{ssl}^{AB} = 39718 \text{ N}$

$= 5732 \text{ lbf}$ $= 8929 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 46.3 \text{ kg/s} = 102.1 \text{ lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = 5.484 \text{ m}$

$= 215.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

WP6A

Manufacturer: Liming - LM China

Application: Q-51, A-5M

Composition: - / - / 9 / 2 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = 0.95 \text{ m}$

$W_{eng} = 725 \text{ kg} = 1598 \text{ lb}$ $= 37.4 \text{ in}$

Static Sea Level:

$T_{ssl} = 29420 \text{ N}$ $T_{ssl}^{AB} = 36773 \text{ N}$

$= 6614 \text{ lbf}$ $= 8267 \text{ lbf}$

$SFC_{ssl} = 2.78 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = 4.52 \cdot 10^{-5} (\text{kg/s})/\text{N}$
 $= 0.98 (\text{lb/h})/\text{lbf}$ $= 1.6 (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = 46.3 \text{ kg/s} = 102.1 \text{ lb/s}$

BPR = OPR = 7.4

FPR = TET = °K

Nb of shafts = 1

$L = 5.484 \text{ m}$

$= 215.9 \text{ in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

WP6B

Manufacturer: Liming - LM China

Application: J-12

Composition: - / - / 9 / 2 / - / -

$D_{fan} = \text{m} = \text{in}$ $D = \text{m}$

$W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$

Static Sea Level:

$T_{ssl} = 24514 \text{ N}$ $T_{ssl}^{AB} = 39718 \text{ N}$

$= 5511 \text{ lbf}$ $= 8929 \text{ lbf}$

$SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$
 $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$

$\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 1

$L = \text{m}$

$= \text{in}$

Cruise:

$T_{cr} = \text{N}$

$= \text{lbf}$

$SFC_{cr} = (\text{kg/s})/\text{N}$

$= (\text{lb/h})/\text{lbf}$

$\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$

OPR_{cr} =

$M_{cr} = , h_{cr} = \text{m}$

WP7**Manufacturer:** Liming - LM China**Application:** J-7**Composition:** 3 / - / 5 / 1 / - / 1 $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 38246 \text{ N}$ $T_{ssl}^{AB} = 56385 \text{ N}$
 $= 8598 \text{ lbf}$ $= 12676 \text{ lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **WP7A****Manufacturer:** Liming - LM China**Application:** J-8**Composition:** 3 / - / 5 / 1 / - / 1 $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 43139 \text{ N}$ $T_{ssl}^{AB} = 59005 \text{ N}$
 $= 9698 \text{ lbf}$ $= 13265 \text{ lbf}$ $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR =$ $OPR =$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **WP7B****Manufacturer:** Liyang - LMC China**Application:** J-7, JJ-7, J-8I**Composition:** 3 / - / 5 / 1 / - / 1 $D_{fan} = m = in$ $D = 0.826 \text{ m}$ $W_{eng} = 1053 \text{ kg} = 2321 \text{ lb}$ $= 32.5 \text{ in}$ **Static Sea Level:** $T_{ssl} = 43148 \text{ N}$ $T_{ssl}^{AB} = 59819 \text{ N}$
 $= 9700 \text{ lbf}$ $= 13448 \text{ lbf}$ $SFC_{ssl} = 2.86 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.64 \cdot 10^{-5} (kg/s)/N$
 $= 1.01 (lb/h)/lbf$ $= 1.99 (lb/h)/lbf$ $\dot{w}_{ssl} = 64.9 \text{ kg/s} = 143.1 \text{ lb/s}$ $BPR =$ $OPR = 8.1$ $FPR = 2.74$ $TET = ^\circ K$

Nb of shafts = 2

 $L = 4.6 \text{ m}$ $= 181.1 \text{ in}$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

WP7C
Manufacturer: Liyang - LMC China

Application: J-7I/II

Composition: 3 / - / 5 / 1 / - / 1

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$
Static Sea Level:
 $T_{ssl} = 42649 N$
 $= 9588 lbf$
 $SFC_{ssl} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$
 $FPR =$
 $T_{ssl}^{AB} = 60598 N$
 $= 13623 lbf$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $OPR =$
 $TET = ^\circ K$
Nb of shafts = 2
 $L = m$
 $= in$
Cruise:
 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
WP7F
Manufacturer: Liyang - LMC China

Application: J-7E

Composition: 3 / - / 5 / 1 / - / 1

 $D_{fan} = m = in$
 $D = m$
 $W_{eng} = kg = lb$
 $= in$
Static Sea Level:
 $T_{ssl} = 44131 N$
 $= 9921 lbf$
 $SFC_{ssl} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR = 0$
 $FPR =$
 $T_{ssl}^{AB} = 63743 N$
 $= 14330 lbf$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $OPR =$
 $TET = ^\circ K$
Nb of shafts = 2
 $L = m$
 $= in$
Cruise:
 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
WP8
Manufacturer: XAE

Application:
Composition: - / - / 8 / ?? / - / -

 $D_{fan} = m = in$
 $D = 1.4 m$
 $W_{eng} = 3132 kg = 6905 lb$
 $= 55.1 in$
Static Sea Level:
 $T_{ssl} = 93163 N$
 $= 20944 lbf$
 $SFC_{ssl} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{ssl} = 150.1 kg/s = 330.9 lb/s$
 $BPR =$
 $FPR =$
 $T_{ssl}^{AB} = N$
 $= lbf$
 $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$
 $OPR =$
 $TET = ^\circ K$
Nb of shafts = 1
 $L = 5.38 m$
 $= 211.8 in$
Cruise:
 $T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

WR19**Manufacturer:** Williams**Application:** Jet Flying belt**Composition:** 2 / 2B / 1C / 1 / - / 2 $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 1913 N$ $T_{ssl}^{AB} = N$ $= 430 lbf$ $= lbf$ $SFC_{ssl} = 1.98 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= 0.7 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = kg/s = lb/s$ $BPR = 1.1$ $OPR = 8$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **WR2-6****Manufacturer:** Williams**Application:** CL-89**Composition:** - / - / 1C / 1 / - / - $D_{fan} = m = in$ $D = m$ $W_{eng} = kg = lb$ $= in$ **Static Sea Level:** $T_{ssl} = 556 N$ $T_{ssl}^{AB} = N$ $= 125 lbf$ $= lbf$ $SFC_{ssl} = 3.54 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$ $= 1.25 (lb/h)/lbf$ $= (lb/h)/lbf$ $\dot{w}_{ssl} = 0.9 kg/s = 2 lb/s$ $BPR =$ $OPR = 4$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = m$ $= in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$ **WS6****Manufacturer:** Liming - LM China**Application:****Composition:** 3 / / 11 / 2 / - / 2 $D_{fan} = m = in$ $D = 1.37 m$ $W_{eng} = 2100 kg = 4630 lb$ $= 53.9 in$ **Static Sea Level:** $T_{ssl} = 71131 N$ $T_{ssl}^{AB} = 122103 N$ $= 15991 lbf$ $= 27450 lbf$ $SFC_{ssl} = 1.76 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 6.4 \cdot 10^{-5} (kg/s)/N$ $= 0.62 (lb/h)/lbf$ $= 2.26 (lb/h)/lbf$ $\dot{w}_{ssl} = 155.1 kg/s = 341.9 lb/s$ $BPR = 1$ $OPR = 14.4$ $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

 $L = 4.653 m$ $= 183.2 in$ **Cruise:** $T_{cr} = N$ $= lbf$ $SFC_{cr} = (kg/s)/N$ $= (lb/h)/lbf$ $\dot{w}_{cr} = kg/s = lb/s$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = m$

WS6A**Manufacturer:** Liming - LM China**Application:****Composition:** / / / / $D_{fan} = 0.668 \text{ m} = 26.3 \text{ in}$ $D = \text{m}$ $W_{eng} = 725 \text{ kg} = 1598 \text{ lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 36780 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 8268 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = 46.3 \text{ kg/s} = 102.1 \text{ lb/s}$ $BPR = 0$ $OPR =$ $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts =

 $L = 5.483 \text{ m}$ $= 215.9 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **WS9****Manufacturer:** XAE**Application:****Composition:** 5 / - / 12 / 2 / - / 2 $D_{fan} = \text{m} = \text{in}$ $D = \text{m}$ $W_{eng} = \text{kg} = \text{lb}$ $= \text{in}$ **Static Sea Level:** $T_{ssl} = 54490 \text{ N}$ $T_{ssl}^{AB} = 91255 \text{ N}$ $= 12250 \text{ lbf}$ $= 20515 \text{ lbf}$ $SFC_{ssl} = (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR = 0.7$ $OPR = 19.5$ $FPR = 2.7$ $TET = ^\circ\text{K}$

Nb of shafts = 2

 $L = \text{m}$ $= \text{in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$ **XJ30-P-7****Manufacturer:** Pratt & Whitney**Application:****Composition:** - / - / 10 / 1 / - / - $D_{fan} = \text{m} = \text{in}$ $D = 0.483 \text{ m}$ $W_{eng} = 312 \text{ kg} = 688 \text{ lb}$ $= 19 \text{ in}$ **Static Sea Level:** $T_{ssl} = 6939 \text{ N}$ $T_{ssl}^{AB} = \text{N}$ $= 1560 \text{ lbf}$ $= \text{lbf}$ $SFC_{ssl} = 3.31 \cdot 10^{-5} (\text{kg/s})/\text{N}$ $SFC_{ssl}^{AB} = (\text{kg/s})/\text{N}$ $= 1.17 (\text{lb/h})/\text{lbf}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$ $BPR =$ $OPR = 3.5$ $FPR =$ $TET = ^\circ\text{K}$

Nb of shafts = 1

 $L = 2.388 \text{ m}$ $= 94 \text{ in}$ **Cruise:** $T_{cr} = \text{N}$ $= \text{lbf}$ $SFC_{cr} = (\text{kg/s})/\text{N}$ $= (\text{lb/h})/\text{lbf}$ $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$ $OPR_{cr} =$ $M_{cr} = , h_{cr} = \text{m}$

XJ30-P-9

Manufacturer: Pratt & Whitney

Application:

Composition: - / - / 10 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = 312 kg = 688 lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 6939 N$ $T_{ssl}^{AB} = N$

$= 1560 lbf$ $= lbf$

$SFC_{ssl} = 3.31 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.17 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.5

FPR = TET = °K

Nb of shafts = 1

$L = 2.388 m$

$= 94 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ30-WE-1

Manufacturer: Westinghouse

Application: XP-79A/B

Composition: - / - / 6 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = 375 kg = 827 lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 6072 N$ $T_{ssl}^{AB} = N$

$= 1365 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.654 m$

$= 104.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ30-WE-3

Manufacturer: Westinghouse

Application: XB-42A

Composition: - / - / 10 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = 306 kg = 675 lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 7117 N$ $T_{ssl}^{AB} = N$

$= 1600 lbf$ $= lbf$

$SFC_{ssl} = 3.26 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.15 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.5

FPR = TET = °K

Nb of shafts = 1

$L = 2.388 m$

$= 94 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ30-WE-5

Manufacturer: Westinghouse

Application: XB-42A

Composition: - / - / 10 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = 299 kg = 659 lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 7562 N$ $T_{ssl}^{AB} = N$

$= 1700 lbf$ $= lbf$

$SFC_{ssl} = 3.14 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.11 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 2.388 m$

$= 94 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ30-WE-7

Manufacturer: Westinghouse

Application: X-4

Composition: - / - / 10 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = 312 kg = 688 lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 6939 N$ $T_{ssl}^{AB} = N$

$= 1560 lbf$ $= lbf$

$SFC_{ssl} = 3.31 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.17 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.5

FPR = TET = °K

Nb of shafts = 1

$L = 2.388 m$

$= 94 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ30-WE-9

Manufacturer: Westinghouse

Application: X-4

Composition: - / - / 10 / 1 / - / -

$D_{fan} = m = in$ $D = 0.483 m$

$W_{eng} = 312 kg = 688 lb$ $= 19 in$

Static Sea Level:

$T_{ssl} = 6939 N$ $T_{ssl}^{AB} = N$

$= 1560 lbf$ $= lbf$

$SFC_{ssl} = 3.31 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.17 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.5

FPR = TET = °K

Nb of shafts = 1

$L = 2.388 m$

$= 94 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ33-GE-1

Manufacturer: GE : General Electric

Application: Prototype

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 805 kg = 1775 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ33-GE-3

Manufacturer: GE : General Electric

Application:

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 805 kg = 1775 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ33-GE-5

Manufacturer: GE : General Electric

Application: XP-81, XP-83

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 805 kg = 1775 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ33-GE-7

Manufacturer: GE : General Electric

Application:

Composition: - / - / 1C / 1 / - / -

$D_{fan} = m = in$ $D = 1.283 m$

$W_{eng} = 805 kg = 1775 lb$ $= 50.5 in$

Static Sea Level:

$T_{ssl} = 17014 N$ $T_{ssl}^{AB} = N$

$= 3825 lbf$ $= lbf$

$SFC_{ssl} = 3.46 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.22 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 2.614 m$

$= 102.9 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ34-WE-1

Manufacturer: Westinghouse

Application: Prototype

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$

$W_{eng} = 528 kg = 1164 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$

$= 3000 lbf$ $= lbf$

$SFC_{ssl} = 2.97 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.05 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 22.7 kg/s = 50 lb/s$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

$L = 3.028 m$

$= 119.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ34-WE-11

Manufacturer: Westinghouse

Application: XF-90

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$

$W_{eng} = 707 kg = 1559 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 12989 N$ $T_{ssl}^{AB} = 18238 N$

$= 2920 lbf$ $= 4100 lbf$

$SFC_{ssl} = 3.29 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.51 \cdot 10^{-5} (kg/s)/N$ $SFC_{cr} = (kg/s)/N$
 $= 1.16 (lb/h)/lbf$ $= 2.65 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

$L = 6.121 m$

$= 241 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ34-WE-13

Manufacturer: Westinghouse

Application: XF-88

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$

$W_{eng} = 552 kg = 1217 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 14012 N$ $T_{ssl}^{AB} = N$

$= 3150 lbf$ $= lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

$L = 3.028 m$

$= 119.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ34-WE-15

Manufacturer: Westinghouse

Application: XF-88A, XF-90A

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$

$W_{eng} = 552 kg = 1217 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 14012 N$ $T_{ssl}^{AB} = 21463 N$

$= 3150 lbf$ $= 4825 lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 3.8

FPR = TET = °K

Nb of shafts = 1

$L = 3.028 m$

$= 119.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ34-WE-17

Manufacturer: Westinghouse

Application: X-3

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$

$W_{eng} = 770 kg = 1698 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 14990 N$ $T_{ssl}^{AB} = 21796 N$

$= 3370 lbf$ $= 4900 lbf$

$SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.37 \cdot 10^{-5} (kg/s)/N$

$= 1.08 (lb/h)/lbf$ $= 2.6 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 4.1

FPR = TET = °K

Nb of shafts = 1

$L = 4.496 m$

$= 177 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ34-WE-3

Manufacturer: Westinghouse

Application:

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$

$W_{eng} = 522 kg = 1151 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$

$= 3000 lbf$ $= lbf$

$SFC_{ssl} = 2.97 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.05 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 22.7 kg/s = 50 lb/s$

$BPR =$ $OPR = 3.8$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 3.028 m$

$= 119.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

XJ34-WE-4

Manufacturer: Westinghouse

Application:

Composition: - / - / 10 / 2 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = 495 kg = 1091 lb$ $= in$

Static Sea Level:

$T_{ssl} = 10676 N$ $T_{ssl}^{AB} = N$

$= 2400 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR = 3.5$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

XJ34-WE-5

Manufacturer: Westinghouse

Application:

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$

$W_{eng} = 532 kg = 1173 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$

$= 3000 lbf$ $= lbf$

$SFC_{ssl} = 2.97 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.05 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 22.7 kg/s = 50 lb/s$

$BPR =$ $OPR = 3.8$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = 3.028 m$

$= 119.2 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

XJ34-WE-7

Manufacturer: Westinghouse

Application: XP-85, XF-87

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$
 $W_{eng} = 537 kg = 1184 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$
 $= 3000 lbf$ $= lbf$
 $SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 3.8$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 3.028 m$
 $= 119.2 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

XJ34-WE-9

Manufacturer: Westinghouse

Application:

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 0.65 m$
 $W_{eng} = 537 kg = 1184 lb$ $= 25.6 in$

Static Sea Level:

$T_{ssl} = 13345 N$ $T_{ssl}^{AB} = N$
 $= 3000 lbf$ $= lbf$
 $SFC_{ssl} = 3.06 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.08 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 3.8$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 3.028 m$
 $= 119.2 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

XJ35-A-23

Manufacturer: Allison

Application:

Composition: - / - / 16 / 2 / - / -

$D_{fan} = m = in$ $D = 0.953 m$
 $W_{eng} = 1583 kg = 3490 lb$ $= 37.5 in$

Static Sea Level:

$T_{ssl} = 43148 N$ $T_{ssl}^{AB} = N$
 $= 9700 lbf$ $= lbf$
 $SFC_{ssl} = 2.72 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.96 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 8.8$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 3.962 m$
 $= 156 in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

XJ35-GE-1

Manufacturer: GE : General Electric

Application: Prototype

Composition: - / - / 11 / 1 / - / -

$D_{fan} = m = in$ $D = 1.016 m$

$W_{eng} = 1089 kg = 2401 lb$ $= 40 in$

Static Sea Level:

$T_{ssl} = 16681 N$ $T_{ssl}^{AB} = N$

$= 3750 lbf$ $= lbf$

$SFC_{ssl} = 3.17 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 1.12 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = 34 kg/s = 75 lb/s$

BPR = OPR = 4

FPR = TET = °K

Nb of shafts = 1

$L = 4.496 m$

$= 177 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ46-WE-1

Manufacturer: Westinghouse

Application: X-10

Composition: - / - / 12 / 2 / - / -

$D_{fan} = m = in$ $D = 0.737 m$

$W_{eng} = 925 kg = 2039 lb$ $= 29 in$

Static Sea Level:

$T_{ssl} = 18149 N$ $T_{ssl}^{AB} = 27134 N$

$= 4080 lbf$ $= 6100 lbf$

$SFC_{ssl} = 2.86 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$

$= 1.01 (lb/h)/lbf$ $= 2.5 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 5.2

FPR = TET = °K

Nb of shafts = 1

$L = 5.032 m$

$= 198.1 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ46-WE-2

Manufacturer: Westinghouse

Application: XF2Y-1, YF2Y-1, XF-90 (not produced)

Composition: - / - / 12 / 2 / - / -

$D_{fan} = m = in$ $D = 0.737 m$

$W_{eng} = 845 kg = 1863 lb$ $= 29 in$

Static Sea Level:

$T_{ssl} = 18149 N$ $T_{ssl}^{AB} = 27134 N$

$= 4080 lbf$ $= 6100 lbf$

$SFC_{ssl} = 2.86 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} (kg/s)/N$

$= 1.01 (lb/h)/lbf$ $= 2.5 (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 5.2

FPR = TET = °K

Nb of shafts = 1

$L = 4.869 m$

$= 191.7 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ47-GE-5
Manufacturer: GE : General Electric

Application:
Composition: - / - / 12 / 1 / - / -

 $D_{fan} = m = in$ $D = 1.041 \text{ m}$
 $W_{eng} = 1383 \text{ kg} = 3049 \text{ lb}$ $= 41 \text{ in}$
Static Sea Level:
 $T_{ssl} = 22241 \text{ N}$ $T_{ssl}^{AB} = 29358 \text{ N}$
 $= 5000 \text{ lbf}$ $= 6600 \text{ lbf}$
 $SFC_{ssl} = 3.4 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 1.2 \text{ (lb/h)/lbf}$ $= 2.5 \text{ (lb/h)/lbf}$
 $\dot{w}_{ssl} = 40.8 \text{ kg/s} = 89.9 \text{ lb/s}$
 $BPR =$ $OPR = 4.3$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = 6.198 \text{ m}$
 $= 244 \text{ in}$
Cruise:
 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
XJ48-P-1
Manufacturer: Pratt & Whitney

Application:
Composition: - / - / 1C / 1 / - / -

 $D_{fan} = m = in$ $D = 1.27 \text{ m}$
 $W_{eng} = 932 \text{ kg} = 2055 \text{ lb}$ $= 50 \text{ in}$
Static Sea Level:
 $T_{ssl} = 27801 \text{ N}$ $T_{ssl}^{AB} = 35586 \text{ N}$
 $= 6250 \text{ lbf}$ $= 8000 \text{ lbf}$
 $SFC_{ssl} = 3.29 \cdot 10^{-5} \text{ (kg/s)/N}$ $SFC_{ssl}^{AB} = 7.08 \cdot 10^{-5} \text{ (kg/s)/N}$
 $= 1.16 \text{ (lb/h)/lbf}$ $= 2.5 \text{ (lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR = 4.4$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1

 $L = 5.131 \text{ m}$
 $= 202 \text{ in}$
Cruise:
 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$
XJ52-P-1
Manufacturer: Pratt & Whitney

Application: Prototype

Composition: - / 5 / 7 / 1 / - / 1

 $D_{fan} = m = in$ $D = m$
 $W_{eng} = \text{kg} = \text{lb}$ $= in$
Static Sea Level:
 $T_{ssl} = 33362 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 7500 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = \text{(kg/s)/N}$ $SFC_{ssl}^{AB} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$ $= \text{(lb/h)/lbf}$
 $\dot{w}_{ssl} = \text{kg/s} = \text{lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2

 $L = m$
 $= in$
Cruise:
 $T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = \text{(kg/s)/N}$
 $= \text{(lb/h)/lbf}$
 $\dot{w}_{cr} = \text{kg/s} = \text{lb/s}$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

XJ53-GE-1

Manufacturer: GE : General Electric

Application: X-6A (not produced)

Composition: / / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 93412 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 21000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

XJ55-FF-1

Manufacturer: Frederic-Flader

Application: XQ-2 (not produced)

Composition: - / - / 1 / 1 / - / 1

$D_{fan} = m = in$ $D = 0.432 \text{ m}$
 $W_{eng} = 136 \text{ kg} = 300 \text{ lb}$ $= 17 \text{ in}$

Static Sea Level:

$T_{ssl} = 3425 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 770 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = 4.65 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 1.64 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 2.7$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 2.106 \text{ m}$
 $= 82.9 \text{ in}$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

XJ57-P-1

Manufacturer: Pratt & Whitney

Application: XA3D-1, YA3D-1, A3D-1 (A-3A)

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.041 \text{ m}$
 $W_{eng} = 1991 \text{ kg} = 4389 \text{ lb}$ $= 41 \text{ in}$

Static Sea Level:

$T_{ssl} = 40034 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 9000 \text{ lbf}$ $= lbf$
 $SFC_{ssl} = 2.21 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= 0.78 (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR = 10$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 2
 $L = 4.661 \text{ m}$
 $= 183.5 \text{ in}$

Cruise:

$T_{cr} = N$
 $= lbf$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

XJ57-P-1W

Manufacturer: Pratt & Whitney

Application: XB-52, YB-52

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 40034 N$ $T_{ssl}^{AB} = N$

$= 9000 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

XJ99-RA-1

Manufacturer: Rolls-Royce Allison

Application: AVS (not produced)

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 38655 N$ $T_{ssl}^{AB} = N$

$= 8690 lbf$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR =

FPR = TET = °K

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

YJ57-P-3

Manufacturer: Pratt & Whitney

Application: XB-52, YB-60

Composition: - / 9 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = 1.041 m$

$W_{eng} = 1991 kg = 4389 lb$ $= 41 in$

Static Sea Level:

$T_{ssl} = 38699 N$ $T_{ssl}^{AB} = N$

$= 8700 lbf$ $= lbf$

$SFC_{ssl} = 2.28 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= 0.8 (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

BPR = OPR = 11.6

FPR = TET = °K

Nb of shafts = 2

$L = 4.661 m$

$= 183.5 in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

OPR_{cr} =

$M_{cr} = , h_{cr} = m$

YJ71-A-5

Manufacturer: Allison

Application: B-47C (not produced)

Composition: / / / /

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 45372 \text{ N}$ $T_{ssl}^{AB} = N$

$= 10200 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts =

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

YJ75-P-9

Manufacturer: Pratt & Whitney

Application: F-106A/B, YF-107A (F-100B)

Composition: - / 8 / 7 / 1 / - / 2

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 76509 \text{ N}$ $T_{ssl}^{AB} = 108981 \text{ N}$

$= 17200 \text{ lbf}$ $= 24500 \text{ lbf}$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 2

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

YJ79-GE-13

Manufacturer: GE : General Electric

Application: X-21A

Composition: - / - / 17 / 3 / - / -

$D_{fan} = m = in$ $D = m$

$W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 42703 \text{ N}$ $T_{ssl}^{AB} = N$

$= 9600 \text{ lbf}$ $= lbf$

$SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$

$= (lb/h)/lbf$ $= (lb/h)/lbf$

$\dot{w}_{ssl} = kg/s = lb/s$

$BPR =$ $OPR =$

$FPR =$ $TET = ^\circ K$

Nb of shafts = 1

$L = m$

$= in$

Cruise:

$T_{cr} = N$

$= lbf$

$SFC_{cr} = (kg/s)/N$

$= (lb/h)/lbf$

$\dot{w}_{cr} = kg/s = lb/s$

$OPR_{cr} =$

$M_{cr} = , h_{cr} = m$

YJ83-R-3

Manufacturer: Fairchild

Application: XSM-73

Composition: / / / /

$D_{fan} = m = in$ $D = m$
 $W_{eng} = kg = lb$ $= in$

Static Sea Level:

$T_{ssl} = 10898 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 2450 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts =
 $L = m$
 $= in$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

YJ85-GE-19

Manufacturer: GE : General Electric

Application: XV-4B, X-14A/B

Composition: - / - / 8 / 2 / - / -

$D_{fan} = m = in$ $D = 0.45 \text{ m}$
 $W_{eng} = 176 \text{ kg} = 388 \text{ lb}$ $= 17.7 \text{ in}$

Static Sea Level:

$T_{ssl} = 13411 \text{ N}$ $T_{ssl}^{AB} = N$
 $= 3015 \text{ lbf}$ $= \text{lbf}$
 $SFC_{ssl} = (kg/s)/N$ $SFC_{ssl}^{AB} = (kg/s)/N$
 $= (lb/h)/lbf$ $= (lb/h)/lbf$
 $\dot{w}_{ssl} = kg/s = lb/s$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 1.029 \text{ m}$
 $= 40.5 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

YJ93-GE-3

Manufacturer: GE : General Electric

Application: NB-58A, XB-70A, XF-108A (not produced)

Composition: - / - / 11 / 2 / - / -

$D_{fan} = m = in$ $D = 1.397 \text{ m}$
 $W_{eng} = 2359 \text{ kg} = 5201 \text{ lb}$ $= 55 \text{ in}$

Static Sea Level:

$T_{ssl} = 97860 \text{ N}$ $T_{ssl}^{AB} = 137894 \text{ N}$
 $= 22000 \text{ lbf}$ $= 31000 \text{ lbf}$
 $SFC_{ssl} = 1.98 \cdot 10^{-5} (kg/s)/N$ $SFC_{ssl}^{AB} = 5.1 \cdot 10^{-5} (kg/s)/N$
 $= 0.7 (lb/h)/lbf$ $= 1.8 (lb/h)/lbf$
 $\dot{w}_{ssl} = 124.7 \text{ kg/s} = 274.9 \text{ lb/s}$
 $BPR =$ $OPR =$
 $FPR =$ $TET = ^\circ K$

Nb of shafts = 1
 $L = 5.969 \text{ m}$
 $= 235 \text{ in}$

Cruise:

$T_{cr} = N$
 $= \text{lbf}$
 $SFC_{cr} = (kg/s)/N$
 $= (lb/h)/lbf$
 $\dot{w}_{cr} = kg/s = lb/s$
 $OPR_{cr} =$
 $M_{cr} = , h_{cr} = m$

Chapter 3

Engines listed in order of thrust

Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
TJ-50	245	3.97	6			
TJ60	267	3.51	4			
TJ80	320	3.51	4			
TJ75	334	3.51	4			
WJ119-2	467					
WR2-6	556	3.54			4	
F121-WR-100	667		19			
S.1	783					
TRS 18-046	1001	3.34	37		3.7	
J400-WR-104	1068	3.4	23			
J400-WR-404	1068	3.4	23			
TRS 18-1	1157	3.34	38		4.7	
J32-WE-5	1223					
S.2	1272					
KJ12	1468		40			
TJ400	1793	2.55	62			
WR19	1913	1.98		1.1	8	
TJM3	1962	3.31	46		5.6	
J104-AD-100	2157	3.51	19			
FJX-1	2402					
F107-WR-400	2669					
F107-WR-101	2825	1.94	66	1	13.8	

... to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl} N	$10^3 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
TJM4	2842	3.17	56		6.7	
J402-CA-700	2847				5.5	
J402-CA-100-2	3025					
J402-CA-100-9B	3025					
J402-CA-400	3025				5.6	
J402-CA-401	3025				5.6	
EJ22-1	3114		39			
F107-WR-402	3114					
F415-WR-400	3114					
F415-WR-402	3114					
FJX-2	3114		39			
F112-WR-100	3256		73			
MC-750	3336					
TRI 40-4	3336	3.34	44		6	
XJ55-FF-1	3425	4.65	136		2.7	
TRI 60-1	3501	3.37	49		3.7	
TRI 60-2	3701	3.57	49		3.8	
W.1X	3825	3.2				
Marbore 2	3923					
Marbore 2A	3923					
Marbore 2C	3923					
Marbore 2F	3923					
Arbizon 3	3924		115	0	5.5	
J69-T-3	3928					
J403-MT-400	4003	3.65	53		3.9	
TRI 60-3	4005		61		3.9	
Arbizon 3B2	4035				5.9	
J69-T-7	4092					
J69-T-9	4092					
Arbizon 3D	4164				5.9	
TRI 60-5	4404	3.54	53		4.1	
S.3A	4413					
S.3B	4413	4.53			2.8	
Adder	4448					
F121-WR-110	4448					
J44-R-1	4448					
J69-T-17	4448					
TF1000	4448	1.13	129			
J69-T-25	4559	3.14	165		3.8	1103
Marbore 6	4706					
Marbore 6F	4706	3.14			3.8	

... to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
Marbore 6C	4715	3.14			3.8	
109-001	4902					
PW610F	4946					
J69-T-27	5115					
FJ33-1	5338		136			
FJ33-4	5338		136	3.4		
TRI 60-20	5338	3.26	64		6.3	
TRI 60-30	5338	2.97	61		6.3	
TF1200	5729	1.16	129			
S.6	5787					
Marbore 8	5872	3.26				
F109-GA-100	5916	1.11	199		20.7	
TFE109-1	5916	1.11				
PW615F	6005					
J30-WE-19	6072					
J30-WE-19A	6072					
XJ30-WE-1	6072		375		3.1	
TF1400	6227	1.16	136			
F121-WR-115	6672					
FJ44-1C	6672	1.3	203	3.4	10.3	
RM15	6672	1.3		3.4	10.3	
TF1500	6672	1.16	136			
J31-GE-5	6895	3.54	392		4.5	
J31-GE-7	6895	3.54	392		4.5	
XJ30-P-7	6939	3.31	312		3.5	
XJ30-P-9	6939	3.31	312		3.5	
XJ30-WE-7	6939	3.31	312		3.5	
XJ30-WE-9	6939	3.31	312		3.5	
J30-WE-20	7117	3.26			3.8	
XJ30-WE-3	7117	3.26	306		3.5	
J31-GE-1	7162	3.48	392		4.5	
J31-GE-3	7162	3.48	392		4.5	
Welland 1	7206	3.17			3.5	
Aubisque 1A	7273	1.7		2	6.9	
RM9A	7273	1.7		2	6.9	
Viper ASV.5	7295	3.09			3.5	
Viper ASV.8 Mk.101	7295					
Astafan 2	7495	1.08		1	8.5	
J69-T-29	7562	3.06	154		5.5	
XJ30-WE-5	7562	3.14	299		4	
HO-10	7651					

... to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl} N	$10^3 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
109-003A	7784	3.97			3.1	
Viper ASV.8 Mk.102	7784				4	
Viper ASV.8 Mk.104	7784					
RD-20	7829					
RD-20F	7829					
SO-1	7847	2.95			4.8	
Bastafan	7851					
F2/1	8007					
J69-T-406	8185	3.14	163		5.5	
J69-T-41	8185				5.5	
RM9B	8229	1.7		2	6.9	
109-004B-0	8238					
Astafan 3	8452					
FJ44	8452	1.3	202	3.28	12.8	1291
FJ44-1A	8452	1.29	203	3.28	12.8	
Viper ASV.9 Mk.103	8452					
J69-T-41A	8541	3.09	159		6	
M-701S-50	8718					
M-701VC-150	8718					
FJ44-1AP	8740		209	2.58		
109-004B-1	8825					
RD-10	8825					
R127-300	8830					
Derwent RB.37 Mk.1	8896	3.33			4	
J85-GE-1	9341					
JT15D-1	9786	1.53	233	3.3		
JT15D-1A	9786	1.53	235	3.3		
JT15D-1B	9786	1.53	235	3.3	10	
Orpheus BOr.3	9786					
RD-10A	9786					
FJ44-2A	10231					
Larzac 49-01	10231	1.73		1.4	9	
109-004D	10298					
R-19-300	10298					
RB.108	10409					
FJ44-2C	10676					
J85-GE-12	10676					
XJ34-WE-4	10676		495		3.5	
Astafan 4	10738					
Gabizo	10765		364			
RD-10F	10765					

... to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
SO-3W	10787					
SO-3	10790		321	0		
J85-GE-3	10898					
J85-GE-7	10898	2.75			6.5	
YJ83-R-3	10898					
109-007	11121	2.31			8	
JT15D-4	11121	1.59	253	2.6		
JT15D-4B	11121	1.59	258	2.6		
JT15D-4C	11121	1.59	261	2.6		
JT15D-4D	11121	1.59	254	2.6		
PW625F	11121					
Viper ASV.11 Mk.200	11121	3.03			4.3	
Viper ASV.11 Mk.201	11121				4.3	
Viper ASV.11 Mk.202	11121	2.95			4.4	
Viper ASV.11 Mk.22-1	11121		281			
Viper ASV.11 Mk.22-6	11121					
Viper ASV.11 Mk.22-8	11121					
J69-T-39	11209	2.72			6.5	
J3-IHI-3	11788					
J85-GE-5	11921	2.92	265		6.7	1167
J85-GE-5A	11921				6.5	
Goblin DGu.1	12010					
J100-CA-100	12010	3.06	191		6.3	
Viper ASV.11 Mk.203	12010					
J85-GE-13	12099	3.57	271		6.5	
J85-GE-13A	12099				6.5	
ALF301	12144	1.25		5.6	9	
PW530A	12224		279	3.7	13.3	
RB.145	12233		207			
FJ44-3A	12540			2.2		
CJ610-1	12677	2.8	181			
CJ610-4	12677	2.8	176			
J85-CAN-40	12677	2.75			6.8	
J85-GE-17	12677	2.69	181		6.5	1167
J85-GE-17A	12677	2.69			6.9	
J85-GE-17B	12677	2.69			6.5	
J85-GE-17C	12677	2.69			6.5	
J85-GE-2	12677					
109-011	12749					
JT15D-5A	12900	1.56	287	2	12.6	
JT15D-5B	12900	1.56				

...to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
XJ34-WE-11	12989	3.29	707		3.8	
PW530	13000	1.24	275	4		
J85-CAN-15	13011	2.61			7	
CJ610-5	13122	2.78	182		6.8	
CJ610-6	13122	2.78	178		6.8	
CJ610-8	13122		185			
CJ610-8A	13122		185			
J85-GE-4	13122	2.78	183		6.5	
J85-GE-J4	13122					
J85-GE-LF1	13122					
Larzac 04-C6	13200	2.03	332	1.13	10.5	1403
JT12A	13342		203	0	6.5	
J34-WE-22	13345	3.06	537		3.8	
J36-AC-1	13345					
J60-P-3	13345	2.72	203		6.5	1144
J60-P-5	13345	2.72	203		6.5	
J60-P-6	13345	2.72	225		6.5	
JT12A-3	13345	2.72	205			
JT12A-5	13345		205			
JT12A-6	13345	2.72	205			
JT12A-6A	13345	2.72	205			
RM1	13345					
TR-1	13345					
XJ34-WE-1	13345	2.97	528		3.8	
XJ34-WE-3	13345	2.97	522		3.8	
XJ34-WE-5	13345	2.97	532		3.8	
XJ34-WE-7	13345	3.06	537		3.8	
XJ34-WE-9	13345	3.06	537		3.8	
YJ85-GE-19	13411		176			
JT15D-5	13545	1.59	287	3.3	12.6	1288
JT15D-5D	13545	1.56	284	2	13.1	
J3-IHI-7C	13700	2.83			4.5	
CJ610-9	13789	2.83	189		6.8	
Goblin DGu.2	13789					
R123-300	13789			6		
Viper Mk.520	13789					
Viper Mk.521	13789	2.8			5.6	
Viper Mk.531	13878	2.83	358		5.4	
J34-WE-30	14012					
J34-WE-30A	14012					
XJ34-WE-13	14012	3.06	552		3.8	

... to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl} N	$10^3 SFC_{ssl}$ $(kg/s)/N$	W_{eng} kg	BPR -	OPR -	TET °K
XJ34-WE-15	14012	3.06	552		3.8	
Larzac 04-C20	14123	2.15	333	1.04	11.1	1433
Larzac 04-R20	14123	2.1	302	1.04	11.1	
JT15D-5C	14190	1.56	302	2	13.5	
J34-IHI-34	14457					
J34-WE-34	14457					
Orpheus BOr.100 (pre-prod)	14612					
AI-25	14679	1.62	320	2.1	8	
J60-P-4	14679	2.82	212			
J60-P-9	14679	2.72			6.5	
JT12A-8	14679	2.82	212		6.7	
JT12A-8A	14679	2.82	212		6.7	
RM11	14679	2.82			6.7	
RM1A	14679					
K-15	14710	2.85	320	0	5.3	
Goblin DGu.3	14901					
Viper Mk.522	14946	2.83	345		5.6	
Viper Mk.526	14946					
Viper Mk.535	14946	2.83	358	0	5.5	
Viper Mk.540	14946	2.83	358			
PW535A	14950			2.55		
J34-WE-32	14990	3.06	770		4.1	
XJ34-WE-17	14990	3.06	770		4.1	
FJ44-4A	15120					
PW535B	15120			2.55		
J34-WE-36	15124					
J34-WE-36A	15124					
J34-WE-42	15124					
J34-WE-46	15124					
J34-WE-48	15124					
Viper 20F20	15156		270	0	2.6	1135
J3-IHI-8	15191					
Derwent RB.37 Mk.8	15444					
TFE731-1	15549		272	2.7	19	1285
TFE731-2	15569	1.43	283	2.67	17.7	
TFE731-2-25	15569		337	2.66		
TFE731-2-2B	15569	1.43	337	2.66	13	
TFE731-2-2N	15569		337	2.56		
TFE731-20	15569	1.25	401	3.1	21	
TFE731-20AR	15569		406	3.1		
TFE731-20BR	15569		406	3.1		

... to be continued ...

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
RD-500	15702					
Derwent RB.37 5/17	16014					
Derwent RB.37 Mk.9	16014					
J85-GE-21	16014	3.51	290		8.3	1250
J85-GE-21A	16014				8.1	
J85-J1	16014	2.69			8.3	
Larzac 04-V3	16178					
TFE731-3-100S	16236		349	2.8	14.6	
TFE731-3A-2B	16236	1.46	352	2.8	14.6	
TFE731-3A-300G	16236		352	2.8	14.6	
TFE731-3B-100	16236	1.44	340	2.8	14.4	
F3-IHL-30	16369	1.98	208	0.9	11	
F3-IHL-30	16370		340	0.9		
TFE731-3	16458	1.45	342	2.8	14.6	
TFE731-3-1D	16458		342	2.8	14.6	
TFE731-3-1G	16458		342	2.8	14.6	
TFE731-3-1H	16458	1.45	342	2.8	14.6	
RD-1700	16672			0.78		
Atar	16681				4.2	
J35-A-11	16681	3.17	1114		4	
J35-A-13	16681	3.17	1114		4	
J35-A-13A	16681	3.17	1114		4	
J35-A-13B	16681	3.17	1114		4	
J35-A-13C	16681	3.17	1114		4	
J35-A-15	16681	3.17	1089		4	
J35-A-15C	16681	3.17	1089		4	
J35-A-2	16681					
J35-A-3	16681					
J35-A-5	16681	3.17	1089		4	
J35-A-9	16681	3.17	1114		4	
J35-C-3	16681	3.17	1089		4	
J35-GE-2	16681					
J35-GE-7	16681	3.17	1089		4	
J35-GE-9	16681	3.17	1114		4	
Viper Mk.600	16681	2.69			5.8	
Viper Mk.601-22	16681	2.69	376		5.8	
XJ33-GE-1	16681	3.46	805		4.1	
XJ33-GE-3	16681	3.46	805		4.1	
XJ33-GE-5	16681	3.46	805		4.1	
XJ35-GE-1	16681	3.17	1089		4	
PW545A	16832		370	4.12	15.7	993

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Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
AI-25TL	16868	1.63	350	2	9.5	
AI-25TLK	16868	1.63	350			
J34-WE-38	16903					
J33-A-13	17014	3.46	850		4.1	
J33-A-17	17014	3.46	850		4.1	
J33-A-17A	17014	3.46	850		4.1	
J33-A-21	17014	3.46	839		4.1	
J33-A-9	17014	3.46	805		4.1	
J33-A-9A	17014	3.46	805		4.1	
J33-A-9B	17014	3.46	853		4.1	
J33-GE-11	17014	3.46	805		4.1	
J33-GE-11A	17014	3.46	805		4.1	
J33-GE-11B	17014	3.46	807		4.1	
J33-GE-15	17014	3.46	805		4.1	
XJ33-GE-7	17014	3.46	805		4.1	
AI-25A	17126			2.1		
D-18A	17650	2.1	380	0.7	8	
Viper Mk.631	17659					
Viper Mk.632-41R	17659	2.75	376		5.9	
Viper Mk.632-43	17659		376		5.9	
Viper Mk.633-41	17659	2.75	553			
Viper Mk.633-47	17659	2.75	553			
PW545B	17750		377	3.8	42	1013
J33-A-6	17793					
J35-A-4	17793					
Orpheus BOr.805	17793				4.4	
ATF3	18015	1.25		3	17	
F104-GA-100	18015	1.25		3	17	
J46-WE-3	18149					
TFE731-4	18149	1.46	373	2.4	14.8	
TFE731-4-1T	18149		372	2.4		
XJ46-WE-1	18149	2.86	925		5.2	
XJ46-WE-2	18149	2.86	845		5.2	
PW545C	18320		377	3.8	42	1013
CF700-2C	18349	1.85	329	1.9	6.9	
TF37-GE-1	18682	1.85	306	1.9	6.9	
Orpheus BOr.100-04	18816					
CF700-2D	18905	1.85	334	1.9	6.2	
TFE731-40	18905	1.29	401	2.9	22	
TFE731-40R	18905		406	2.9		
TFE731-40R-200G	18905	1.29	406	2.9	22	

...to be continued ...

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
CF700-2B	19130		334	1.9	6.8	
TFE731-5-1J	19145	1.37	386	3.65	14.4	
CF700-2D2	19194	1.82	348	1.9	6.8	
Viper Mk.680	19394		379	0	6.8	
Viper Mk.680-43	19394		379		6.8	
Ghost 50	19572					
RB.162-4D	19572		125			
RB.162-1	19612		125		4.3	
TFE731-40AR-200G	19661		406	2.9		
TFE731-5	20000	1.33	401	3.15	19.4	1378
J46-WE-4	20017					
Orpheus BOr.701	20017					
TFE731-5AR	20017	1.33	401	3.65	14.6	
Orpheus BOr.101	20106					
J33-A-10	20462	3.18			4.4	953
J33-A-18A	20462					
J33-A-19	20462	3.26	810		4.5	
J33-A-23	20462	3.23	814		4.5	
J33-A-31	20462	3.2	797		4.5	
J33-A-33	20462	3.26	1084		4	
J33-A-33A	20462	3.26	1084		4	
J33-A-35	20462	3.23	814		4	
J33-A-37	20462					
J33-A-8	20462					
J46-WE-8	20462					
J46-WE-8A	20462					
Nene RB.41-1	20462	2.97			4	
PW305A	20813	1.1	450	4.3	15.5	
Orpheus BOr.701-01	20907					
RB.162-4	20907		125		4.3	
TFE731-5BR	21129	1.33	408	3.5	15.1	
TFE731-5BR-1C	21129		408	3.2		
AM-5A	21574					
Atar 101A-0	21574	3.25	880		4.2	1083
Ghost 103	21574					
Ghost 48	21574	2.89	912		4.3	1073
J47-GE-1	21574	3.12	1123		4.3	
J47-GE-3	21574	3.12	1120		4.3	
Orpheus BOr.703	21574					
RD-35	21574	1.73		1.41	14.7	
DV-2	21583	1.69	450	1.46	13.5	1463

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
J35-A-17	21796	3.06	1025		4.7	
J35-A-17A	21796	3.06	1025		4.7	
J35-A-17B	21796	3.06	1025		4.7	
J35-A-17C	21796	3.06	1025		4.7	
J35-A-17D	21796	3.06	1025		4.7	
J35-A-19	21796	3.06	1002		4.7	
Ghost 104	22019					
GE1	22241	1.98			11	
Ghost 50 Mk.1	22241					
J42-P-6	22241	3.09	778		4.3	1014
J42-P-8	22241	3.09	778		4.3	1014
J47-GE-7	22241	3.2	1145		4.3	
J47-GE-9	22241	3.2			4.3	
J48-P-4	22241					
Nene Mk.102	22241	3.09	753		4	1098
Nene RB.41-2	22241					
Orpheus BOr.803	22241	3.06				
Orpheus BOr.803-02	22241	3.06				
RM2A	22241					
RM2B	22241					
TFE731-60	22241	1.15	448	3.9	22	
XJ47-GE-5	22241	3.4	1383		4.3	
Ghost 50 Mk.2	22330					
Ghost 101	22508	2.89			4.5	
J35-A-21A	22686	3.14	1195		4.7	
Nene RB.41-10	22686					
Nene RB.41-3 Mk.101	22686					
Adour RT.172 Mk.102	22730	2.1	704		9.6	
Adour RT.172 Mk.104	22730		713			
Atar 101C	22908					
J35-A-21	22908	3.14	1195		4.7	
ATF3-6	23130	1.47	510	2.9	21	1449
Adour Mk.851	23131		568			
Adour RT.172 Mk.151	23131		544	0.8	11	
ATF3-6A	23131		510	2.8	21.3	
F405-RR-400	23131		568			
J47-GE-11	23131	3.2	1123		4.5	
J47-GE-13	23131	3.17	1145		4.5	
J47-GE-15	23131	3.17	1141		4.5	
J47-GE-19	23131					
Nene Mk.103	23131					

... to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
Nene Mk.104	23131					
J33-A-25	23353		814		4.5	
J33-A-41	23353					
RB.162-86	23353	3.17	236		4.3	
PW305B	23389	1.11	450	4.3	15.5	
J97-GE-100	23442					
Atar 101B	23535					
Ghost 105	23575					
J35-A-25	23575	3.13	1025		4.7	
Adour RT.172 Mk.804	23664		713			
Derwent RB.37 Mk.5	24020	3.17			4.3	
J35-A-33	24020					
J35-A-33A	24020					
Nene RB.41-6/21	24020					
J35-A-35	24198					
J35-A-35A	24198					
Adour Mk.861-49	24243		582			
F405-RR-400L	24243					
GE1/J1A1	24465	1.98			11	
RB.162-30	24465					
RB.162-31	24465					
RB.162-32	24465					
DV-2F	24501	1.67	630	1.46	15.5	
J47-GE-17	24510	2.86			5.5	
J47-GE-17B	24510					
RD-60K	24510					
WP6B	24514					
Adour RT.172 Mk.811	24554	2.03	738	0.75	11.3	1413
Adour RT.172 Mk.815	24554		741	0.75	11.3	
Adour RT.172 Mk.106	24910					
J33-A-29	24910	3.26	998		4.5	
J35-A-29	24910					
J35-A-41	24910					
J47-GE-33	24910				5.5	
RD-9B	24999	2.67			7.1	
J47-GE-21	25221					
J47-GE-23	25221					
J47-GE-25	25221					
J47-GE-25A	25221					
PW306C	25292		473	4.5		
Adour Mk.861	25355		577		11.3	

...to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
PW306	25400		473	4.5		
CFE738-1-1B	25466	1.05	601	5.3	23	
AM-5B	25488					
WP6	25497		725			
Orpheus BOr.500	25577					
ALF501	25800	1.13		6	9.3	
F405-RR-401	26000		592	0.8		
J33-A-27	26022	3	810		4.5	
J47-GE-2	26289					
J47-GE-27	26289	2.56			5.5	
CFE738	26325	1.05	551	5.3	23	1643
VK-1A	26387					
VK-1	26476	2.97			4.4	
VK-1F	26476	3.25			4.4	
WP5	26476					
AM-5F	26689					
Avon RA.2	26689					
Avon RA.3 Mk.101-2	26689					
Orenda 2	26689					
Orenda 3	26689					
Orenda 8	26689					
RB.162-81	26734	2.72			4.5	
F125-GA-100	26800	2.27	617	0.3	18.5	
TFE1042-70	26800	2.27	617	0.3	18.5	
Adour Mk.871	26823		603	0.8	11.3	
PW306A	26867	1.12	473	4.5	18.3	
RD-45FA	26872					
PW306B	26912		473	4.5		
PW307A	27134					
109-012	27445	3.25			5.5	
RD-9	27490					
RD-9F	27579					
J33-A-16	27801					
J48-P-2	27801	3.29	932		4.4	
J48-P-3	27801	3.29	939		4.4	
J48-P-6	27801					
J48-P-6A	27801					
XJ48-P-1	27801	3.29	932		4.4	
Tay Mk.250 (Nene + AB)	27935					
F125	28000	2.28	617	0.49	18.5	1645
F124-GA-100	28024	2.29	499	0.4	19.4	

... to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	$(kg/s)/N$	kg	-	-	$^{\circ}K$
Orenda 10	28179					
J33-A-16A	28246					
J48-P-5	28246					
Orenda 9	28268					
AE3007C	28655		719	5.3		
AS907	28913	1.19	619	4.5	21	
Avon RA.25 Mk.502	28913					
Avon RA.25 Mk.503	28913					
Avon RA.25 Mk.504	28913					
Avon RA.3 Mk.100	28913	2.5			6.2	
Avon RA.3 Mk.101-3	28913					
Avon RA.3 Mk.103	28913					
RM3A	28913					
PW308A	29247		597	4.1		
RD-9E	29358					
WP6A	29420	2.78	725		7.4	
Atar 101D	29425	3.09			4.5	
Atar 101D-1	29425					
Atar 101D-2	29425					
Atar 101D-3	29425					
ALF502R-3	29803	1.16	606	5.71	11.6	
RD-36-35FVR	29914		201			
RD-36-35PR	29914		201			
AE3007C1	30088		720	5.3		
J40-WE-6	30248					
HTF7000	30400		619	4.4	28.2	
RB.153-61	30470		649	0.7	18	
RB.153-61R	30470			0.7	18	
Pirna 014A0	30915	2.42			7	
ALF502R-3A	31004	1.16	606	5.71	11.6	
ALF502R-5	31004	1.16	606	5.6	12.2	
AE3007A3	31137		730	5.3		
F102-LD-100	31137					
J40-WE-12	31137					
LF507-1F	31137	1.15	628	5.7	13.8	
LF507-1H	31137		624	5.7	13.8	
LF507-1N	31137		624			
PW308C	31137			4.1		
LF507	31138	1.12	628	5.6	13.8	
AS977-1A	31582	1.18	619	4.5	23	
RD-38	31871		231			

... to be continued ...

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Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
AE3007	32000	1.02	717	5	23	
AE3007A1/3	32027		730	5.3		
J40-WE-22	32027					
J40-WE-22A	32027					
J65-W-1	32027					
J65-W-1A	32027					
J65-W-2	32027					
Orenda 11	32072					
J65-W-5	32116					
J48-P-8	32249					
J48-P-8A	32249					
J48-P-8B	32249					
J48-P-8C	32249					
Pirna 014A1	32294	2.36			7	
Orenda 14	32361					
J65-B-3	32605					
J65-W-3	32605					
Avon RA.7 Mk.117	32694					
Atar 101G	32917	3.06			4.8	
Atar 101G-2	32917					
Atar 101G-2-1	32917					
Atar 101G-3	32917					
Avon RA.3 Mk.109	32917					
J40-WE-8	32917					
Avon RA.7 Mk.122	33028					
109-018	33317	3.33			7	
ALF502L	33362	1.21	595	5.2	13.6	
ALF502L-2	33362	1.21	595	5	13.6	
ALF502L-2A	33362	1.17	595	5	13.8	
ALF502L-2C	33362	1.17	595	5	13.8	
ALF502R-6	33362	1.18	624	5.6	13.8	
Atar 101E	33362					
Avon RA.3 Mk.104	33362					
Avon RA.3 Mk.107	33362					
Avon RA.4 Mk.107	33362					
Avon RA.7 Mk.113	33362					
Avon RA.7 Mk.20	33362					
Avon RA.7 Mk.26	33362					
J52-P-3	33362					
J65-B-7	33362					
J65-W-7	33362					

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Turbofan and turbojet engines : database handbook

Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
Sapphire ASSa.1 Mk.100	33362					
XJ52-P-1	33362					
Avon RA.7R Mk.114	33406	2.44			7	
AE3007A	33717	1.02	719	5.3	24	
AE3007A1	33717	1.02	719	5.3	24	
AE3007A1/1	33717		730	5.3		
AE3007A1P	33717		730	5.3		
J65-W-16	34251					
J65-W-16A	34251					
J65-W-18	34251					
Pirna 016	34251	2			10	
Verdon	34318					
Atar 101E-3	34322					
M45H-D Mk.501	34518	1.28	673	2.85	18.8	
M45H-01	34531		673	2.8	18	1330
ALF502L-3	34696	1.18	595	5	13.8	
J65-W-4	34696					
J65-W-4B	34696					
J65-W-6	34696					
PW308B	35981			4.1		
AE3007A1E	36075		730	5.3		
F124-GA-X	36119					
Atar 101E-4	36208					
Atar 101E-5	36208					
WS6A	36780		725	0		
F137-AD-100	36876	1.11	717	5		
Sapphire ASSa.6 Mk.101	36920					
J52-P-6	37810	2.32	933			
J52-P-6A	37810	2.32	933			
J52-P-6B	37810					
DV-22/AI-22	37952	1.05		5		
WP7	38246					
R-11B-300	38255					
R-11F-300	38255	2.67			8.7	
CF34-1A	38477	1.02	737	6.2		
R-11F2S-300	38477	2.72			8.8	
XJ99-RA-1	38655					
YJ57-P-3	38699	2.28	1991		11.6	
J73-GE-5	38922					
M45H-C	39144					
RB.199-34R-04 Mk.101	39144	1.75		1.1	23.4	

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Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
R126-300	39224					
R-95	39233					
J73-GE-7	39678					
RB.199-34R-04 Mk.104D	40034					
XJ57-P-1	40034	2.21	1991		10	
XJ57-P-1W	40034					
WP13	40207	2.72	1211	0		
R-13-300	40212	2.72			8.9	
RD-41	40212		290			
R-25-300	40256	2.72			9.6	
TF34-GE-100	40323	1.05	645	6.42	20	1496
TF34-GE-100A	40323		653	6.24	20	
AI-222-25	40345	1.81		1.19	15.9	
Atar 08C	40479					
RB.199-34R-04 Mk.104	40479		976			
RB.199-34R-04 Mk.103	40700	1.81	1061	1.06	23.5	1598
Atar 09B	40923					
Atar 09B-3	40923					
J73-GE-3	40923					
J73-GE-3A	40923					
J73-GE-3D	40923					
J73-GE-3E	40923					
CF34-3A1	41012	1.01	751	6.3	21	
CF34-3B	41012	0.98	757	6.3	21	
CF34-3B1	41012	0.98	757	6.3	21	
CF34-3A	41013	0.99	737	6.2	21	1477
J101-GE-100	41146	2.22		0.25	21	
M45H-E1	41146					
TF34-GE-2	41257			6.23		
TF34-GE-400A	41257	1.03	670	6.24	21	
TF34-GE-400B	41257		670	6.24	21	
J52-P-8	41368	2.44	961		13	
J52-P-8A	41368	2.44	961		13	
J52-P-8B	41368				13	
Atar 09C	41947	2.86	1456		5.7	
Atar 09C-3	41947					
Atar 09C-5	41947					
Avon RA.14 Mk.201	42258					
J71-A-2	42258					
J71-A-2A	42258					
J71-A-2B	42258					

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
WP7C	42649					
WP13A II	42658	2.8	1201			
M45H-E2	42703					
YJ79-GE-13	42703					
RB.199-34R-04 Mk.105	42952	1.8	980	0.97	23.4	
WP7A	43139					
Atar 08C-1	43148	2.75			5.8	
J57-P-2	43148					
J57-P-39	43148					
J57-P-6	43148				12.4	
J57-P-6A	43148				12.4	
J57-P-7	43148					
WP7B	43148	2.86	1053		8.1	
XJ35-A-23	43148	2.72	1583		8.8	
J79-GE-3	43592					
J79-GE-3A	43592	2.4			12	
J79-GE-3B	43592		1508		12	
Spey Jr. RB.183-2 Mk.555-15	43815	2.12	1024	1	15.4	990
Spey Jr. RB.183-2 Mk.555-15P	44037		1024	1	15.4	
Tay RB.183-55515P	44037	1.59	1037	0.71	15.5	
WP13F	44100			0		
R-195	44131		990			
WP7F	44131			0		
Trent-RB203,08	44439		805	3	16	
Avon RA.26 Mk.522	44482					
Avon RA.28 Mk.203	44482				7.8	
GE1/10	44482	2.27				1365+
J57-P-11	44482					
J57-P-12	44482					
J57-P-12A	44482					
J57-P-4A	44482					
J57-P-9	44482					
J57-P-9W	44482					
J79-GE-11	44482	2.39			12.9	
J79-GE-11A	44482		1615		12.9	
J79-GE-7	44482	2.39				
J79-GE-7A	44482					
J79-OEL-7	44482	2.39	1622			
JTF16	44482					
Olympus Mk.101	44482	2.17			11	
Avon RA.28 Mk.204	44704				7.8	

... to be continued ...

Turbofan and turbojet engines : database handbook

Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
Avon RA.28 Mk.205	44704				7.8	
Avon RA.28 Mk.207	44704	2.49	1301		7.8	
SM-X	45000			5		
AI-222-28	45149	1.91		1.13	16.9	
RB.193-12	45207					
J57-P-13	45372					
J57-P-21	45372	2.18				
J57-P-21A	45372					
J57-P-23	45372		2345		11.5	1144
J57-P-25	45372					
J57-P-8	45372					
J57-P-8A	45372				13.6	
J57-P-8B	45372				13.6	
J71-A-11	45372					
J71-A-13	45372					
YJ71-A-5	45372					
Avon RA.29/1 Mk.524	45594	2.23	1516		8.8	
Avon RA.29/1 Mk.525B	45594	2.23			8.8	
Avon RA.29/1 Mk.526	45594	2.23	1516		8.8	
J79-GE-4	45816					
J79-GE-5	45816					
J79-GE-5A	45816					
J79-GE-5B	45816					
J79-GE-5C	45816	2.39	1671			
J79-GE-2	46039	2.46	1642		12.5	
J79-GE-2A	46039				12.5	
Spey RSp.3 Mk.506-14	46306		1024	0.71		
Spey RSp.3 Mk.506-14A	46306		1024	0.71		
Spey RSp.3 Mk.506-14D	46306		1024	0.71		
Spey RSp.3 Mk.506-2	46306			0.71		
Spey RSp.3W Mk.506-14AW	46306		1038	0.71		
Avon RA.29/1 Mk.524B	46696		1516	0	8.7	1100
Avon RA.29 Mk.522	46706					
Avon RA.29 Mk.523	46706					
J57-P-10	46706					
J57-P-19W	46706				12.5	
J57-P-29W	46706				12.5	
J57-P-29WA	46706				12.5	
J79-MTU-J1K	46706	2.39			12.4	
F404-GE-F1D2	46884	2.29	785		24	
WP13A	47100		1201	0		

... to be continued ...

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
WP13B	47100			0		
F404-GE-400	47151	2.42	996	0.34	26	
F404-GE-400D	47151				26	
RM6B	47151					
J57-P-16	47596					
J57-P-20	47596	2.18	2155		13	
J57-P-20A	47596		2155		13	
J57-P-22	47596					
TF30-PW-1	47818	1.8		1.1	17.1	
TF30-PW-3	47818	2.27	1769	1.1	17.1	1144
J79-GE-15	48485	2.44	1678		12.9	
J79-GE-8	48485	2.44	1666		12.9	
J79-GE-8A	48485				12.9	
F404-GE-100D	48930	2.27	826		24	
F404-GE-102	48930		1035		26	
F404-GE-102D	48930					
Gyron Junior DGJ.10	48930					
J57-P-37A	48930					
J57-P-47	48930					
Pegasus 2	48930					
Sapphire ASSa.7 Mk.200	48930					
Sapphire ASSa.7R Mk.200R	48930					
Spey RSp.4 Mk.510-14	48930	1.7	1058	0.71	18.4	
Spey RSp.4 Mk.510-14W	48930	1.7	1189	0.71	18.4	
Spey RSp.4 Mk.510-5	48930		1049	0.71		
Spey RB.168 Mk.807	49064	1.87	1096	0.96	16.8	
Spey RB.168-1A RSp.2 Mk.101	49064	1.79	1121	0.7	16.5	
Atar 08K-50	49175	2.75			6.2	
Atar 09K-50	49175	2.78	1582	0	6.2	1208
RD-33	49500	2.18	1217	0.55	21.7	1680
CJ805-3	49820					
CJ805-3A	49820					
J52-PW-408	49820	2.24	1051		14.6	
J52-PW-408A	49820				14.6	
J57-P-43WA	49820	2.18			12.5	
J57-P-43WB	49820	2.18	1755		12.5	1144
J57-P-7A	49820					
JT3C-2	49820		1755			
JT3C-4	49820					
JT3C-6	49820	2.2	1921			
M88-2	50000	2.22	897	0.3	24.5	1850

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Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
Avon RA.24R Mk.200R	50042					
Avon RA.24R Mk.202	50042				7.8	
Avon RA.24R Mk.206	50042				8.2	
Avon RA.24R Mk.208	50042				7.8	
Avon RA.24R Mk.210R	50042				8.2	
Avon RA.24R Mk.211R	50042				8.2	
TF30-PW-6	50487	1.76	1231			
Avon RA.29/3 Mk.527B	50709	2.42	1518			
RM10	50709	2.42				
Spey RB.168-?? Mk.511-8	50709	1.7	1126	0.64	18.4	
Spey RSp.4 Mk.511-14	50709	1.7	1126	0.71	18.4	
Spey RSp.4 Mk.511-14W	50709	1.7	1189	0.71	18.4	
Spey RSp.4 Mk.511-5	50709	1.7	1049	0.71	18.4	
Spey RSp.4 Mk.511-5W	50709	1.7	1051	0.71	18.4	
Spey RSp.4 Mk.511-8	50709	1.7	1126	0.64	18.4	
Spey RSp.4 Mk.511-1	50718		1050	0.64	19	1350
F124-GA-XX	51154					
J57-P-17	51154					
CJ805-3B	51822					
Kaveri	52000					
TF306E	52044	1.84		1.1	17	
D-21A1	52266		2100	0.83	20.2	
J79-GE-10	52800	2.39	1749		13.4	
J79-GE-10B	52800	2.39			13.4	
J79-GE-17	52800	2.39	1740		13.5	928
J79-GE-17C	52800				13.5	
J79-GE-17E	52800				13.5	
J79-GE-19	52800	2.39	1740			
J79-MTU-17A	52800	2.39	1749		13.5	
D-20	52956					
D-20P	52956	1.76	1468	1	13.6	
F404-GE-402	53156		1035	0.31	26	
J57-P-55	53334					
Spey RB.168-20 Mk.251	53356	1.79	1243	0.7	19.2	
Spey RB.168-20 RSp.5-1 Mk.250	53356	1.79	1243	0.7	19.2	
J52-PW-409	53378					
JT3C-12	53378	2.2	1610		13.8	
JT3C-7	53378	2.22	1585	0	13	
Olympus Mk.102	53378					
Pegasus 3	53378					
Spey RSp.4 Mk.512-5W	53378	1.7	1183	0.71	20.7	

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
TF104	53378					
J79-GE-119	53601	2.36	1715	0	13.4	1273
Avon RB.146 Mk.301	53823	2.64			8.4	
RM6C	53823	2.64			8.4	
AL-5	53934			1	10	
RM12	54001	2.33	1050	0.31	27.5	
Avon RA.29/6 Mk.531B	54268	2.27	1582			
TF30-PW-8	54268	1.79	1146		17.1	
M53-2	54401	2.44		0.4	8.5	
M53-5	54401	2.44	1470		9	
JT8D-5	54490	1.6	1404			
Spey RB.168-25R RSp.2 Mk.202	54490	1.93	1857	0.7	19.5	
Spey RB.168-25R RSp.2 Mk.203	54490		1857	0.7	19.5	
WS9	54490			0.7	19.5	
CF34-8D1	55603	1.11	1120			
F414-GE-400	55603			0.4	30	
PW800 (AFTI)	55603			7.8		
Spey RSp.4 Mk.512	55800		1168	0.71		
Spey RB.168-25R RSp.2 Mk.201	55825	1.79		0.7	20.1	
Spey RSp.1 Mk.505-5	55825		998	0.71		
Spey RSp.4 Mk.512-14	55825	1.7	1183	0.71	20.7	
Spey RSp.4 Mk.512-14DW	55825	1.7	1183	0.71	20.7	
Spey RSp.4 Mk.512-14DWE	55825		1183	0.71		
Spey RSp.4 Mk.512-25	55825	1.7	1183	0.71	20.7	
Avon RA.29/6 Mk.533R	56047	2.22				
Avon RA.29/6 Mk.535R	56047	2.22			10.3	
Avon RB.146 Mk.302	56448	2.41			8.4	
Avon RB.146 Mk.302C	56448	2.41			8.4	
R-37F-300	56492					
CF34-8D3	57271	1.11	1120	4.9	27	
CF34-8D6	58049	1.11	1120			
RB.202	58271					
EJ200 Mk.100	58939	2.22	1037	0.4	25	1755
TF30-PW-408	59606					
M88-3	60051	2.22			26	
Olympus Mk.104	60051					
J57-P-59W	61163	2.69	1960			
PW1120	61300	2.29	1323	0.2	26.8	1523
CF34-8C1	61341	1.05	1066	4.9	27	
RM14	61608	1.22		3.04	15.8	
Tay RB.183-3 Mk.611	61608	1.22	1339	3.04	15.8	

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
Tay RB.183-3 Mk.611-8	61608	1.22	1339	3.04	15.8	
Tay RB.183-3 Mk.611-8C	61608	1.22	1339	3.04	15.8	
Tay RB.183-3 Mk.620-15	61608		1445	3.04	15.8	
CF34-8E2	62275	1.11	1120	5	27	
F412-GE-400	62275					
JT8D-1	62275	1.66	1404	1.06	15.4	
JT8D-1A	62275	1.66	1404	1.06	15.4	
JT8D-1B	62275	1.66	1404	1.06	15.4	
JT8D-7	62275	1.66	1431	1.07	15.8	
JT8D-7A	62275	1.66	1404	1.07	15.8	
JT8D-7B	62275	1.66	1404	1.07	15.8	
RM8A	62275	1.66		1.07	15.4	
SPW14	62275					
TF41-A-1	63387	1.79	1475	0.77	20	1455
CF34-8C5B1	63409		1120	4.9		
R-27F2M-300	63698	2.78	1497		10.9	
R-27M-300	63698					
AL-7	63743					
AL-7F	63743					
D-36-1	63743	1.02	1109	6.3	18.7	
D-36-3A	63743	1.02	1109	6.3	18.7	
D-36-4A	63743		1109	6.3		
M53-P2	64000	2.56	1500	0.35	9.8	1533
CF34-8C5	64499	1.11	1120	4.9		
JT3D-7B	64499	1.66	1475	1.03	16.9	853
JT8D-9	64499	1.6	1450	1.03	15.9	
JT8D-9A	64499	1.6	1450	1.03	15.9	
JT8D-M-9	64499			1.03	15.9	
TF41-A-1B	64499	1.83	1593	0.76	20	1458
F414	64900	2.38	1110	0.37	30	
F100-IHI-100	65255	2.08	1442	0.71	23	
F100-IHI-220E	65255	2.07	1464		24	
F100-PW-100	65255	2.04	1375	0.71	24.8	1553
F100-PW-200	65255	2.03	1375	0.71	25	1553
F100-PW-220	65255		1451	0.71	25	
F100-PW-220E	65255		1429		25	
BR710A1-10	65611	1.11	1597	4.2	25.7	
BR710A2-20	65611	1.11	1597	4.2	25.7	
BR710C4-11	65611	1.11	1597	4.2	25.7	
R-27V-300	65700		1350			
BR710	66034	1.1	1597	4	25.7	

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
RD-3	66194					
BR710B3-40 Mk.101	66278	1.11		4.2	25.5	
D-30-1	66679	1.7	1550	1	18.6	
D-30-2	66679			1		
D-30-3	66679	1.72	1550	1	17.7	
D-30U-154	66679	1.7	1550	1	18.6	
CJ805-21	66708		1680	1.5	12	
D-30P	66708		1520	1	18.6	1300
JT8D-11	66723	1.76	1501	1.05	16.2	
SaM146	66723					
TF30-PW-18	66723				22	
TF41-A-2	66723	1.88	1475	0.74	21.4	
TF41-A-2B	66723	1.88	1475	0.74	21.4	
TF41-A-400	66723	1.88	1475	0.74	21.4	
Tay RB.183-3 Mk.650	67150		1515	3.1	16.4	1370
Tay RB.183-3 Mk.650-14	67168		1515	3.06	16.2	
Tay RB.183-3 Mk.650-15	67168		1515	3.06	16.2	
R-28-300	68057					
TF30-PW-100	68057	1.89	1814	0.73	21.8	1397
Tay RB.183-3 Mk.651-54	68502	1.28	1533	3.07	16.6	
Tay RB.183-3 Mk.651	68503	1.27	1533	3.07	16.6	
RD-36-51V	68636		4125			
AL-7F-1	68645	2.78			9.1	
AL-7F-2	68645					
AL-7PB	68645					
JT8D-15	68947	1.79	1549	1.03	16.5	
JT8D-15A	68947	1.67	1576	1.04	16.6	
Pegasus 5-1	68947					
Pegasus 5-2	68947					
JT4A-3	70282	2.18	2277			
JT4A-5	70282	2.18	2184			
JT4A-7	70282	2.18				
GE1/6	70415	0.95		8	25	
WS6	71131	1.76	2100	1	14.4	
BR710-48	71171			4.2		
JT8D-17	71171	1.7	1556	1.01	16.9	
JT8D-17A	71171	1.7	1576	1.02	17.1	
RB.432	71171					
CJ805-23B	71616	1.5			13	
CJ805-23C	71616					
J75-P-19	72061				12	

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Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
JT4B-21	72728					
JT8D-17AR	72950	1.73	1585	1	17.3	
RM8B	72950	1.7		0.96	16.9	
J75-P-3	73395					
J75-P-5	73395					
D-436K	73551	1.05		6.2	21	
D-436TP	73551	1.05				
R-15-300	73551					
R-15B-300	73551					
R-15BD-300	73551					
F100-PW-220P	74285		1526	0.36		
PW1128	74285	2.42			27	
JT4A-10	74730	2.29	2313			
JT4A-9	74730	2.29	2291			
D-436T1	75019	1.06	1450	4.95	25.2	1550
D-436TM	75019		1450	4.95	25.2	
J52-P-16	75175					
F110-GE-400	75600	1.86	1526	0.87	30.3	1643
F101-GE-100	75619	1.61		2.1	26.5	
F110-GE-129	75619		1805	0.76	30.7	
F110-IHI-129	75619		1787	0.76	30.7	
J75-P-13B	75619					
JT3D-1	75619	1.47	1880	1.4	12.5	
Olympus Mk.201	75619					
PS-7	75619		1350			
TF33-PW-3	75619	1.47	1769	1.55	13	1144
AL-21F-3	76509	2.15	2005		14.8	
AL-21F-3A	76509					
J75-P-19W	76509	2.24	2703		12	
YJ75-P-9	76509					
CF34-10D5	77199	1.08	1724	5	29	
F101-GE-102	77355	1.59	2018	1.91	26.8	1672
JT8D-17R	77399		1585	1	17.5	
Conway RB.80 RCo.11 Mk.101	77844			0.3		
Conway RB.80 RCo.12 Mk.508	77844	2.06	2061	0.3	14.1	
Conway RCo.12 Mk.508	77844	2.06	2061	0.3	14.1	
Conway RCo.12 Mk.509	77844		2061	0.3	14.1	1315
JT4A-11	77844	2.38	2313		12.5	
JT4A-12	77844	2.38	2220		12.5	
R-29-300	78444	2.69	1880		13.1	
R-29B-300	78444		1760		12.4	

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	$(kg/s)/N$	kg	-	-	$^{\circ}K$
R-29BS-300	78444					
R-29PN-300	78444					
F100-PW-229	79178	2.1	1377	0.36	32.4	1755
F100-PW-229A	79178				35	
AL-31F	79400	1.86	1530	0.57	23	1600
AL-31MF	79400		1520	0.57		
AL-21	79601					
CF34-10A	80068		1701	5		
Conway RCo.12 Mk.508A	80068	2.08	2061	0.3	14	
Conway RCo.12 Mk.509A	80068	2.08	2061	0.3	14	
JT3D-3B	80068	1.52	1950	1.37	13.6	1144
JT3D-3C	80068	1.45	1969	1.4	13	
Tay RB.183-3 Mk.670	80068		1701	3.2	19	
TF33-PW-102	80068	1.52		1.37	13.6	
TF33-PW-102C	80068	1.52		1.37	13.6	
TF33-PW-11	80068					
TF33-PW-11A	80068					
TF33-PW-5	80068	1.52	1891			
TF33-PW-9	80068	1.52	1891			
JT3D-3	80148	2.18	2170	1.25	16	1233
D-436T2	80415		1450	4.9	26.2	
F110-GE-100	81536	2.11	1767	0.87	30.4	
BR715A1-30	82292	1.05	2085	4.7	32.1	
CF34-10E5	82292	1.08	1724	5		
CFM56-7B18	82292	0.99	2366	5.6	21.7	
JT8D-209	82292	1.45	2000	1.82	17.4	
CF34-10D6	83404	1.08	1724	5	29	
R-35-300	83849	2.72	1765		13.1	
F118-GE-100	84516	1.06	1451		35.1	
F118-GE-101	84516	1.06	1429		35.1	
JT3D-7	84516	1.47	1969	1.43	13.5	
JT3D-7A	84516	1.47	1969	1.43	13.5	
Pegasus 11 Mk.101	84516		1642		14.6	
AM-3D	85316					
RD-3M	85316					
AM-3A	85806					
Iroquois PS-13	86295					
BR715-55	88444	1.05	2062	4.7	32.1	
BR715B1-30	88964		2114	4.4		
CFM56-3B1	88964	1.08	1940	6	22.6	
CFM56-9	88964	1.08	1929	5.08	23.2	

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Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
Gyron 1	88964					
JT8D-217	88964	1.5	2009	1.77	18.6	
JT8D-217A	88964	1.5	2009	1.77	18.6	
JT8D-217C	88964	1.42	2041	1.72	20.1	
Olympus Mk.301	88964	2.28			13.2	
MTFE	89000		1769	5.2		
PS-90A10	90223		1896	3.76	23.1	
TF30-PW-108	90525				16.5	
Conway RCo.42 Mk.540	90610	1.86	2268	0.6	14.8	
Pegasus 11 Mk.102	91188	1.7	1642	1.3	14.6	
Pegasus 11 Mk.103	91188	1.7	1642	1.5	14.6	
Pegasus 11 Mk.104	91188		1642	1.2	14.6	
CFM56-7B20	91633	1.02	2366	5.6	22.7	
Conway RB.80 RCo.17 Mk.201	91633			0.3		
AM-3M-500	93145					
D-30F6	93163	2.03	2416	0.57	21.5	
NK-8-2	93163	1.64	2100	1	21.5	
RD-3M-500	93163	2.83			6.4	
WP8	93163		3132			
VD-7B	93168					
NK-8-3	93190					
BR715C1-30	93412		2085	5	32.6	
PS-30V-12	93412					
TF33-PW-100	93412				15.6	
TF33-PW-100A	93412				15.6	
TF33-PW-7	93412	1.59	2109	1.21	15.6	1228
TF33-PW-7A	93412			1.21	16	
XJ53-GE-1	93412					
F402-RR-406A	95414	2.1	1796		15.3	
Pegasus 11-21 Mk.106	95636		1796	1.2	15.3	
CFM56-5B8/P	96080		2381	6		
CFM56-5B8	96082		2381	6		
F108-CF-100	96233	1.03	2091	6		1493
JT8D-219	96526	1.47	2048	1.77	19.2	1411
Conway RB.80 RCo.43D Mk.301	96971		2314			
Conway RCo.43D Mk.550B	96971	1.67	2314	0.6	15.8	
Pegasus 11-21 Mk.105	97000		1475	1.34	12.9	1496
Conway RCo.42-3	97119		2310	0.6	15.1	
CFM56-2B1	97860	1.02	2119	6	23.7	1560
CFM56-2C1	97860	0.99	2102	6	24.7	1543
CFM56-3B2	97860	1.11	1951	5.9	24.3	1642

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
CFM56-5A4	97860	0.91	2257	6.2	24.1	
CFM56-5B5	97860	0.91	2381	6	24.4	
CFM56-5B5/P	97860	0.91	2381	6	24.4	
CFM56-7B22	97860		2366	5.4	24.6	
F110-GE-X	97860					
PS-9	97860		1750			
PW6122	97860	1.02	1867	4.9	27.2	
V2522-D5	97860	0.96		4.9	25.2	
YJ93-GE-3	97860	1.98	2359			
F199-PW-100	98000	1.72	1360	0.2		
V2522-A5	102490	0.96	2382	4.9	25.2	
NK-8-2U	102976	1.61	2100	1.05	23.2	
NK-8-4	102976	1.67	2100	1.02	23.2	
NK-84	103005		2200	1	23.2	1145
CFM56-5B9	103644		2381	5.9		
CFM56-5B9/P	103644		2381	6		
CFM56-3C1	104533	0.93	1951	6	25.2	1646
CFM56-5A5	104533	0.91	2257	6.2	25.4	
CFM56-5B6	104533	0.93	2381	5.9	25.8	
CFM56-5B6/2	104533	0.93	2381	5.9	25.8	
CFM56-5B6/2P	104533	0.93	2381	5.9	25.8	
CFM56-5B6/P	104533	0.93	2381	5.9	25.8	
VD-7D	105422					
PW6124	105700			4.9		
F402-RR-408	105867	2.15	1932	1.2	16.3	
Pegasus 11-61 Mk.107	105900		1932	1.2	16.3	
D-30KU-2	106090		2318	2.35		
CFM56-2A2	106757	1.02	2186	5.9	25.4	1628
CFM56-2C2	106757	1.02			26.5	
CFM56-7B24	106757	1.05	2366	5.3	26	
Pegasus 15	106757					
PW6162	106757	1.05	1867	4.9	29.6	
RB.220	106757					
R-79-300	107646	1.87	2750	1		
D-30KU	107869	1.4	2668	2.35	17.4	
VD-7	107869					
V2524-A5	108894	1.02	2331	4.9	26.5	
V2500-A1	110310	0.99	2363	5.42	29.7	1537
V2527-A5	110310	1.02	2331	4.75	27.4	
CFM56-5A1	111205	0.93	2266	6	26.5	1537
J58-P-4	111205	2.27			8.8	

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
V2525-D5	111206	1.02	2382	4.8	27.7	
D-30K	112815		2150	2.3	20	
CFM56-7B26	117432	1.08	2366	5.1	27.9	
D-30KU-90	117677		2400	2.44		
PS-90A12	117677		2300	5.05	25.3	
D-30KP	117699	1.36		2.42	18.4	
D-30KP-2	117699			2.42		
D-30KPV	117699					
CFM56-5A3	117877	0.93	2266	6	27.8	
CFM56-5B4	120101	0.96	2381	5.7	29.1	
CFM56-5B4/2	120101	0.96	2381	5.7	29.1	
CFM56-5B4/2P	120101	0.96	2381	5.7	29.1	
CFM56-5B4/P	120101	0.96	2381	5.7	29.1	
CFM56-5B7/P	120101	0.96	2381		29.1	
CFM56-5B7	120102		2381	5.7	29.1	
CFM56-7B27	121436	1.08	2366	5.1	28.9	
V2528-D5	124550	0.99	2382	4.7	30.4	
RB.178	126774					
D-15	127485					
NK-144	127485			0.6	14.2	
NK-86	127485		2450	1.15	13.4	
VD-5	127485					
PS-12	132387		2449	8.39	40.2	
V2530-A5	133000	1.02	2331	4.6	31.6	
CFM56-5B1	133446	0.99	2381	5.5	32	
CFM56-5B1/2	133446	0.99	2381	5.5	32	
CFM56-5B1/P	133446	0.99	2381	5.5	32	
V2530-D5	133446	1.02		4.6	31.6	
Olympus Mk.320	136159					
NK-321	137196		3442	1.4	28.4	
CFM56-5B2	137894	0.99	2381	5.5	32.9	
CFM56-5B2/P	137894	0.99	2381	5.5	32.9	
CFM56-5C2	138784	0.91	2585	6.6	31.5	1633
Olympus 593 Mk.610	139460	2.5	4529	0	14.5	1440
V2533-A5	140560	1.05	2331	4.5	33.4	
CFM56-5B3	142342	1.02	2381	5.4	33.7	
CFM56-5B3/2P	142342	1.02	2381	5.4	33.7	
CFM56-5B3/P	142342	1.02	2381	5.4	33.7	
CFM56-5C3	144567	0.91	2585	6.5	32.6	
CFM56-5C3/F	144567	0.91	2585	6.5	32.6	
Olympus 593 Mk.601	145011	1.98	2637		15.5	

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
PS-12M	145634		2449			
NK-144-22	147102					
NK-144A	147102			0.53	17	
CFM56-5C4	151239	0.93	2585	6.4	33.9	
CFM56-5C4/P	151239	0.93	2585	6.4		
R-79V-300	152128					
PS-90	156800	1.07	2950	4.6	31.9	1640
PS-90AN-76	156910		2950	4.6	35.5	
PS-90A	156911		2950	4.6	35.5	1609
NK-22	158867					
PW2237	162804	0.95	3259	5.8	27.9	
PW2337	162804	0.95	3259	5.8	27.4	
RB.211-535C-37	166363		3308	4.4	21.1	
RB.211-535C	166400		3309	4.4	21.1	
PW2037	170144	0.94	3259	5.8	27.4	1678
JTF17A-21	170366	2.12				
RB.211-23	170722					
Olympus 593 Mk.611	170811	1.98	2637			
Olympus 593 Mk.621	170811	1.98	2637			
R-79M-300	176149					
NK-93	176518	0.67	3650	16.6	28.9	1520
CF6-6	177928		3334	6.2	26.6	
CF6-6D	177928	1	3582	5.72	24.3	
PW2040	178373	0.93	3259	5.9	29.9	
PW2240	178373	0.93	3259	5.9	27.6	
RB.211-535E4-37	178373	0.92	3295	4.3	25.8	
CF6-6E	180597					
RB.211-22-02	180597		3261	4.8	27	
TF39-GE-1	181509	0.89	3260	8	26	1561
TF39-GE-5CA	182800	0.89	3583	8	25.7	1643
CF6-6D1	184600	0.99	3582	5.76	25.2	
CF6-6D1A	184600	0.99	3582	5.76	25.2	
CF6-6K	184600	0.98	3709		25	
CF6-6K2	184600	0.98	3709		25	
F117-PW-100	185490	0.96	3221	5.8	27.6	
NK-25	186380					
RB.211-22B	186800		4171	5	24.5	
CF6-6F	186824					
D-100	186824			8	35	
JT9D-1	186824			5	21.5	
RB.211-22B-02	186824	1.06	4171	4.8	24.5	

... to be continued ...

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Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
RB.211-22C-02	186824		4171	4.8		
PW2043	189493	0.99	3248	6	31.9	
PW2143	189493	0.99	3248	6	31.2	
PW2643	189493	0.99	3248	6	31.2	
TF39-GE-1C	191295			8		
RB.211-40	191451					
RB.211-535E4B-37	191717		3295	4.3	25.8	
RB.211-535F5-37	191717		3295	4.3		
RB.211-535E4	191718	1.72	3295	4.3	25.8	1500
JT9D-3	193497	0.98	3824	5.2	22	
D-110	196121			3	31	
JT9D-3A	196833	0.98	3905	5.2	21.5	
JT9D-15	202393	1.01				
JT9D-20	205952	1.05	3833	5.2	21.1	
JT9D-20J	205952	1.05	3833	5.2	23.5	
JT9D-7	205952	1.01	4014	5.2	22.3	
CF6-45A	206841		3977	4.64	26.3	
CF6-45A2	206841		3977	4.64	26.3	
CF6-45B	206841		3977	4.64	26.3	
CF6-45B2	206841		3977	4.64	26.3	
CF6-50C2F	206841		3960	4.64	26.3	
JT9D-7A	208843	1.03	3982	5.1	22.5	
JT9D-7AH	208843		4014	5.2		
JT9D-7ASP	208843	1.03	3983	5.1	22.5	
JT9D-7AW	208843	1.03	4014	5.1	22.5	
JT9D-25	209065			5.2		
RB.207	211290	1.53		5	27	
CF6-80A	213514	0.97	3854	4.66	27.3	
CF6-80A1	213514	0.97	3819	4.66	27.3	
JT9D-7F	213514	1.04	4014	5.1	22.8	
JT9D-7FW	213514		4014	5.1		
JT9D-7R	213514		4039	4.9	23.4	
JT9D-7R4D	213514	0.97	4039	4.9	23.4	
RB.211-524	213514		4452	4.5		
JT9D-7R4D1	213600	0.97	4039	4.9	23.4	
D-18T-1	214172		4100	5.6		
CF6-50A	215000	1.1	3720	4.4	28.6	
CF6-80A3	217900	1.01	3819	4.59	28.4	
CF6-50	217962		3674			
CF6-50B	217962	1.1	3720	4.4	28.6	
CF6-80A2	222410	0.99	3854	4.59	28.4	

... to be continued ...

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Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
JT9D-7J	222410		4014	5.1	23.5	
JT9D-7R4E	222410	0.97	4039	4.9	24.2	
JT9D-7R4E3	222410	0.97	4128	4.9	24.2	
JT9D-7R4E4	222410	0.97	4128	4.9	24.2	
RB.211-24	222410					
RB.211-524B	222410		4452	4.5	28.4	
RB.211-524B-02	222410		4452	4.5	28.4	
RB.211-524B2-02	222410		4452	4.5	28.4	
RB.211-524B4-02	222410		4452	4.4	29	
RB.211-524B4D-02	222410		4452	4.4	28.6	
RB.211-524BD-02	222410		4452	4.5	28.4	
RB.211-61	222410					
JT9D-7R4E1	222500	0.97	4039	4.9	24.2	
CF6-50C	224000	1.12	3956	4.26	29.3	
CF6-50C2R	224000	1.04	3960	4.31	29.2	
CF6-50D	226858		3776			
CF6-50D1	226858					
GE4/J5P	229082	2.95	5126		12.5	
RB.211-524C	229082		4472	4.5	28.6	
RB.211-524C2	229082		4472	4.5	28.6	
CF6-80C2B2	229483	0.9	4258	5.31	27.1	1608
D-18T	229794	1.02	4100	5.6	25	1600
D-18T-3	229794		4100			
F103-GE-101	230022	1.13	3977	4.31	30.2	1639
JT9D-59A	230150	1.06	4146	4.9	24.5	
CF6-50C1	230500	1.05	3956	4.24	30.1	
CF6-50C2	230500	1.05	3960	4.31	30.4	
PW4152	231310	0.88	4179	4.85	27.3	
CF6-80C2B2F	231351		4309	5.31		
CF6-80C2B3	231351		4258			
CF6-80C2B3F	231351		4309			
PW4052	232196	0.88	4179	4.85	26.4	
RB.211-56	232196			5.04	26	
CF6-80C2A2	233353	0.9	4246	5.05	27.8	
CF6-50E	233531	1.07	3851	4.24	30.1	
CF6-50E1	233531	1.05	3851	4.24	30.1	
CF6-50E2	233531	1.05	3977	4.31	30.4	
CF6-80C2	233531	0.93	4144	5.2	30.4	
JT9D-59	235755	1.06	4146	4.9	24.5	
JT9D-70A	235755	1.06	4153	4.9	24.5	
JT9D-7Q	235755		4216	4.9	24.5	

... to be continued ...

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Engine	T_{ssl} N	$10^5 SFC_{ssl}$ $(kg/s)/N$	W_{eng} kg	BPR -	OPR -	TET °K
JT9D-7Q3	235755		4216	4.9	24.5	
JT9D-9	235755					
RB.211-524D4	235755		4479	4.4	29.3	
RB.211-524D4B	235755		4479	4.4	29.6	
Trent 1000	235755		6437	10.8		
CF6-50C2B	240203	1.09	3960	4.25	31.1	
CF6-50E2B	240203	1.06	3977	4.24	30.9	
JT9D-59B	242427		4155	4.8	25.2	
JT9D-70B	242427		4162	4.8	25.2	
JT9D-7R4G2	243539	1.02	4144	4.8	26.3	
D-18TM	248107		4750	5.5		
Trent 553-61	248130		4717	7.7	35.1	
PW4156A	249080	0.91	4179	4.85	29.8	
JT9D-7R4H1	249200	1.03	4040	4.8	26.7	1616
RB.211-524G4-T	250878		4387	4.1		
CF6-80C2B1	252213	0.91	4258	5.19	29.3	
PW4056	252435	0.91	4179	4.85	28.4	
PW4156	252435	0.91	4179	4.85	30.2	
CF6-80C2B1F	254259	0.9	4309	5.15	30.4	1608
CF6-80C2B4	254348	0.92	4263	5.15	29.9	
CF6-80C2B4F	254793	0.9	4427	5.14	29.9	
CF6-80C2A1	257400	0.95	4246	5.15	30.4	
CF6-80C2A8	257400	0.97	4259	5.05	30.4	
CF6-80C2B1F2	257551		4309	5.19		
PW4158	257996	0.91	4179	4.75	30.7	
RB.211-524G	257996		4387	4.3	32.9	
RB.211-524G-T	257996		4295	4.3	32.9	
RB.211-524G/H-T	257996		4387	4.3		
RB.211-524G3	257996		4387	4.1		
Trent 758	257996					
PW4358	258000		4173	5.2	29.6	1538
Trent 556-61	260064		4717	7.32	35.6	1581
Trent 560-61	261500		4717	7.5	36.7	
CF6-80C2A3	262221	0.93	4246	5.05	31.1	
CF6-80C2A7	262444		4259	5.05		
RB.211-524H2-T	264668		4295	4.1		
PW4060	266892	0.93	4179	4.85	30	
PW4060A	266892	0.93	4179	4.85	31.5	
PW4460	266892	0.93	4179	4.85	31.5	
CF6-80C2B6F	267025	0.91	4427	5.06	31.4	
CF6-80C2B6FA	267025	0.91	4427	5.06	31.4	

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Turbofan and turbojet engines : database handbook

Engine	T_{ssl}	$10^5 SFC_{ssl}$	W_{eng}	BPR	OPR	TET
	N	(kg/s)/N	kg	-	-	°K
CF6-80C2B6	267203	0.95	4386	5.06	31.1	
CF6-80C2A5	267337	0.96	4259	5.05	31.5	1608
CF6-80C2A5F	267337	0.96	4259	5.05	31.5	
RB.211-524H-T	269561		4295	4.1	34.5	
RB.211-524H2	269561		4387	4.1		
RB.211-524H3	269561		4387	4.1		
RB.211-524H	269562	1.59	4386	4.3	34.5	1548
D-18TR	269681		4750			
CF6-80C2D1F	269961	0.91	4468	5.03	31.8	
CF6-80C2B5F	276233	0.91	4427		31.4	
CF6-80C2B7F	276233	0.91	4427		31.4	
CF6-80C2A6F	280237		4300	5.05		
CF6-80C2B9F	281571				31.4	
PW4062	281571		4179	4.85	32.3	
PW4462	281571		4179	4.85	32.3	
CF6-80C2B8F	282461		4522		31.4	
CF6-80C2A6	284685		4300	5.05		
Trent 764	284685					
PW4164	286920		5625	5.1	32	
CF6-80E1A2	287055	0.94	4865	5.3	32.4	
PW8160	289133					
Trent 665	289133		5171	7		
CF6-80E1	291357	0.93	5063	5.3	32.4	
CF6-80E1A1	291357	0.93	5063	5.3	32.4	
CF6-80E1A4	297451	0.96	4865	5	33.7	
GENx-2B67	298000			8	45	
Trent 768-60	300254		4785	4.97	35.2	
GP7168	302478		5216	7	42.3	
GP7268	302478		5216	8	46	
Trent 600	302478		4719	8		
CF6-80E1A3	304840		4865	5	33.7	
PW4168	305148		5625	5.1	33.4	
PW4168A	305148		5625	5.1	32	
GENx-1B70	311000			9.6	43	
GP7270	311374			8.7	45.6	
GP7172	315822			8.7	43.9	
Trent 871-17	315822		5942			
Trent 772-60	316267		4785	4.89	36.8	
Trent 772B-60	316279		4748	4.89	36.8	
GENx-1A72	320000			8.9	43	
Trent 672	320270		5171		43.2	

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Turbofan and turbojet engines : database handbook

Engine	T_{ssl} N	$10^5 SFC_{ssl}$ (kg/s)/N	W_{eng} kg	BPR -	OPR -	TET °K
PW4074	331391		6597	6	30.3	
Trent 975	333615		6271	7.8	35.8	
Trent 1700	334000					
Trent 775-60	334282		4786	4.77	39	
Trent 970-84	334282		6271	7.1		
GP7176	338000			8.7	43.9	
Trent 976	338000		5806	8		
GE90-76B	339842		7074	8.4	39.3	
Trent 900	340289		6271	7.14	41	1593
GP7277	342511		6033	8.7	45.6	
PW4077	342511		6597	6.2	31.5	
Trent 875-17	346515		5942	6.21	34.9	
Trent 970B-84	348294		6271	7.1		
Trent 877-17	359059		5942	6.15	35.9	
Trent 977-84	359326		6271	7.1		
Trent 977B-84	372915		6271	7.1		
PW4084	373649		6597	6.41	36.3	1634
Trent 980-84	374094		6271	7.1		
GE90-85B	376763	0.92	7074	8.4	39.3	
Trent 882-17	376763		5942		38.8	
Trent 884-17	386593		5942	5.95	39.8	
GE90-90B	400338		7074	8.4	40	
PW4090	401228		7069	6.3	38.6	
Trent 890-17	406121		5942	5.74	42.7	
Trent 892-17	406788		5957	5.79	40.8	
GE90-92B	409234		7074	8.3	40	
GE90-94B	416796		7550	8.7	40	
Trent 895-17	422579		5981	5.79	41.6	
Trent 895C-17	422579		5981	5.79	41.6	
PW4098	435924		7484	5.8	42.8	
Trent 8104	462613		6532	5.8	45	
GE90-110B1	489302		8550	7.2		
GE90-115B	511543		8283	7.2	42	

Chapter 4

Engines mounted on a given civil aircraft

A300-600ST : CF6-80C2A8	A310-304 : CF6-80C2A2
A300-B1 : CF6-50C	A310-308 : CF6-80C2A8
A300-B2-1A : CF6-50A	A310-322 : JT9D-7R4E1
A300-B2-1C : CF6-50C	A310-324 : PW4152
A300-B2-202 : CF6-50C1	A310-325 : PW4156A
A300-B2-203 : CF6-50C2	A318-111 : CFM56-5B8/P
A300-B2K-3C : CF6-50C	A318-112 : CFM56-5B9/P
A300-B2-320 : JT9D-59A	A318-121 : PW6122
A300-B4-203 : CF6-50C2	A318-122 : PW6124
A300-B4-220 : JT9D-59A	A319-111 : CFM56-5B5
A300-C4-203 : CF6-50C2	A319-112 : CFM56-5B6
A300-F4-203 : CF6-50C2	A319-113 : CFM56-5A4
A300-B4-2C : CF6-50C	A319-114 : CFM56-5A5
A300-B4-102 : CF6-50C1	A319-115 : CFM56-5B7
A300-B4-103 : CF6-50C2	A319-131 : V2522-A5
A300-B4-120 : JT9D-59A	A319-132 : V2524-A5
A300-B4-601 : CF6-80C2A1	A319-133 : V2527-A5
A300-B4-603 : CF6-80C2A3	A320-111 : CFM56-5A1
A300-B4-608 : CF6-80C2A8	A320-211 : CFM56-5A1
A300-B4-620 : JT9D-7R4H1	A320-212 : CFM56-5A3
A300-B4-622 : PW4158	A320-214 : CFM56-5B4
A300-C4-620 : JT9D-7R4H1	A320-231 : V2500-A1
A300-B4-605R : CF6-80C2A5	A320-232 : V2527-A5
A300-B4-622R : PW4158	A320-233 : V2527-A5
A300-C4-605R : CF6-80C2A5	A321-111 : CFM56-5B1
A300-F4-605R : CF6-80C2A5	A321-112 : CFM56-5B2
A300-F4-622R : PW4158	A321-131 : V2530-A5
A300-B4-622F : PW4158	A321-211 : CFM56-5B3/P
A300-C4-605F : CF6-80C2A5	A321-212 : CFM56-5B1
A310-203 : CF6-80A3	A321-213 : CFM56-5B2
A310-204 : CF6-80C2A2	A321-231 : V2533-A5
A310-221 : JT9D-7R4D1	A321-232 : V2530-A5
A310-222 : JT9D-7R4E1	A330-201 : CF6-80E1A2
A310-203C : CF6-80A3	A330-202 : CF6-80E1A4
A310-222 Adv : JT9D-7R4E1	A330-203 : CF6-80E1A3

A330-223 : PW4168A	A380-863F : GP7277
A330-243 : Trent 772B-60	An 72 : D-36-1
A330-201F : CF6-80E1A2	An 74-200 : D-36-3A
A330-202F : CF6-80E1A4	An 74-300 : D-36-4A
A330-203F : CF6-80E1A3	An 74-TK100 : D-36-3A
A330-223F : PW4168A	An-124 Ruslan : D-18T
A330-243F : Trent 772B-60	An124-100M150 : D-18T-3
A330-301 : CF6-80E1A2	An124-100M : D-18T-3
A330-302 : CF6-80E1A4	An-124-200 : CF6-80C2
A330-303 : CF6-80E1A3	An-148 : D-436K
A330-321 : CF6-80E1A3	An-148 : CF34-10A
A330-322 : PW4168	An-148 : PW800 (AFTI)
A330-323 : PW4168A	An-148 : SaM146
A330-341 : Trent 768-60	An-225 Mriya : D-18T
A330-342 : Trent 772-60	An-225 Mriya : Trent 892-17
A330-343 : Trent 772B-60	An-225 Mriya : PW4098
A340-211 : CFM56-5C2	ARJ21-700 : CF34-10A
A340-212 : CFM56-5C3	ARJ21-900 : CF34-10A
A340-213 : CFM56-5C4	B707-121 : JT3D-3B
A340-213E : CFM56-5C4	B707-123 : JT3D-1
A340-311 : CFM56-5C2	B707-124 : JT3C-6
A340-312 : CFM56-5C3/F	B707-131 : JT3C-6
A340-313 : CFM56-5C4	B707-138 : JT3D-1
A340-313E : CFM56-5C4	B707-227 : JT4A-3
A340-541 : Trent 553-61	B707-2 : JT4A-5
A340-642 : Trent 556-61	B707-2 : JT4A-9
A350-100? : GENx-1A72	B707-2 : JT4A-10
A350-104? : Trent 1000	B707-320 : JT4A-11
A350-80? : GENx-1A72	B707-320B : JT3D-3B
A350-84? : Trent 1700	B707-320C : JT3D-3B
A350-90? : GENx-1A72	B717-2 : BR715A1-30
A350-94? : Trent 1000	B717-2 : BR715C1-30
A380-841 : Trent 970-84	B720 : JT3C-7
A380-861 : GP7270	B720B : JT3D-3
A380-843F : Trent 977-84	B720-020 : JT3D-1

B727-100 : JT8D-7	B737-900ER : CFM56-7B20
B727-100 : JT8D-1	B737-900W : CFM56-7B20
B727-100 : JT8D-9	B747-100 : JT9D-3A
B727-100 : JT8D-11	B747-100B : RB.211-524C2
B727-100 : JT8D-15	B747-100B SR : CF6-45A2
B727-100 : JT8D-17	B747-100SF : JT9D-7A
B727-200 : JT8D-7	B747-200B : JT9D-7AW
B727-200 : JT8D-9	B747-200C : JT9D-7FW
B727-200 : JT8D-11	B747-200F : RB.211-524D4
B727-200 : JT8D-15A	B747-200M : JT9D-7F
B727-200 : JT8D-17	B747-200 : CF6-50E2
B727-200 : JT8D-17R	B747-200 : JT9D-7Q
B737-100 : JT8D-7	B747-200 : JT9D-7J
B737-100 : JT8D-9	B747-200 : JT9D-7R4G2
B737-100 : JT8D-15	B747-300 : RB.211-524B2-02
B737-200 : JT8D-9A	B747-300M : CF6-50E2
B737-200 Adv : JT8D-15A	B747-300SR : JT9D-7A
B737-200 Adv : JT8D-17A	B747-400 PB : PW4056
B737-200 Adv : JT8D-17AR	B747-400 GB : CF6-80C2B1F
B737-300 : CFM56-3B1	B747-400 RB : RB.211-524G
B737-300 : CFM56-3B2	B747-400 GM : CF6-80C2B5F
B737-400 : CFM56-3B2	B747-400 PM : PW4062
B737-400 : CFM56-3C1	B747-400D : CF6-80C2B1
B737-500 : CFM56-3B1	B747-400ERF : CF6-80C2B5F
B737-600 : CFM56-7B18	B747-400ERF : PW4062
B737-600 : CFM56-7B22	B747-400ERF : RB.211-524H-T
B737-700 : CFM56-7B20	B747-400ERGM : CF6-80C2B5F
B737-700 : CFM56-7B24	B747-400ERPM : PW4062
B737-700ER : CFM56-7B20	B747-400ERRM : RB.211-524H-T
B737-700W-BBJ : CFM56-7B18	B747-400F : CF6-80C2B1
B737-800 : CFM56-7B24	B747-400F : PW4056
B737-800 : CFM56-7B27	B747-400F : RB.211-524G
B737-800W-BBJ2 : CFM56-7B18	B747-400M : PW4056
B737-900 : CFM56-7B26	B747-400M : CF6-80C2B1
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